

Post Construction Storm Water

BMP

BEST MANAGEMENT PRACTICES



Dodge City, Kansas

Post Construction Storm Water **BMP** **BEST MANAGEMENT PRACTICES**

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WILSON
& COMPANY

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Section 1

Introduction

1.1 Background

Stormwater runoff is defined as excess water from any precipitation event not intercepted or retained by vegetation and that results in overland flow (Davis, 2005). Runoff, when managed by traditional systems, adversely impacts surface water quality in two ways: through the introduction of nonpoint source (NPS) pollutants and by altering the hydrologic cycle. Thus, sustainable stormwater management is crucial for the protection of public health and safety and for the maintenance of surface water quality and quantity.

The National Pollutant Discharge Elimination System (NPDES) permit program was developed by the Environmental Protection Agency (EPA) to address water quality issues imposed by urban stormwater runoff. The NPDES permit program requires municipalities and local entities to meet technology based effluent limitations and attain a 5-year renewable permit (EPA, 1999). Phase II of this program requires operators of municipal separate storm sewer systems (MS4) as defined by the EPA to pursue stormwater programs that protect water quality and reduce discharge of pollutants from new and re-developed areas (EPA, 2005).

The EPA designated the Kansas Department of Health and Environment (KDHE) to regulate the NPDES MS4 Stormwater Phase II program in Kansas. KDHE implemented a general permitting procedure to meet this requirement. The operator of a Phase II MS4 submitted a notice of intent in March 2003 that included a list of Post-Construction Best Management Practices (BMPs) specific to their community, and a measurable goal for each BMP to achieve over the 5-year permit term. The purpose of this manual is to assist Phase II cities in Kansas to meet the BMP implementation requirements defined in this permit.

1.2 Why a BMP Manual?

As part of complying with the NPDES general MS4 permit, a complete Stormwater Management Plan (SMP) is required. By implementing post construction BMPs in a stormwater management system, an agency can work to protect and improve water quality. The six minimum controls defined in this plan, and measures put in place to achieve each control, are described below.

- **Public Education and Outreach.** Installation of post construction BMPs provides opportunities for education using signs and brochures to communicate what a BMP is and how they function (Section 2.4). This manual provides guidance for construction and maintenance of lot level BMPs that can be implemented by an individual homeowner or business (Section 4.2).
- **Public Involvement and Participation.** BMPs provide volunteer opportunities for inspection and maintenance (Section 2.4 and Section 5.3).

- **Illicit Discharge Detection and Elimination.** Not applicable to this manual.
- **Construction Site Stormwater Runoff Control.** Not applicable to this manual. Please refer to local Construction Manual (if applicable).
- **Post-Construction Stormwater Management in New Development and Redevelopment Projects.** This manual focuses on providing structural BMP definition, design guidance, implementation guidelines, and inspection and maintenance practices, as well as non-structural BMP recommended guidelines. (Section 2, Section 3, Section 4, Section 5)
- **Pollution Prevention/Good Housekeeping for Municipal Operations.** BMP short and long-term inspection and maintenance requirements are defined in this manual (Section 5).

1.3 How to Use This Manual

This manual is intended to be used as a guide for the successful implementation of post construction stormwater BMPs. The design criteria, implementation guidelines, and inspection and maintenance recommendations outlined in this manual are intended to assist Kansas Stormwater Consortium Phase II cities in meeting requirements mandated in the 2004 NPDES permit for Post-Construction BMPs. This manual should serve as a guideline from which each agency can develop ordinances, design criteria, and construction standards and specifications for implementation of BMPs.

- **Section 2 – Implementation Guidelines.** Section 2 provides guidelines on how to implement BMPs into an agency’s stormwater infrastructure, from what BMP is appropriate for a specified type of development, what questions should be asked in relation to BMPs during the development process, and to how to combine BMPs together in a treatment train for increased water quality benefits. This section also contains information on how to use post construction BMPs for meeting public outreach goals.
- **Section 3 – Non-Structural BMPs.** Section 3 provides guidelines for non-structural BMPs, including stream buffer policy definition, preserving natural vegetation, and restoring natural vegetation. These BMPs are typically designated in an agency’s stormwater or watershed master plan, or defined during the planning stage of the development process. These BMPs can provide extraordinary benefits to stream health and stormwater runoff water quality with minimal long-term maintenance cost.
- **Section 4 – Structural BMPs.** Section 4 provides design guidance and examples for lot level BMPs, bioretention facility, vegetated swale, filter strip, infiltration trench, and extended dry and wet detention. Each section is intended to be independent; other sections may need to be referenced for additional calculation and/or

- maintenance information. The design summary table at the beginning of each structural BMP section provides condensed design guidance.
- **Section 5 – Operation and Maintenance.** Section 5 provides information on bringing BMPs into an agency’s maintenance schedule, including inspection and acceptance guidelines for BMPs associated with development practices. Inspection and scheduled maintenance checklists and forms are included for both vegetated and non-vegetated BMPs for designated time-frames.
- **Appendix A – Precipitation Information.** This section provides a map of varying precipitation zones in Kansas and the complete table of precipitation information for 14 cities in Kansas. The purpose of the map is to show how varied precipitation is across Kansas and the importance of precipitation as a factor in choosing appropriate BMPs. The table provides the water quality rainfall event, 14 day wet season rainfall event, and mean event rainfall for Phase II Kansas cities. This table is used for all hydrologic calculations.
- **Appendix B – Soils Information.** Appendix B provides soil texture and hydrologic class information. This data can be used to guide BMP and plant selection. Section 4 outlines appropriate soils for each BMP by hydrologic group. Appendix B.3 includes more detailed soil maps for each Kansas Phase II city.
- **Appendix C – Vegetation Information.** This section presents guidelines for the selection of native vegetation for BMPs. Appendix C.1 provides the general vegetation map for Kansas. Appendix C.2 can be used for more specific vegetation guidelines by ecoregion. Information from this section can be used to inform vegetation specialists with guidelines specific to the ecoregion in which the BMP will be installed.
- **Appendix D – Maintenance Tables.** Appendix D presents the maintenance tables described in Section 5. These tables should be used to guide the design and implementation of a maintenance schedule for each agency. This table can be copied and distributed as checklist form for BMP inspections.
- **Appendix E – Example Stream Buffer Ordinance**
- **Appendix F – Example BMP Brochure**
- **Appendix G – Detention Basin Outlet Structure Calculations and Example Design Worksheets**
- **Appendix H – BMP Application.** Appendix H presents graphs that use the impervious/pervious ratio and soil type as a guide to when BMPs should be applied to a site. A graph is presented for each Kansas Phase II city.
- **Appendix I – Post Construction Stormwater BMP Ordinance**

1.4 Definitions and Acronyms

- American Public Works Association (APWA)
- **Bioretention Soil Mixture (BSM):** A soil mix having defined chemical and physical properties to support a diverse microbial and plant community.
- California Stormwater Quality Association (CASQA)
- Clean Water Act (CWA)
- **Development:** The alteration of the natural landscape for human needs which results in increasing impervious area. This includes installation of utilities, infrastructure, and buildings.
- **Ecoregion:** A relatively homogeneous ecological area defined by similarity of climate, landform, soil, potential natural vegetation, hydrology, or other ecologically relevant variables.
- Environmental Protection Agency (EPA)
- Extended Dry Detention Basin (EDDB)
- Extended Wet Detention Basin (EWDB)
- Federal Emergency Management Agency (FEMA)
- **First Flush:** The quantity of initial runoff from a storm or snowmelt event that commonly contains elevated pollutant concentrations. The first flush often contains a majority of pollutants in a drainage area.
- Hydrologic soil groups (HSG)
- Idaho Department of Environmental Quality (IDEQ)
- Kansas City Metropolitan Chapter of the APWA (KCMetro APWA)
- Kansas Department of Health and Environment (KDHE)
- **Karst:** A landscape characterized by the dissolution of a layer or layers of soluble bedrock, such as limestone.
- Manual of Uniform Traffic Control Devices (MUTCD)
- MidAmerica Regional Council (MARC)
- Municipal separate storm sewer system (MS4)

- **National Pollutant Discharge Elimination System (NPDES):** Defined in Section 402 of the Clean Water Act, this provides for the permit system that is key for enforcing the effluent limitations and water quality standards of the Act. The Phase II final Rule – published in the Federal Register on December 8, 1999 – requires NPDES permit coverage for stormwater discharges from certain regulated, small, municipal, separate storm sewer systems (MS4s) and from land areas greater than 1 acre disturbed by construction.
- **Native Vegetation:** Plant types historically located in this geographic area that are extremely well adapted to the climate and natural disturbances (e.g., fire, grazing, and/or flooding) of the region. Furthermore, these plant species have co-evolved with a suite of insects, microbes, and other wildlife. As a result, the grasses, wildflowers, sedges, forbs, shrubs, and trees of these plant communities are drought tolerant, disease and insect resistant, and hardy.
- Natural Resources Conservation Service (NRCS)
- **Non-point Source (NPS) pollutant:** Pollution that occurs over a diffuse area when rainfall, snowmelt, or irrigation runs over land or through the ground, picks up pollutants, and deposits them into rivers, lakes, and coastal waters or introduces them into ground water.
- **Post-Construction Best Management Practices (BMPs):** Methods that have been determined to be the most effective, practical means of preventing or reducing pollution from non-point sources and minimizing runoff to waters of the United States after construction of an area is complete.
- **Pre-Development:** Conditions that existed prior to development (actual or proposed).
- **Redevelopment:** Development activities that occur on a site that is already developed. This includes remodeling that adds impervious area, tearing down/rebuilding structures, and expanding existing development, including constructing parking lots and non-habitable buildings.
- Stormwater Management Plan (SMP)
- **Time of Concentration (T_c):** The overland flow time to the most upstream inlet or other point of entry to an enclosed system or channel (T_i) plus the time for flow to travel in the enclosed system or channel to the point of consideration (T_T).
- **Total Maximum Daily Load (TMDL):** A regulatory limit on the amount of pollutants that can be released into a body of water without adversely affecting water quality.
- **Treatment train:** BMPs in series that work as a system to remove pollutants by providing treatment efficiencies necessary for managing stormwater runoff.

- Urban Drainage and Flood Control District (UDFCD) Denver, Colorado
- **Water Quality Rainfall Event:** The storm event that produces less than or equal a defined percent volume of all rainfall events on an annual basis.
- **Water Quality Volume (WQv):** The runoff generated by the water quality rainfall event.
- **Watershed:** All the land area that drains to a given point that may also be called a basin, catchment, or drainage area.

1.5 References

Davis, A.P. 2005. *Green Engineering Principles Promote Low Impact Development*. American Chemical Society: Environmental Science and Technology. 39: 3 39A344A.

EPA. 1999. *Federal Registrar Report to Congress on Phase II Stormwater Regulations Final Rule*. (64) 235.

EPA. 2005. *Stormwater Phase II Final Rule*. EPA 833-F011. Available at: www.epa.gov/NPDES/stormwater. Accessed 19 May 2008.

MARC and APWA. 2008. *Manual of Best Management Practices for Stormwater Quality*. Available at www.marc.org/environment/Water/bmp_manual.htm

Wilson & Company with Camp Dresser & McKee, Inc. 2003. *Best Management Practices Menu for NPDES MS4 Stormwater Phase II Services*.



Section 2

Implementation Guidelines

2.1 Applying BMPs to Development Practices

Post construction stormwater BMPs should be applied when areas are developed or redeveloped. In general, development changes the land cover from pervious areas that can infiltrate rain water to impervious areas that do not infiltrate rain water. Impervious areas such as roof tops, driveways, streets, and parking lots increase the amount of impervious area, which increases the amount of stormwater runoff. Studies have shown that impervious areas accumulate more pollutants that runoff with the first flush of stormwater. Therefore, stormwater BMPs should be applied to developments or redevelopments to reduce the impacts of the increased impervious area.

A guideline for applying BMPs to development or redevelopment projects is the impervious to pervious ratio. For a given project, the amount of impervious and pervious area should be calculated and reviewed by the local jurisdiction. The calculated ratio of impervious to pervious area gives an indication of the impact of the development to the water quality of the receiving water body. A ratio of 1 or greater indicates a very high water quality impact, which will require the implementation of stormwater BMPs. A ratio of less than 1 indicates a likely need for BMPs depending on the soils and the water quality event. Appendix H contains figures of the impervious to pervious ratio verses excess water quality volume for each city at the 85 and 90 percent rainfall events. Two figures (85-percent and 90-percent events, respectively) for each City are provided as a guide for when BMPs should be applied to sites for impervious to pervious ratios of less than 1 by hydrologic soils group (HSG). BMPs are required within the shaded area of the graph based on the impervious to pervious ratios and HSG.

The HSG of the site soils should be determined from the Natural Resources Conservation Service (NRCS) county soil survey. Appendix B provides a general map of the HSG by City. Soils on sites developed since the publication of the NRCS soil survey should be decreased a HSG (e.g. HSG B would be HSG C). The HSG used should also be reduced one level if the existing site soils are not protected and restored. During development soils are significantly impacted either by compaction, which reduces infiltration, or removal of the top soil during site grading which is often not restored. In either case, the developed HSG used with Appendix H should be reduced one level (e.g. HSG B to HSG C). The original soils HSG should only be used if the native site soils are removed prior to construction, stockpiled, and restored after construction.

In some cases, an on-site infiltration test, or percolation test, may be used to determine the actual pervious area infiltration rate. In those cases, Table 2-1 can be used to determine the HSG for the site. It is recommended that at least three locations be

tested with this method, and the median infiltration rate then used for determining the HSG in Table 2-1.

Table 2-1 Infiltration Rates by HSG

HSG	Median Infiltration Rate (in/hr)
A	0.375
B	0.225
C	0.100
D	0.025

Example:

A new single family residential development in Emporia, Kansas with a total area of 4.5 acres has the following proposed impervious area:

Imp. Cover	Area (sq. ft)
Streets	21,500
Sidewalks	3,285
Driveway	16,500
Buildings	24,750
Total	66,035

The impervious/pervious ratio is $66,035/129,985 = 0.51$

The existing site soils are HSG B. The developer does NOT plan on removing, stockpiling, and restoring the native soils so the developed site soils are HSG C.

Assuming a 90-percent rainfall event for Emporia, Kansas, the corresponding figure in Appendix H indicates that BMPs are required for this site (within the shaded area).

The developer will need to apply post construction BMPs to this site.

The figures provided in Appendix H are a guideline for applying BMPs to new development or redevelopment. Local jurisdictions may require BMPs outside of the shaded area in cases where there is an existing TMDL or the site area drains to a sensitive water body. Check with your local jurisdiction in these cases.

As development within a community occurs, Table 2-2 provides guidance in how to apply BMPs to a given site, based on type of development and the drainage area to that development. The table provides applicability guidelines for each BMP in relation to the type of development. For example, infiltration trenches have a low applicability to industrial development due to a potential ground water pollution risk. On the other hand, bioretention has a high applicability to development of commercial sites, based on the drainage area to the site and the water quality treatment that the BMP provides.

Table 2-2 Development Matrix for BMP Application

BMP	Agricultural and Park Land	Residential Large Lot >2 ac	Residential Small Lot <2 ac	Multi-Family	Commercial	Industrial	Streets / Parking Lots	Drainage Area
Lot Level BMPs	M	H	H	H	M	M	M	< 1/8 acre
Bioretention	L	L	L	M	H	H	H	< 4 acres
Vegetated Swale	M	H	L	M	M ¹	M	M	< 5 acres
Filter Strips	H	H	M	M	H	H	H	< 2 acres ³
Infiltration Trench	L	L	L	M	H	L ²	H	< 5 acres
Infiltration Basin	L	M	S	H, S	H, S	L ²	H	< 5 acres
Extended Dry Detention	H	S	S	S	H, S	H, S	M	> 10 acres
Extended Wet Detention	H	S	S	S	H, S	H, S	M	Water budget > 40 acres
H High applicability								
M Medium applicability								
L Low applicability								
S Subdivision level applicability								

¹ Consider trash and floatables during selection and design.

² Consider potential groundwater pollution risk during selection and design.

³ Limit concentrated flow.

Specific policy regarding implementation of BMPs in relation to development, redevelopment, and public improvement projects should be defined by the respective municipality, county, or agency that adopts this manual.

It is important to pay special attention to when in the construction process a specific BMP is defined and/or installed. Site conditions during installation can affect the overall function of both non-structural and structural BMPs, and ultimately the respective BMPs' long-term success. Table 2-3 outlines the earliest possible installation time for a BMP during the site construction process.

Table 2-3 BMP Earliest Installation

Prior to any Land Disturbance	
Stream Buffer	Boundary of buffer or preservation area should be delineated with orange construction fence and silt fence.
Preserve Existing Vegetation	
Erosion and Sediment Control / Land Disturbance Plan	
Filter Strips	Can be used in conjunction with other erosion control measures, as part of a comprehensive land disturbance plan
Extended Dry Detention	Possible sedimentation basin location. After drainage area stabilization, will require cleaning/dredging and converting to detention.
Extended Wet Detention	
Site Stabilization	
Rain Gardens (<i>non lot level</i>)	Drainage area to BMP stabilized, with a minimum of 70% vegetation density
Bioretention	
Vegetated Swale	
Infiltration Basin	
Infiltration Trench	
Individual Lot Close-Out and/or Issuance of Occupancy Permit	
Restoration of Native Vegetation	Post infrastructure and building construction; Part of final site stabilization; Installed prior to issuance of occupancy permit
Lot Level BMPs	

2.2 Guidelines for BMPs in Series (Treatment Train)

The preferred approach for water quality improvement is a combination of stormwater BMPs in series called a “treatment train.” A treatment train can increase pollutant removal efficiency by providing additional treatment and volume reduction. Selection of treatment train components should be based on a combination of local and state stormwater requirements, site characteristics, development needs, runoff sources, financial resources, and BMP characteristics (such as space requirements, design capacities, and construction and maintenance costs). (MARC, 2008)

A treatment train is two or more BMPs in series that capture, filter, then infiltrate or store and treat stormwater. The combination of processes provides cumulative water quality benefits. The BMPs chosen for a treatment train should be placed in series as follows:

- (1) Capture at source (rain barrels),
 - (2) Filter overland flow (swales; filter strips),
 - (3a) Infiltration systems (bioretention; infiltration trench; rain gardens),
- Or,
- (3b) Treatment and storage (extended wet detention; extended dry detention).

Depending on the combination of BMPs chosen, different levels of water quality benefits can be experienced. Table 2-4 presents BMP combinations for treatment trains and the associated applicability for water quality benefits.

Table 2-4 Treatment Trains and Water Quality Benefits

Treatment Trains and Water Quality Benefits								
	Second BMP in Series							
First BMP in Series	Infiltration Trench	Infiltration Basin	Filter Strip	Vegetated Swale	Rain Garden	Bioretention	Extended Wet Detention	Extended Dry Detention Basin
Filter Strip	H	H		L	H	H	M	M
Vegetated Swale	H	H	L		M	H	M	L
Bioretention ¹				M			M	M
Extended Wet Detention		L		L			M	M
Extended Dry Detention Basin				L			L	L
H	High							
M	Medium							
L	Low							
(1) Assumes underdrain system.								

2.3 Design Considerations for BMP Implementation

Design considerations for BMP implementation can be divided among three broad categories: planning and design, construction practices, and maintenance/inspection. All should be considered and outlined prior to a project beginning construction. These processes will be presented in more detail in Sections 3, 4, and 5. The following is a series of questions agencies, planners, designers, and contractors should consider during the BMP project process.

2.3.1 Planning and Design (Section 3 and Section 4)

As a project enters the planning and design stage, some key questions to ask in relation to applicability and design of BMPs include:

- What is the existing land use of the site?
- What is the designated land use of the site?
- What is the area of the project site?
- What is the total tributary drainage area of the site being developed, including the site and any drainage area to the site?
- How much impervious area is planned for the site? Are pervious alternatives an option?
- What is the ground slope of the site?
- What portions of the site will be left undisturbed, if any?

- Is there any known downstream water quality or flooding issues?
- What are the adjoining land uses to the site?
- What vegetation is planned for the site?
- Where are the BMPs located?
- Who will be responsible for long-term maintenance of any infrastructure and/or BMPs installed?
- What percentage of the site area drains to proposed BMPs?
- Have maintenance and access easements/agreements been defined for the BMP?
- Have complete construction plans, including at a minimum design plans and details, vegetation plan (if required), and implementation schedule, been provided for use by a contractor?

2.3.2 Construction Practices (Section 4 and Section 5)

As a project enters the construction stage, some key questions to ask in relation to the construction and implementation of BMPs include:

- Has an erosion and sediment control plan, including site stabilization, been defined for the site?
- Has erosion control and land disturbance practices been defined using a phased approach?
- How will silt, sediment, and construction activity affect proposed BMPs?
- When in the construction schedule should the BMP be constructed? How does this compare to the growing season?
- When in the construction schedule should the BMP be put on-line?
- How will the construction of the BMP be validated? Who will inspect and do initial maintenance of the BMP?
- Has the maintenance and inspection requirements been recorded with property?

2.3.3 Maintenance and Inspection (Section 5)

As a BMP comes on-line and therefore becomes part of infrastructure routine maintenance and inspection practices, some considerations include:

- Who will be responsible for on-going maintenance of the BMP?

- Have short and long-term maintenance schedules been defined for the BMP?
- Have short and long-term maintenance plans been defined for the BMP?
- How will inspection and maintenance activities be monitored and documented?

2.4 Public Outreach

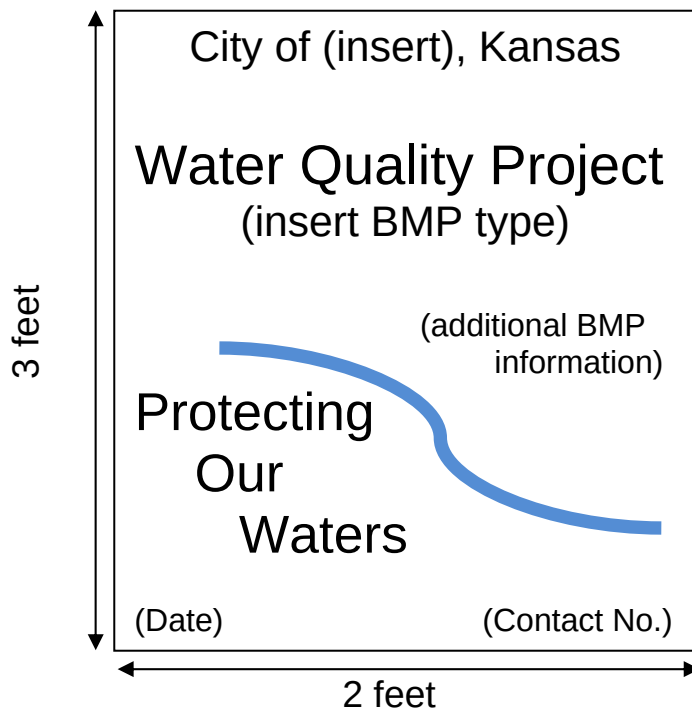
The installation of a BMP presents itself as an education tool for the community. Post construction BMPs are often installed in areas of high visibility to the public. Using signage, the Internet, brochures, and community programs provides opportunities for those who live, work, and play near a BMP to learn about this piece of infrastructure, and even aid in its long-term success by helping to maintain it.

Routine maintenance tasks can provide volunteer opportunities for the community. This can be accomplished in a number of ways. Regardless of how volunteers are utilized, inspection and maintenance guidelines would still need to be established by the overseeing agency. The agency would also need to document any inspection and maintenance performed by this organization to ensure the long-term integrity of the BMP. Examples include:

- **Green Team.** A “Green Team” comprised of community volunteer members could be established to routinely inspect and complete some maintenance tasks on a BMP. The Green Team could even be a management point for interested volunteer organizations throughout the community, designating which volunteer organization is going to perform what maintenance, and when this will occur.
- **Adopt-A-BMP.** Similar to the “Adopt-A-Highway” program, an agency can implement an “Adopt-A-BMP” program. An adopting business or volunteer group could contribute funding or time to inspection and maintenance of the BMP. This program could be utilized for funding and/or long-term maintenance programs.

Signs and brochures provide great opportunities for communication and discussion in the community. It is recommended that each BMP installed be designated using signage defined by the respective agency. To identify a BMP from other surrounding vegetation and development, a sign should be installed at a location in which the BMP would be most accessed. Signage can range from simply stating the type of BMP installed, to complete details on what it is, and why it is installed. Below is an example of a recommended format for a BMP informational sign:

Figure 2-1 Recommended Format for a BMP Informational Sign



Any signs that will be adjacent to public streets should follow Manual of Uniform Traffic Control Devices (MUTCD) guidelines. Design criteria for sign to be installed (size, height of lettering, color, site placement, information to be included) can be agency specific or project specific and should be defined during the planning and design stage of a project.

Brochures can also be good educational tools for BMPs. See Appendix F for an example of a BMP brochure used by the North Carolina Forest Service.

2.5 References

North Carolina Division of Forest Resources.
<http://www.dfr.state.nc.us/publications/WQ0307.pdf>.

MARC and APWA. 2008. *Manual of Best Management Practices for Stormwater Quality*. Available at www.marc.org/environment/Water/bmp_manual.htm.



Section 3

Non-Structural BMPs

3.1 Stream Buffers

A stream buffer or stream setback is a designated area around a stream, lake, or wetland left in a natural, densely vegetated state so as to protect the receiving water quality and provide space for the natural stream to meander. Within this designated area, development, construction practices, and land uses are restricted for a given width adjacent to a stream. A stream buffer preserves land adjacent to streams and wetlands rather than constructing an element to filter or treat stormwater, thus fitting the definition of a non-structural BMP.

3.1.1 Stream Buffer Policy Definition

Stream buffers are generally implemented through an agency's specific policy or ordinance. There are three major components to development of stream buffer policy and/or ordinance: application of the buffer, buffer width, and permissible land uses within the buffer. In order to define these components, an agency must determine

- Where in a watershed will a stream buffer apply?
- What width is the stream buffer?
- What land uses and/or construction activities are restricted or allowed within the stream buffer?

In general, the determination of stream buffer application, width, and land uses amounts to what is acceptable risk to an agency with regards to water quality and habitat preservation.

EPA Region 7 has a model stream protection ordinance that an agency can utilize. An example of this ordinance is included in Appendix E. This ordinance should be reviewed thoroughly by an agency and an agency's legal council before enactment.

3.1.2 A Typical Stream Buffer

A stream buffer's total width is typically divided into two to three zones. Zones closest to a stream have the most restrictions (inner zone). Zones further from the stream have increased flexibility of use (outer zone(s)). Permanent structures, including impervious surfaces, are typically not allowed in either the inner or first outer zone.

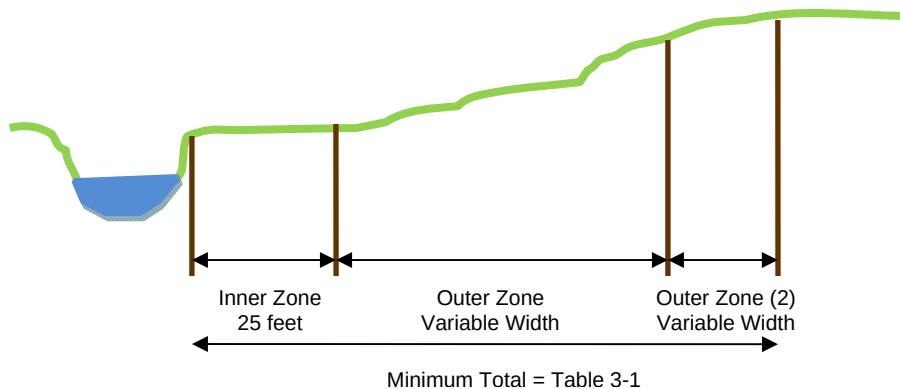
- Inner Zone. The inner zone extends from the stream centerline or from the edge of bank for a specified width to protect the immediate streamside area. Construction and land disturbance is prohibited in this zone, but if native vegetation establishment is needed, planting with fast growing tree and shrub species, native grasses, and wildflowers is recommended.

- **Outer Zone(s).** The outer zone extends from the limits of the inner zone for a width that may be set or variable. The variable width allows flexibility for an agency to apply a zone width based on different degrees of protection for different stream characteristics, such as floodplains and steep slopes. It is common to divide the outer zone into two zones based on floodplain location and/or permitted land use, with the least amount of restriction in the most outer zone. The advantage of multiple outer zones is that the transition from highly protected to minimally protected areas is more gradual. Construction and land use is restrictive in the outer zone(s). Park trail systems, utility construction, and residential landscaping could be permitted.

3.1.3 Proposed Stream Buffer Guidelines

The following are proposed recommended stream buffer guidelines. An example of stream buffer zones is demonstrated on Figure 3-1.

Figure 3-1 Example of Stream Buffer Zones



- **Application.** Streams with a drainage area exceeding 40 acres shall have a defined stream buffer. Should an agency choose, the minimum stream buffer width could also be used for drainage areas less than 40 acres.
- **Width.** Table 3-1 provides recommended minimum stream buffer total widths based on drainage area to a stream. This width is equal to the inner zone plus outer zone(s).

Table 3-1 Minimum Stream Buffer Width (Inner Zone plus Outer Zone(s))

Drainage Area (acres)	Minimum Buffer Width, from Edge of Stream Bank Outwards, Measured Separately in Each Direction (feet)
Less than 40	40
40 to 160	60
160 to 5,000	100
Greater than 5,000	120

- **Define Stream Buffer Inner Zone.** It is recommended that the width of this zone extend a minimum of 25 feet outward from the edge of the stream bank.
- **Define Stream Buffer Outer Zone(s).** This zone(s) will extend from the edge of the inner zone outward a variable distance. It is recommended that at a minimum this width include the FEMA 100-year floodplain and any defined floodplain by the local agency. Width of more than one defined outer zone can be correlated with permittable land use.
- **Permittable Land Use.** This will vary by agency. Land uses in the inner zone should follow recommendations presented in 3.1.2 for Inner Zone, with construction and land disturbance prohibited or severely restricted. Land uses in the outer zone(s) should follow recommendations presented in 3.1.2 for Outer Zone(s), with construction and land use restricted.

3.1.4 Implementation

To preserve a defined stream buffer's integrity adjacent to developed sites, temporary measures are necessary during construction stages. It is recommended to delineate a defined stream buffer boundary on the construction site with orange construction fence to ensure no access will occur that might disturb native vegetation. Depending on land disturbance adjacent to the stream buffer and the lay of the land, silt fence may also be required to prevent sedimentation from accumulating in the stream buffer area. Construction plans, including plans for public improvement, grading, building, site development, or other utility installation, should clearly show all stream buffer areas on a site and indicate that stream buffer areas are to be left undisturbed.

Permanent measures should also be implemented to ensure the long-term integrity of the stream buffer. As buffers can extend onto private property, there is a risk that this portion of the land may be changed over time by a property owner (i.e. installation of a fence). Survey pins may be installed to assist future property owners, contractors, or surveyors in delineating the original boundary of a stream buffer. In addition, it is recommended that an agency inspect their respective stream buffer a minimum of every three years for vegetation health and violations of permitted land use.

3.1.5 References

Black & Veatch. 2002. Stream Protection Guidelines, prepared for EPA Region 7.

EPA. 2006. Model Stream Buffer Ordinance. Available at:
www.epa.gov/owow/nps/ordinance/buffers.htm

MARC and APWA. 2008. *Manual of Best Management Practices for Stormwater Quality*. Located at www.marc.org/environment/Water/bmp_manual.htm

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Section 3

Non-Structural BMPs

3.2 Preserve Existing Native Vegetation

To preserve existing native vegetation, land must be delineated prior to development and left completely undisturbed during construction (CASQA, 2003). This area may be utilized for non-invasive recreational uses post-development, but primarily must be left untouched. Many times native vegetation preservation can be designated in sights undesirable for development (steep slopes, watercourse). Public or private right-of-ways, utility easements, wetlands, and surface water bodies may not be considered for preservation purposes. Advantages of preserving a site with native vegetation include (IDEQ, 2005 and Stormwater Authority, 2009):

- Decreases stormwater runoff through interception, infiltration, and evapotranspiration
- Effective immediately, no time required for establishment
- Allows areas for wildlife to retain natural habitat
- Provides buffers and screens against noise or visual disturbances
- Protects natural resources for future generations.

Figure 3-2 is a photograph of preserved existing native vegetation.

Figure 3-2 Tall-grass Prairie Alongside McDowell Creek Road Outside of Manhattan, KS (City-Data.com)



3.2.1 Goals

The goal of native vegetation preservation is to maintain pre-development hydrologic patterns in the midst of development. Preserved land also provides habitat for wildlife. In addition, studies have shown that connected open space along stream corridors is the most beneficial for wildlife habitat.

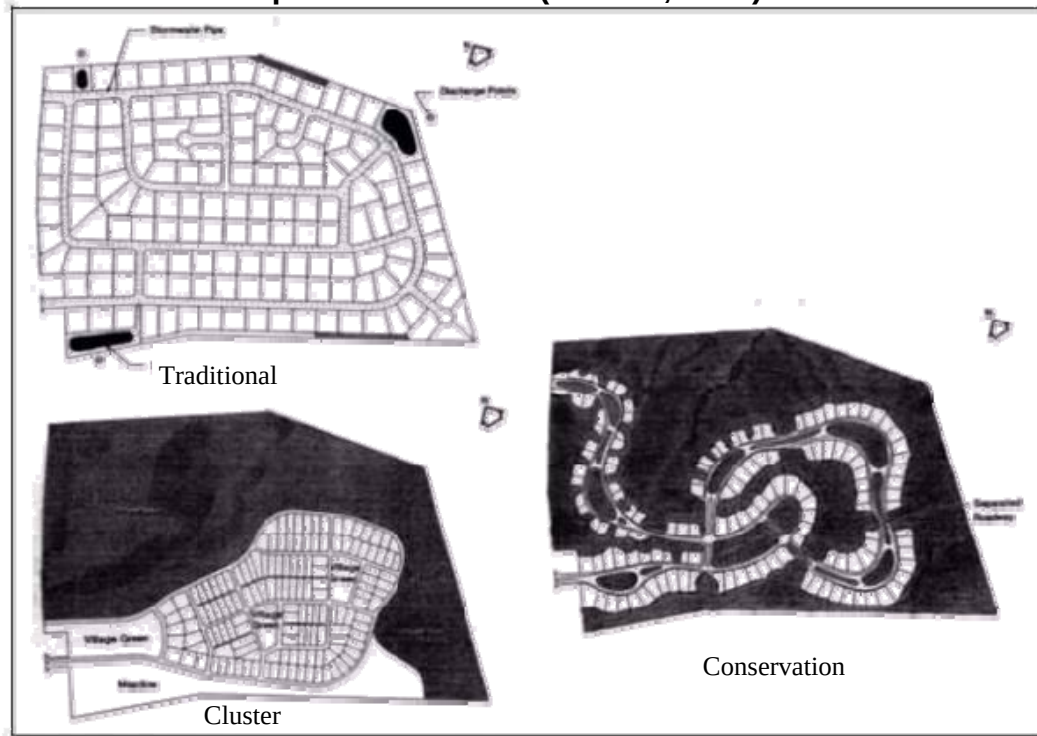
3.2.2 Preservation Process

Preservation of existing native vegetation can be achieved in a number of ways:

- **Master Plan.** An agency can designate certain areas for preservation as part of their master plan process. This can be achieved through a land dedication process, through either easement or agency land acquisition. It is recommended that an agency investigate what percentage of their current land area is defined as preserved. This can establish a baseline from which an agency can increase land preserved. Goals might include increasing an agency's preserved land by a certain percentage over the next five years, or require a certain percentage of all new development sites to be preserved. Typical goals are 10 to 20-percent open space preservation.
- **Development Practices.** An agency can encourage cluster land development of a site. This method of development limits the amount of land disturbed on a site, by concentrating all utility, road, and building construction to a defined portion of the site. Often this is defined by limiting development to a certain percentage of the

site. Figure 3-3 shows three examples of a site that has been developed using three different methods.

Figure 3-3 Cluster Land Development Schedule With Schematics Of Development Scenarios (DNREC, 1997)



3.2.3 Maintenance

Manage construction activities to limit impacts on native vegetation in areas marked for preservation. It is recommended to delineate the preservation area boundary on the construction site with orange construction fence during construction to ensure no access will occur that might disturb native vegetation. Depending on land disturbance adjacent to the preservation area and the lay of the land, silt fence may also be required to prevent sedimentation from accumulating in the preservation area. Construction plans, including plans for public improvement, grading, building, site development, or other utility installation, should clearly show all preservation areas on a site and indicate that native vegetation areas are to be left undisturbed. Implement erosion control devices to limit sedimentation influx into preserved areas.

After development is complete, routinely check native vegetation preservation area to ensure stabilization and to check for sedimentation. In addition, it is recommended that an agency inspect their preservation areas a minimum of every three years for vegetation health and violations of permitted land use. As a preservation area could extend onto private property, there is a risk that this portion of the land may be changed over time by a property owner (i.e. installation of a fence). Survey pins may be installed to assist future property owners, contractors, or surveyors in delineating

the original boundary of a preservation area. Irrigation of the preserved landscaping may be needed to ensure survival during extended dry periods (IDEQ, 2005).

3.2.4 References

CASQA. 2003. *California Stormwater Quality Association Stormwater Best Management Practice Handbook*. Available at www.dot.ca.gov/hq/construc/stormwater/manuals.htm

IDEQ. 2005. *IDEQ Storm Water Best Management Practices Catalog*. Available at www.deq.state.id.us/

Stormwater Authority Organization. Available at www.stormwaterauthority.org

Section 3

Non-Structural BMPs

3.3 Restoration of Native Vegetation

For instances where land has been disturbed, it can be advantageous to restore vegetation to its native condition. Native vegetation reduces stormwater runoff by intercepting rainfall in its canopy, reducing surface water velocity across the ground surface, and by increasing the infiltration capacity of the soil by extending deep roots and facility soil microbial interactions that create permeable soil structure. Restoration of native vegetation is beneficial at all scales. Advantages of restoring a site with native vegetation include (MARC 2008):

- Less maintenance with regards to watering, fertilizer or chemical maintenance.
- Deep roots provide increased infiltration and durability in extreme weather.
- Attracts wildlife and improves biological diversity.

An example of an area that has been developed and then restored back to native vegetation is shown in Figure 3-4.

Figure 3-4 Native Vegetation Area That Serves as a Stormwater BMP, Wildlife Habitat and Aesthetic Area (US Army Corps, 2000)



3.3.1 Goals

To restore an area to pre-development native vegetation, soil and land slope conditions must be met to establish pre-development hydrologic function.

3.3.2 Restoration Process

- **Restore Site Quality.** It may be necessary to augment soil to restore it to pre-development conditions with compost or other sub-soil additions (Pennsylvania, 2006). Exotic and invasive species should be removed (preferably mechanically, not chemically). Other non-native landscape features should also be removed (dams, tile drainage) and erosion should be contained (MARC, 2008).
- **Select Native Vegetation.** Based on the restoration site size, consider the desired aesthetic appearance of the BMP (plant height, mixes). A smaller site should use only a few native vegetation varieties, while a large site may be able to incorporate many varieties. Also determine the following characteristics specific to the restoration site:
 - Soil types (soil tests, soil maps in Appendix B)
 - Annual precipitation with dates for wet/dry season (Maps in Appendix A)
 - Ecoregion and corresponding native vegetation (Map and table in Appendix C)
 - Previous land use

Provide the soil type, precipitation, previous land use, and ecoregion information to a native vegetation expert for planting suggestions (native vegetation types, seeding rates, establishment procedures, maintenance procedures). Use the “typical vegetation by ecoregion” listed in Appendix C as a guideline to check final plant list. Native vegetation contacts and links are listed in Appendix C.

Preservation of existing native vegetation can be achieved in a master plan or in a development plan as outlined in 3.2.2 for native vegetation preservation.

3.3.3 Maintenance

Manage construction activities to limit impacts to areas designated for restoration. Implement erosion control devices to limit sedimentation influx into the defined area. After native vegetation planting is complete, routinely check to ensure stabilization of restored area and to check for sedimentation. Stormwater runoff to restored area may need to be rerouted around the area until native vegetation is densely established (70-percent of ground cover). Irrigation of the landscaping may be needed to ensure survival during extended dry periods (IDEQ, 2005). Reference maintenance guidelines outlined for vegetated BMPs in Appendix D.

3.3.4 References

MARC and APWA. 2008. *Manual of Best Management Practices for Stormwater Quality*. Located at www.marc.org/environment/Water/bmp_manual.htm

Pennsylvania. 2006. *Pennsylvania Stormwater Best Management Practices Manual*. Available at www.blairconservationdistrict.org/SWBMP.htm

IDEQ. 2005. *IDEQ Storm Water Best Management Practices Catalog*. Available at www.deq.state.id.us/



Section 4

Structural BMPs

4.1 Hydrology Methods

Sizing BMPs properly is critical to their success. Two hydrology methods are typically used in calculations depending on whether the intent of the BMP is to capture and treat the Water Quality Volume (WQ_v), or to handle the peak discharge of the WQ_v. Table 4-1 is a summary of BMP hydrologic calculation types and their application.

Table 4-1 BMP Hydrologic Calculation Types

BMP	Hydrology Methods	
	WQ _v	Peak WQ Discharge
Bioretention	X	
Extended Dry Detention Basin	X	
Extended Wet Detention Basin	X	
Filter Strip		X
Infiltration Trench	X	
Swales		X

4.1.1 Water Quality Volume (WQ_v)

Detention and retention BMPs should be designed to capture and treat the WQ_v. Conveyance BMPs should be designed to handle the peak discharge of the WQ_v. WQ_v is based on the water quality rainfall event and volumetric runoff coefficient of the drainage area. The water quality rainfall event for each city can be found using Table 4-2.

Table 4-2 The 90-percent and 85-percent Water Quality Rainfall Event by City

City	County	KS Region	90% (inch)	85% (inch)
Dodge City	Ford	West	0.79	0.58
Garden City	Finney	West	0.89	0.60
Hays	Ellis	West	0.90	0.70
Great Bend	Barton	Central	1.00	0.80
Manhattan	Riley	Central	1.10	0.82
Newton	Harvey	Central	1.20	0.90
Salina	Saline	Central	1.07	0.80
Arkansas City	Cowley	Central	1.20	0.92
Hutchinson	Reno	Central	1.20	0.90
Winfield	Cowley	Central	1.20	0.92
Coffeyville	Montgomery	East	1.50	1.10
Lawrence	Douglas	East	1.18	0.90
Ottawa	Franklin	East	1.20	0.90
Emporia	Lyon	East	1.20	0.90

Two methods can be used to estimate the WQ_v for a proposed development – the Short-Cut Method and the Small-Storm Hydrology Method.

4.1.1.1 Short-Cut Method (Claytor and Schueler 1996)

The Short-Cut Method should only be used for sites with one predominant land cover type and a drainage area less than 10 acres. This method can be utilized for larger drainage areas if the percent site imperviousness is known.

Short-Cut Method Equations

Equation 4.1 Volumetric Runoff Coefficient

$$R_v = 0.05 + 0.009(I)$$

Where:

R_v = Volumetric runoff coefficient (unitless)
 I = Percent impervious of tributary area (%)

Equation 4.2 Water Quality Volume (Short-Cut Method)

$$WQ_v = \frac{P_{wQ} \times R_v \times A_T}{12}$$

Where:

WQ_v = Water quality volume (acre-feet)
 P_{wQ} = Water quality rainfall event (inches) from Table 4-2
 R_v = Volumetric runoff coefficient
 A_T = Tributary area (acres)

4.1.1.2 Small Storm Hydrology Method (Claytor and Schueler 1996)

The Small Storm Hydrology Method is based on the volumetric runoff coefficient (R_v), which accounts for specific characteristics for the pervious and impervious surfaces of the tributary drainage area. The method may be used for all drainage areas. R_v s are determined by land cover type.

A reduction factor may be applied to the R_v values for drainage areas with disconnected impervious surfaces. The pervious surface flow path below an impervious area must be at least twice the impervious flow path. A summary of volumetric runoff coefficients are provided in Tables 4-3 and 4-4.

Table 4-3 Volumetric Coefficients for Urban Runoff for Directly Connected Impervious Areas (adapted from Pitt, 1987)

Rainfall (inches)	Flat roofs and large unpaved parking lots	Pitched roofs and large impervious areas (large parking lots)	Small impervious areas and narrow streets	Silty soils HSG-B	Clayey soils HSG-C and D
0.50	0.76	0.94	0.62	0.09	0.17
0.75	0.82	0.97	0.66	0.11	0.20
1.00	0.84	0.97	0.70	0.11	0.21
1.25	0.86	0.98	0.74	0.13	0.22
1.50	0.88	0.99	0.77	0.15	0.24

Table 4-4 Reduction Factors to Volumetric Runoff Coefficients for Disconnected Impervious Surfaces (adapted from Pitt, 1987)

Rainfall (inches)	Strip commercial and shopping center	Medium to high density residential with paved alleys	Medium to high density residential without alleys	Low density residential
0.50	0.95	0.18	0.18	0.17
0.75	0.99	0.27	0.21	0.20
1.00	0.99	0.38	0.22	0.21
1.25	0.99	0.48	0.22	0.22
1.50	0.99	0.59	0.24	0.24

Note: To use the reduction factors for disconnected impervious surfaces listed above, the impervious area uphill from a pervious area (a cover type that allows stormwater to infiltrate) should be less than one-half the area of the pervious surface, and the flow path through the pervious area should be at least twice the impervious surface flow path. For example, a 10-foot wide sidewalk would be a “disconnected impervious surface” if separated from the conveyance system by a 20-foot grassed strip other pervious cover.

Small Storm Hydrology Method

Equation 4.3 Weighted volumetric runoff coefficient

$$R_{V,W} = \frac{\Sigma(R_{Vi} * A_{Ci}) + (R_{V2} * A_{C2}) + \dots(R_{Vi} * A_{Ci})}{A_T}$$

Where:

- $R_{V,W}$ = Weighted volumetric runoff coefficient
- R_{Vi} = Volumetric runoff coefficient for cover type i
- A_{Ci} = Area of cover type i (acre)
- A_T = Total tributary area (acre)

Equation 4.4 Water Quality Volume (Small Storm Method)

$$WQ_V = \frac{P_{WQ} \times R_{V,weighted} \times A_T}{12}$$

Where:

- WQ_V = Water quality volume (acre-feet)
- P_{WQ} = Water quality rainfall (inches)
- $R_{V,weighted}$ = Weighted volumetric runoff coefficient
- A_T = Tributary area (acres)

4.1.2 Rational Method

A conveyance BMP should be designed by calculating the peak discharge for the water quality rainfall event using the Rational Method.

Rational Method

Equation 4.5 Runoff Coefficient (Rational Method)

$$C = 0.3 + (0.6 \times I)$$

Where:

C = Runoff Coefficient

I = Percent impervious divided by 100

Equation 4.6 Peak Runoff Rate (Rational Method)

$$Q = C \times i \times A$$

Where:

Q = Peak rate of runoff (cfs)

C = Runoff Coefficient

i = Rainfall intensity for water quality rainfall event from Appendix A at the duration equal to the calculated time of concentration (inches/hr)

A = Tributary drainage area (acres)

Time of Concentration (T_c)

Equation 4.7 Time of Concentration

$$T_C = T_I + T_T$$

Where:

T_C = Time of concentration (minutes)

T_I = Overland flow time to the most upstream inlet or point of entry (minutes)

T_T = Travel time in an enclosed system or channel (minutes)*

**For this manual, this is only used in instances where concentrated flow is entering a BMP.*

(Source: Section 5602.7 of APWA 5600, November 2005)

Overland Flow Time (T_I)

Use the following formula or other method approved by the reviewing agency to calculate overland flow time. Overland flow time shall not be greater than 15 minutes.

Travel Time in an Enclosed System or Channel (T_T)

Equation 4.8 Overland Flow Time

$$T_I = \frac{1.8(1.1 - C)D^{1/2}}{S^{1/3}}$$

Where:

- T_I = Overland flow time to the most upstream inlet or point of entry (min)
- C = Overland Flow Runoff Coefficient for cover type
- D = Overland flow distance parallel to slope (feet); 100 feet shall be the maximum distance for overland flow
- S = Slope of overland flow path (%)

Use the following formula or other method approved by the reviewing agency to calculate the travel time in an enclosed system or channel by dividing the length of travel by the velocity of flow.

Equation 4.9 Channelized Travel Time

$$T_T = \frac{D_C}{V}$$

Where:

- T_T = Channelized travel time (min)
- D_C = Channelized flow distance (feet)
- V = Velocity of flow (ft/min) calculated using Manning's equation

4.1.3 References

MARC and APWA. 2008. *Manual of Best Management Practices for Stormwater Quality*.

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Section 4

Structural BMPs

4.2 Lot Level BMPs

Lot level BMPs are defined as a localized practice that is appropriate for private land owners and concerned citizens to install and operate. These BMPs are relatively easy to maintain as they can only accept and treat stormwater from a small drainage area less than one acre. However, on a watershed level, a single lot level BMP will only have a limited impact on water quality or quantity. Lot level BMPs should be executed as a regional or a neighborhood wide effort in order to improve stormwater runoff quality in a watershed.

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Lot Level BMPs

4.2.1 Rain Gardens

A rain garden is a depressed area of native vegetation that is designed to capture and hold stormwater. A rain garden is designed to accept runoff from very small areas such as roof tops, driveways, or residential streets. Runoff from surrounding impervious areas should enter the rain garden as sheetflow. Direct discharge from rain spouts and gutters should enter the garden through an energy dissipater device. Individual gardens aid in controlling the volume of runoff from individual lots that would otherwise combine with and contribute to runoff from other properties into the stormwater sewer system. However, to provide an effective contribution to stormwater management, rain gardens must be sufficient in number and common throughout an area (MARC, 2008). Figure 4-1 is an example of a rain garden BMP.

Figure 4-1 Rain Garden at University of Missouri-Kansas City



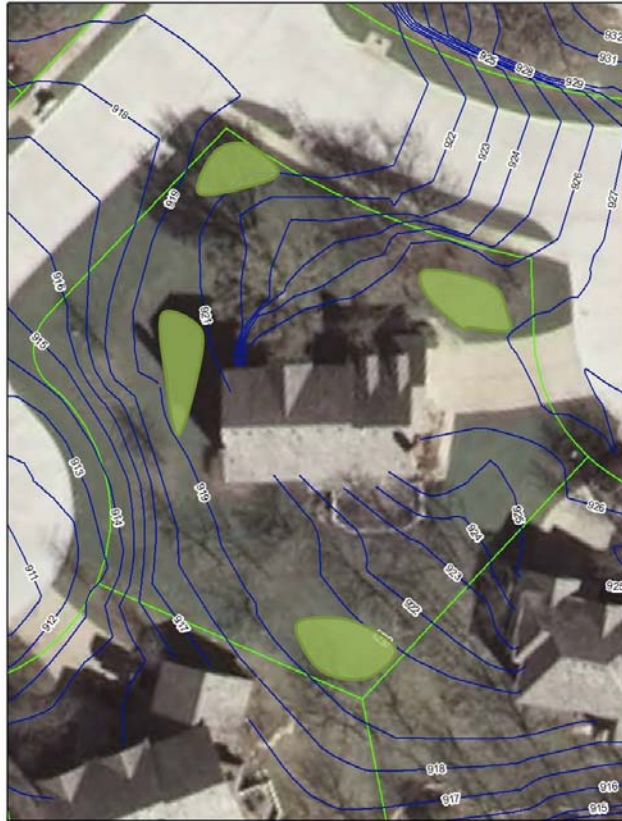
<i>Location characteristics (Slope, Soil Type)</i>	Slope: < 5 percent Soil Type: A, B
<i>Contributing drainage area</i>	< 1 acres
<i>Design size</i>	10 to 20% drainage area
<i>Detention time for WQv treatment</i>	24-48 hours
<i>Pollutant removal efficiencies¹</i>	82-95% TSS, 80-85% TN, 65% TP
<i>Potential for education and outreach</i>	High. Lot level private gardens can be part of your NPDES outreach activities
<i>Potential for use with other BMPs</i>	Moderate. As a downstream infiltration BMP, can be used in treatment train.
<i>Implementation Category</i>	Short Term: Easy Long Term: Difficult (See Section 5.4.1)
<i>Maintenance</i>	High. Sediment/debris removal, vegetation upkeep (See Section 5.4.1)

¹New York State, 2003

4.2.1.1 General Application

Rain gardens can be used to improve the quality of urban/suburban runoff coming from roof tops, driveways, and lawns of residential neighborhoods, small commercial areas, and parking lots. They are typically most effective for catchments less than one acre. Rain gardens work well with other BMPs such as downstream infiltration management practices. Rain gardens should be placed near the source of stormwater runoff, or in a low area of the property where water collects as shown on Figure 4-2. Refrain from placing a rain garden in just any location where water typically pools for long periods as this may indicate low soil infiltration rates (Ellingson, 2008).

Figure 4-2 Example Placement of Rain Gardens on a Residential Lot



4.2.1.2 Design Requirements

Rain gardens require that captured rainfall and runoff be infiltrated below the surface within 24 to 48 hours. Consider more than just the aesthetic and hydrologic benefits of a rain garden; remember that having a natural space will promote wildlife habitat and a connection with nature. Therefore, the critical design requirement is the rate at which water can infiltrate into the soil.

Site Considerations

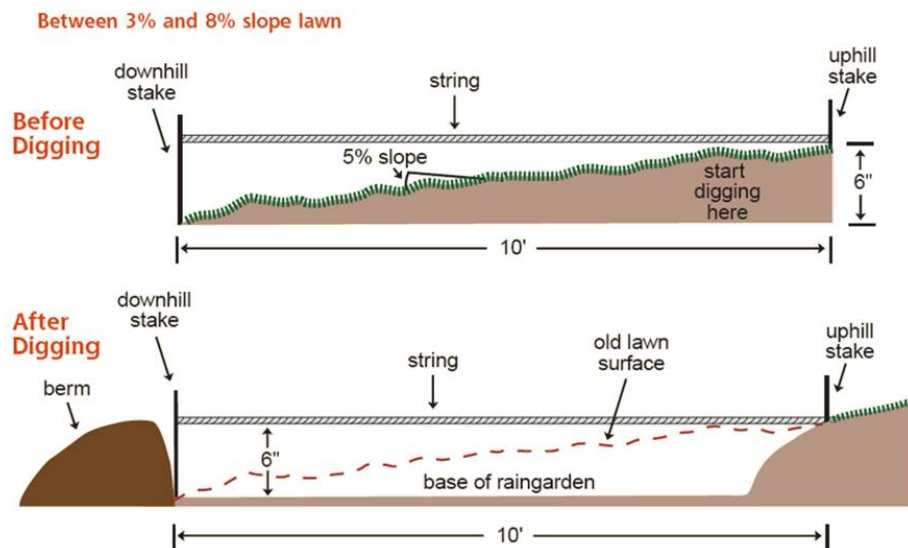
- Rain gardens should be placed in the lowest portion of a yard to ensure that runoff will flow into it. Do not place the garden in an area that typically has ponded water (indicating poor infiltration) or that is not the lowest point. Ponded water in other areas of the yard may indicate soils with low permeabilities.
- Perform a percolation test to determine the infiltration rate of the soil. To perform this test, choose a level ground location. Cut the bottom from a can or other hard-material cylinder and push it 2 to 3 inches into the ground. Fill can with water, measure water level with a ruler, and time how long it takes water to completely drain. Infiltration rate can then be calculated by dividing the measured water level by the total time to drain.

- To build an infiltration garden in an area with low permeability, augment native soil with an engineered soil with a 1:1 ratio of sand to compost mix
- An organic-rich top soil will initiate plant growth and soak up excess runoff
- The rain garden should not be placed in the proximity of a foundation or in any other area where ponded water may create problems

Rain Garden Configuration

- The ponding depth shall be the depth of water that will infiltrate into the soil in 24 hours based on the percolation test results (3 to 6 inches typical). The soil from excavation can be used to create a berm on the side of the rain garden as shown in Figure 4-3.
- The garden shall be sized to treat and accept the WQv and shall have a flat bottom to ensure even infiltration into the soil across the garden.
- Plant selection should include native species that are tolerant of both wet and dry cycles. This will achieve the highest level of success in a rain garden.
- Route stormwater away from the garden initially until vegetation becomes established, typically for a 30 to 60 day timeframe.
- Irrigate as needed during the first 60 days to establish plants.

Figure 4-3 Example of Where to Place Excavated Soil When Building Rain Garden (University of Wisconsin-Extension, 2003)



Vegetation Selection

Utilize native vegetation in the rain garden design. These plants have deep roots that can sustain periods of drought. Determine the following specific for the rain garden site in order to select proper vegetation:

- Soil types (soil tests, soil maps in Appendix B) and organic matter
- Annual precipitation with dates for wet/dry season (Maps in Appendix A)
- Ecoregion and corresponding vegetation (Map and table in Appendix C)
- Previous land use

Provide the soil type, precipitation, previous land use, and ecoregion information to a local nursery or landscaping specialist for planting suggestions (vegetation types, seeding rates, establishment procedures, maintenance procedures). Use the “typical vegetation” listed in Appendix C as a guideline to check final list. Native vegetation contacts and links are listed in Appendix C.

4.2.1.3 Submittal Requirements

For review purposes prior to construction, the following minimum submittal requirements are recommended:

- Drainage area map to rain garden.
- Percolation test results.
- Dimensions of rain garden (L x W x D).
- Plan view. Components clearly labeled with dimensions. Distances from structures and locations of downspouts should be noted.
- Vegetation plan stating typical height of plants along with schedule for installation and initial maintenance.

4.2.1.4 Web-Based Resources

10,000 Raingarden initiative: www.rainkc.com/_ccLib/image/pages/PDF2-66.pdf

Citizen's Guide to Protecting Wilmington's Waterways:
www.wilmingtonnc.gov/Portals/_default/stormwater/cguide.pdf

How to Build Your Own Backyard Rain Garden: www.stormwater.kytc.ky.gov

Native vegetation establishment: www.grownnative.com,
www.kansasnativeplantsociety.org,

www.oznet.ksu.edu/library/crpsl2/MF2291.pdf

Stormwater Management Rain Garden Design for Homeowners:
www.ianrpubs.unl.edu/epublic/live/g1758/build/g1758.pdf

MARC Raingarden Design Brochure:
www.marc.org/environment/Water/bmp_manual.htm

4.2.1.5 References

Ellingson, Sue. 2008. *Sue's rules for raingardens*. Located at
sueellingson.com/raingardens.

MARC and APWA. 2008. *Manual of Best Management Practices for Stormwater Quality*.
Located at www.marc.org/environment/Water/bmp_manual.htm

University of Wisconsin-Extension. 2003. *Rain Gardens: A how-to manual for homeowners*. Located at clean-water.uwex.edu/pubs/raingarden/rgmanual.pdf

New York State. 2003. *New York State Stormwater Design Manual*. Located at
www.westchester.gov.com/planning/environmental/soilwater/reports/altpractices.pdf

Lot Level BMPs

4.2.2 Rain Barrels and Cisterns

Rain barrels and cisterns are storage vessels used to capture rooftop runoff for reuse for landscaping and other non-potable uses. Water collected has various uses, including lawn irrigation, vegetable and flower gardening, and watering houseplants. By diverting water from storm drainage systems, rain barrels and cisterns reduce pollutants and the volume of runoff entering local rivers and streams.

<i>Location characteristics (Slope, Soil Type)</i>	Slope: N/A Soil Type: All
<i>Contributing drainage area</i>	Rooftop drainage
<i>Design size</i>	50-60 gallons (rain barrel) 50-5000 gallons (cistern)
<i>Detention time for WQv treatment</i>	N/A
<i>Pollutant removal efficiencies</i>	N/A
<i>Potential for education and outreach</i>	High. Lot level practices can be part of your NPDES outreach activities
<i>Potential for use with other BMPs</i>	Moderate. Can be used for BMP irrigation during dry periods
<i>Implementation Category</i>	Short Term: Easy Long Term: Easy
<i>Maintenance</i>	Moderate. Keep barrel free of organic material, mesh screens and olive oil will keep mosquitoes from breeding, use stormwater regularly to allow adequate storage room for future rain events

4.2.2.1 Rain Barrels

A rain barrel is typically a 50-60 gallon tank to which downspouts are directed. An example of a rain barrel is shown in Figure 4-4. Roof rainwater collects in these barrels and a drainage valve and/or garden hose is used to distribute water for irrigation in between storm events.

Design and Installation Requirements

- **Components.** 50 to 60 gallon covered plastic tank with an opening at the top for downspout discharge, an overflow outlet, and a valve and hose adapter at the bottom. It is recommended that the barrel have a sealed, child resistant top that can be easily removed for cleaning.
- **Location.** Locate the barrel under downspouts where water can be easily collected for transport away from building foundations.
- **Installation Guidelines.** The base of the rain barrel must be level and secure. Concrete blocks or pavers can be used to achieve this. Downspouts should be cut to allow a three inch gap between the top of the barrel and the end of the downspout, allowing for space to remove the lid and clean the inside of the barrel. Overflow outlets should be routed away from foundations and to pervious areas. Additional

rain barrels will increase the quantity of water stored. Table 4-5 provides the total runoff volume generated based on a roof's square footage and the amount of rainfall.

**Figure 4-4 (left) Rain Barrel Diagram (townofblackmountain.org)
(right) Residential Rain Barrel in River Falls, Wisconsin (rfcity.org)**

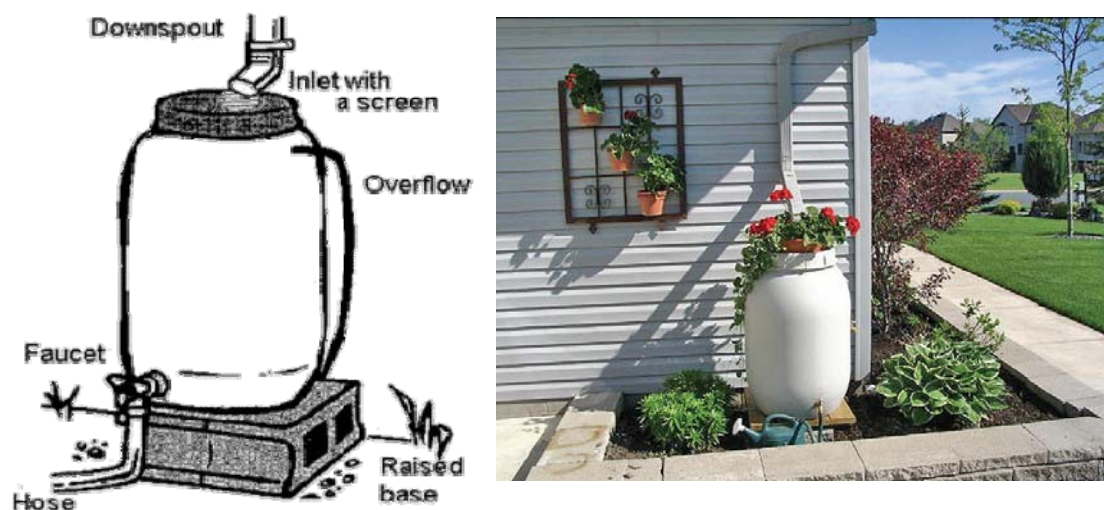


Table 4-5 Total Runoff Volume Generated Based on Roof's Square Footage

		Gallons of Water Produced									
		Rainfall (inches)									
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1
Roof Area (square feet)	100	6	12	18	24	30	36	41	47	53	59
	250	15	30	44	59	74	89	104	118	133	148
	500	30	59	89	118	148	178	207	237	266	296
	750	44	89	133	178	222	266	311	355	400	444
	1000	59	118	178	237	296	355	415	474	533	592
	1250	74	148	222	296	370	444	518	592	666	740
	1500	89	178	266	355	444	533	622	711	799	888
	1750	104	207	311	415	518	622	725	829	933	1036
	2000	118	237	355	474	592	711	829	947	1066	1184

Web Based Resources

Low Impact Development Sustainable School Projects:

www.lowimpactdevelopment.org/school/rainb/rbm.html

Watershed Activities to Encourage Restoration:

www.watershedactivities.com/projects/spring/rainbarl.html

Lake Superior Streams Stormwater Page and Rain Barrel Guidance:

www.lakesuperiorstreams.org/stormwater/toolkit/rainbarrels.html

Town of Black Mountain Rain Barrel Information:

www.townofblackmountain.org/rain_barrel.htm

EPA Fact Sheet: www.epa.gov/region03/p2/what-is-rainbarrel.pdf

MARC Rain Barrel Information:

www.marc.org/Environment/Water/buildrainbarrel.htm

www.mtwatercourse.org/NSP/KSMO_buildarainbarrel.pdf

Rain Barrel Guide: www.rainbarrelguide.com

Where to Purchase Rain barrels

Check with local hardware store.

www.gardeners.com

www.rainbarrelsource.com

www.aridsolutionsinc.com/page/page/522317.htm

www.bayteccontainers.com

4.2.2.2 Cisterns

Cisterns are only distinguishable from rain barrels given their large size, and provide considerably more storage as well as pressurized distribution. One or more downspouts can be connected to a partially or fully buried cistern, storing water for use between rain events. Stored water is distributed using an electric pump. An example of a cistern is shown in Figure 4-5.

**Figure 4-5 Residential Aboveground Cistern
in Portland, Oregon (www.rwh.in)**



Design and Installation Requirements

- **Components.** Variable size tank constructed of an impervious, water retaining material. Includes electric discharge pump, secured access point, piped intake locations, and an overflow point.
- **Location.** Cistern can be located above or below ground. Should be located away from foundations.
- **Installation Guidelines.** Due to the size, complexity, and potential proximity of cisterns to foundations, a structural engineer should be consulted for design and construction.

Web Based Resources

Urban Design Tools: Rain Water Cistern: www.lid-stormwater.net/raincist_construct.htm

Boston Metro Area Planning Council LID Toolkit
www.mapc.org/regional_planning/LID/cisterns_barrels.html

Texas Manual of Rainwater Harvesting:
www.twdb.state.tx.us/publications/reports/RainwaterHarvestingManual_3rdedition.pdf

Lot Level BMPs

4.2.3 Disconnect Impervious Areas

Runoff from connected impervious areas often flows directly to a stormwater collection system with no possibility for infiltration into the soil. The direct runoff from these areas is one of the greatest contributors to nonpoint source pollution. The convergence of runoff from numerous impervious drainage areas combines volumes, runoff rates, and pollutant load. By disconnecting impervious areas, runoff from rooftops, driveways, and parking lots is diverted from a stormwater management system or a curb and gutter system. Water is instead directed to a vegetated area, a bioretention area, or a holding device. Disconnecting impervious areas can potentially reduce runoff volume and filter out pollutants. Figure 4-6 provides an example of green space that runoff could be redirected to.

Figure 4-6 Sidewalk Median in Topeka, KS Provides Pervious Area



4.2.3.1 General Application

Disconnection practices can be applied in almost any area containing impervious surfaces. However, the runoff must be able to discharge to a suitable receiving area, such as a densely vegetated lawn, in order for the BMP to be effective.

4.2.3.2 Design Requirements

Disconnecting impervious areas requires little construction and few materials. Options include rooftop disconnection and installation of curb cuts along existing parking lots or streets.

- Rooftop disconnection requires minimal modifications to downspouts to direct runoff away from collection systems and impervious areas
- Curb cuts may be installed to encourage stormwater flows away from inlets

Figures 4-7 and 4-8 demonstrate typical lot diagrams for disconnecting impervious areas. Figure 4-7 is a typical lot diagram with downspouts indicated by black dots. The orange arrows show flow direction into the grassed lawn and other vegetated areas (adapted from Portland, 2008). Figure 4-8 demonstrates a highly urbanized area where there are potential disconnection locations available adjacent to buildings and other impervious area.

Figure 4-7 Typical Lot Diagram (Adapted From Portland, 2008)

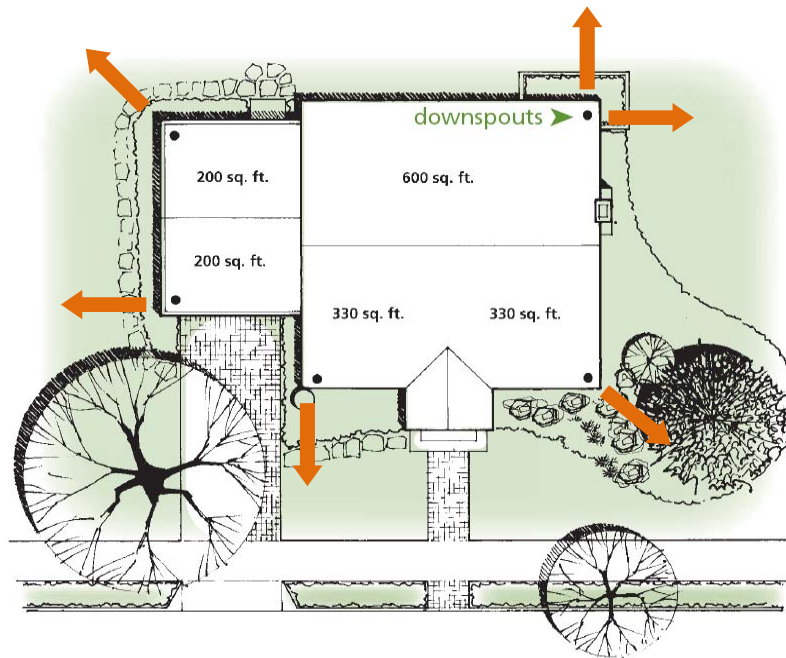


Figure 4-8 Sprint Campus in Overland Park Provides Pervious Area Around Buildings for Downspout Discharge



Section 4 Structural BMPs

4.3 Bioretention

Bioretention utilizes vegetation to accept and treat stormwater runoff through infiltration into layers of plant roots and the growing medium. Reductions in stormwater runoff are achieved via natural plant processes and movement through soil media. Runoff volumes are also decreased by temporary storage in the soil media and permanent removal by evapotranspiration from the vegetation. Bioretention facilities should be designed so that runoff in excess of the water quality volume (WQv) may bypass the facility through an overflow structure. The WQv is the volume of runoff that must be captured to achieve water quality benefits. The WQv is allowed either to infiltrate into the surrounding soil or be collected by an underdrain system that discharges to the storm sewer system. Thus, bioretention facilities can be designed to be on or off-line of existing stormwater systems. Figure 4-9 provides examples of bioretention cells.

Sections from this manual that may need to be referenced for additional information are: Section 2; Section 4.1; Section 5.

<i>Location characteristics (Slope, Soil Type)</i>	Slope: < 10% ¹ Soil Type: A, B, C, D
<i>Contributing drainage area</i>	< 4 acres ¹
<i>Design size</i>	1-15% drainage area Minimum (W x L): 15 ft x 40 ft ¹
<i>Detention time for WQv treatment Pollutant removal efficiencies¹</i>	1-3 days ¹ 40% TN, 65% TP, and 80 to 90% Zn, Cu, Pb reduction ^{2,3}
<i>Potential for education and outreach</i>	High (highly trafficked areas-education, aesthetics)
<i>Potential for use with other BMPs</i>	Works well with upstream source controls and filter strips and swales
<i>Implementation Category</i>	Long term: 15-20 year lifespan based on metal accumulation ⁴
<i>Maintenance</i>	High initially, lower with establishment of BMP (Refer to Section 5.4.1)

¹MARC, 2008, ²Davis et al., 2003, ³Hunt et al., 2006, ⁴Mac, 2005

Figure 4-9 Series of Bioretention Cells on Jackson Street, Topeka, Kansas (Source: GreenTopeka.org)



4.3.1 General Application

Bioretention is a good BMP to be used in urban areas because of the minimal land requirement and thus is usually located in highly trafficked areas. This provides opportunities for BMP public education and signage. Bioretention facilities should be located upland from inlets that receive sheet flow from graded areas or in recessed areas that receive runoff from impervious urban infrastructure. Typical applications include median strips, parking lot islands, and landscaped swales alongside roads. These areas can be designed so that runoff is either diverted directly into the bioretention area or conveyed into the bioretention area by a curb and gutter collection system (EPA, 1999, UDFCD, 2008). To maximize treatment effectiveness, the drainage area must be graded in such a way that minimizes erosive conditions as sheet flow is conveyed to the treatment area. To effectively minimize sediment loading in the treatment area, bioretention should only be used where all upstream tributary area is stabilized (EPA, 1999, UDFCD, 2008). Bioretention cells will not function correctly in an area under construction or with exposed soil, as inundation with suspended sediment will prevent infiltration from occurring in the bioretention cells (MARC, 2008).

4.3.2 Advantages and Disadvantages

Advantages	Disadvantages
High volume reduction (+/- 90-percent)	Easily clogged with suspended sediment
40-percent TN, 65-percent TP, and 80 to 90-percent Zn, Cu, Pb reduction ^{1,2}	Higher construction costs per impervious acre ⁴
Aesthetic and educational opportunities in high traffic areas	Cannot be used in areas with a high water table
Intercepts water near source, alleviating need for stormwater infrastructure elsewhere	Cannot be used in drainage areas with slopes > 20-percent ³
Effective in a "treatment train" with BMPs that reduce sediment loads	May not effectively remove pollutants when first brought on-line
Minimal footprint (1-15-percent of drainage area)	
Function increases with time	
May contribute to groundwater recharge	

¹Davis et al. (2003), ²Hunt et al. (2006), ³EPA, 1999

4.3.3 Design Requirements and Considerations

The procedure for designing a bioretention cell is outlined below. The design components are described in the order of construction starting with the underdrain and continuing through bioretention media, planting soil, vegetation, ponding area, and overflow system.

4.3.3.1 Overall Design Guidance

- Bioretention facilities shall not be constructed until all tributary areas are permanently stabilized against erosion and sedimentation or a pre-treatment practice is implemented. Heavy sediment loads to the cell will reduce infiltration rates and require reconstruction of the cell to restore its defined performance.
- The bioretention facility shall be designed to capture the WQv. The WQv should filter through the facility's planting soil bed in 1 to 3 days.
- The bottom area should be sized such that standing water is present less than 24 hours.
- Any facilities wider than 20 feet shall be twice as long as they are wide (UDFCD, 2005).
- The tributary area for a bioretention area shall be less than 4 acres. Multiple bioretention areas may be required for larger tributary areas (EPA, 1999).

4.3.3.2 Excavation

Excavation is almost always required to meet the design requirements except in an area with soils with high permeability with no underdrain. The bioretention facility can be excavated before final stabilization of the tributary area and utilized for erosion and sediment purposes, such as a sediment basin; however, the bioretention soil mixture and underdrain system shall not be placed until the entire tributary area has been stabilized. Bioretention facility side slopes shall be excavated at 4:1 or flatter. Low ground-contact pressure equipment, such as excavators and backhoes, is preferred on bioretention facilities to minimize disturbance to established areas around the perimeter of the cell. No heavy equipment shall operate within the perimeter of a bioretention facility during underdrain placement, backfilling, planting, or mulching of the facility

4.3.3.3 Underdrain/Outlet

The underdrain/outlet is always required for bioretention cells in highly urbanized areas or in soils with a low permeability where excess overflow may be a concern. An underdrain structure allows operators to control the stormwater detention time and allows detained runoff to be released into an existing storm sewer system. The underdrain also increases airflow into the soil media keeping it aerobic. Figure 4-10 shows a side view of the underdrain configuration.

Figure 4-10 Underdrain Configuration Side View
(Source: MARC, 2008)

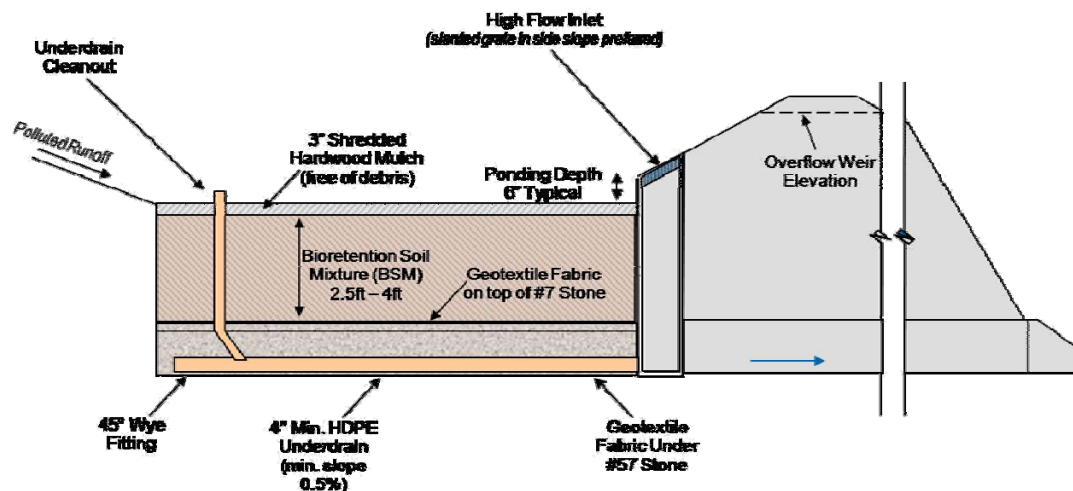
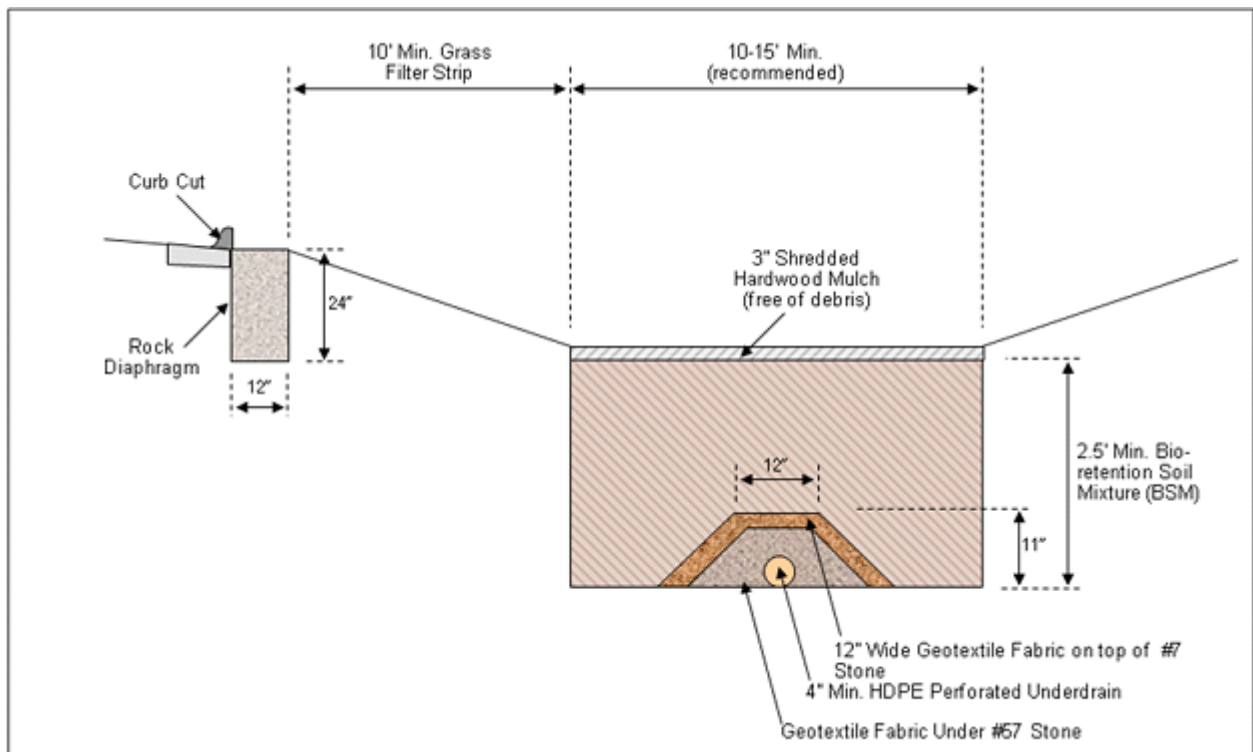


Figure 4-11 provides an example of a bioretention underdrain. Key components of an underdrain/outlet for a bioretention cell include:

- Four-inch or larger perforated pipe with perforations between 0.25-0.375 inches spaced at 6-inch centers with a minimum of 4 holes per row.

- The minimum grade of the underdrain must be 0.5-percent with one cleanout run every fifty feet.
- A valve/cap system at the end of the underdrain allows operator to plug the system and increase the detention time.
- The underdrain shall be covered with 8-inch coarse rock in a trapezoid shape. Filter fabric shall be on the top of the trapezoid only.

Figure 4-11 Bioretention Underdrain Example



4.3.3.4 High Flow Structures

An overflow system is crucial in commercial and industrial settings to ensure that the stormwater does not back up onto surrounding parking lots and public areas. Having a high flow structure also reduces the possibility of hydraulic overload on the bioretention area. If the bioretention facility will be utilized with existing stormwater management systems, the overflow should be connected to this system. An example of an overflow device is shown in Figure 4-12.

**Figure 4-12 Mize Lake, Lenexa, Kansas
Bioretention High Flow Structure**



Source: CDM

4.3.3.5 Bioretention Soil Mixture (BSM)

It is recommended that bioretention facilities utilize native soil with an organic-rich top soil. The bioretention soil mixture must meet the BSM specification in Appendix B.4 (MARC, 2008). The soil must have the appropriate chemical and physical properties to support a diverse microbial and plant community.

The depth of BSM shall be sized to hold the Water Quality volume. The minimum depth shall be 2.5 feet.

4.3.3.6 Ponding Area

The aboveground storage of runoff must drain within 24 hours, but the ponding depth should be minimized to reduce the hydraulic load on soils. Ponding depths should range from 6 to 12 inches.

4.3.3.7 Flow Entrance

Typically, bioretention areas are constructed in space-limited urban settings like parking lots and medians. However, care must be taken to ensure that all runoff entering the bioretention area is in sheet-flow. Runoff must be evenly distributed in order to minimize erosion and loss of vegetation. If curb cuts, cut parking blocks, or other concentrated flow generators are adjacent to the cell, energy dissipation is necessary. The designer should show in design calculations that flow is unconcentrated prior to entering the bioretention cell. An example of where flow enters a bioretention cell is shown in Figure 4-13.

Figure 4-13 Vegetated Swale Guides Runoff From Surrounding Parking Lots Into Bioretention Cell Kansas City, MO (Source: CDM)



4.3.3.8 Vegetation

Native tall-grass prairie plant species are believed to improve soil physical and chemical processes in a Midwestern bioretention cell. Tall-grass species are associated with exceptionally productive soil systems and have extremely dense root structure. Native grasses can withstand the climatic variability typical throughout Kansas. Guidelines for using native vegetation are outlined in Section 5.

4.3.4 Design Calculations

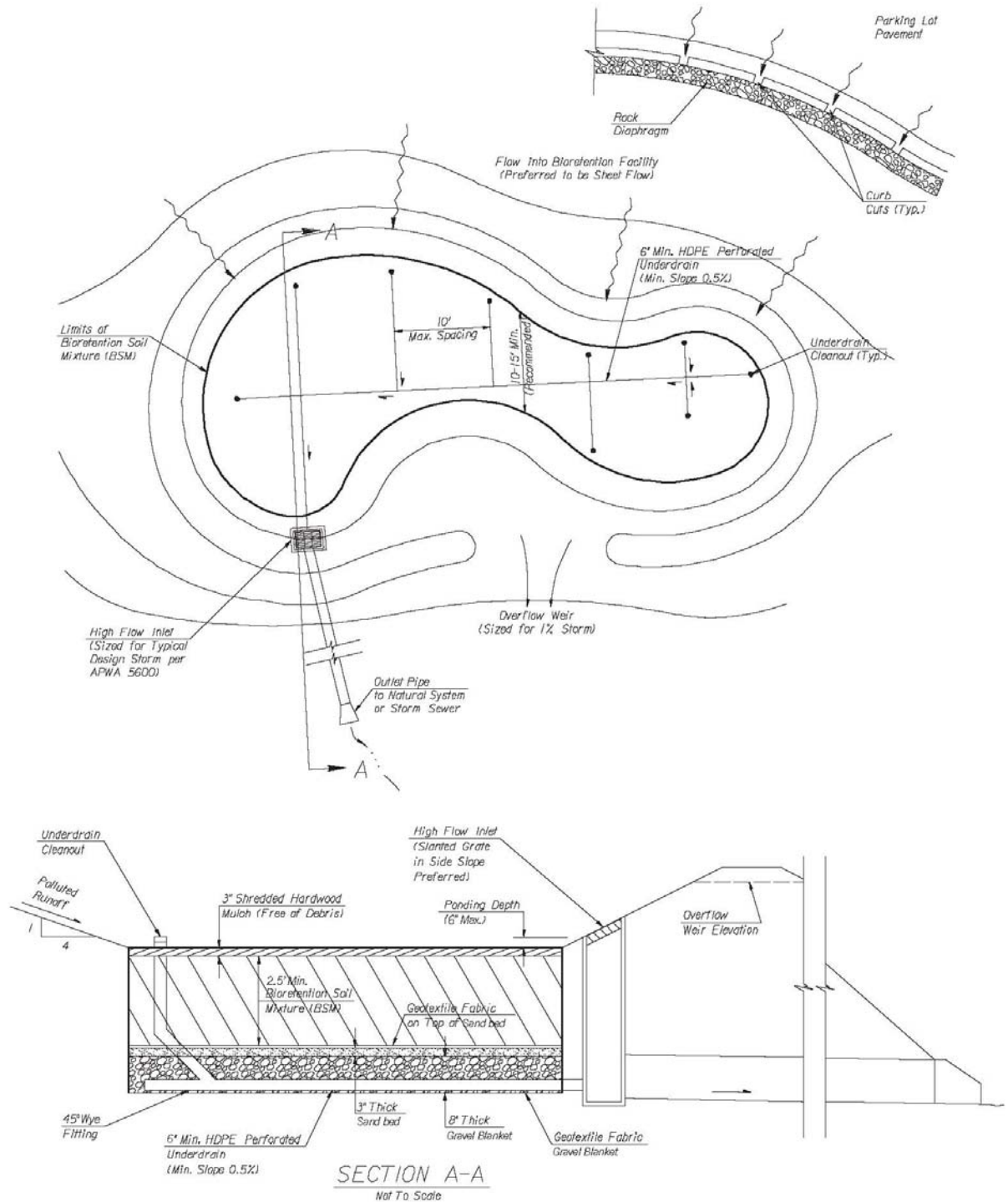
A short summary of the design calculations is presented below. A detailed design example is outlined in 4.3.5. A typical bioretention plan and profile is shown in Figure 4-14.

- **Step 1** Determine WQ_v based on drainage area and regional precipitation information according to Equation 4. 1 and 4.2.

$$\text{Equation 4.1} \quad R_v = 0.05 + 0.009(I)$$

$$\text{Equation 4.2} \quad WQ_v = \frac{P_{wQ} \times R_v \times A_T}{12 \text{ (in)}}$$

Figure 4-14 Bioretention Plan and Profile
Source: MARC, 2008



- **Step 2** Design a pretreatment entity to slow runoff and retain sediments, such as a swale or filter strip.
- **Step 3** Size the bioretention soil bed and planting area based on WQ_V and soil characteristics according to Equation 4.10 and 4.11. Equation 4.11 is valid to calculate a bioretention cell length based on the recommended 2:1 length to width ratio.
- **Step 4** Design the underdrain for connection to existing stormwater infrastructure or to drain soils with low permeabilities. Find the number of transverse collector pipes using equation 4.12.

Equation 4.10 Filter Bed Surface Area

$$A_F = \frac{WQ_V \times d_f}{k \times t_f \times (h_{avg} + d_f)}$$

Where:

A_F	=	Filter bed surface area (acres)
WQ_V	=	Water quality volume (acre feet)
k	=	Coefficient of soil permeability (feet/day)
t_f	=	Time required for WQ_V to filter through soil (days)
h_{avg}	=	Average ponding depth above plant in soil bed (feet)
d_f	=	Planting soil bed depth (feet)

Equation 4.11 Filter Bed Length (Assuming L:W = 2:1)

$$L_f (ft) = \sqrt{87120 \times A_f}$$

Where:

L_F	=	Filter bed length (feet)
A_F	=	Filter bed surface area (acres)

Equation 4.12 Number of Transverse Collector Pipes

$$N_{TU} = \frac{L_f}{S_{TU}}$$

Where:

N_{TU}	=	Number of transverse collector pipes
L_F	=	Filter bed length (feet)
S_{TU}	=	Transverse collector pipe spacing (inches)

- **Step 5** Install appropriate vegetation using methodology provided by local native vegetation experts. Provide an overflow to maintain vegetation integrity during high flow.

4.3.5 Design Example

Design a bioretention area for a small parking lot median of a local grocery store in Arkansas City, KS. The median will drain a 0.5 acre parking lot and 1 acre of roof runoff with a total of 99-percent imperviousness. The parking lot is graded to drain to the bioretention cell. The parking lot is located in southeast Arkansas City with type C soils.

4.3.5.1 Basin Water Quality Volume

Determine the tributary drainage area to the bioretention area (A_T)

The tributary area, A_T , is 1.5 acres. Due to the fact that $A_T = 1.5$ acres and the percentage imperviousness is known, we shall utilize the Short-Cut Hydrology Method.

Calculate the R_v based on equation 4.1

The tributary area is 99-percent impervious. Thus, $R_v = 0.05 + 0.009(99) = 0.941$

Calculate the WQ_v based on equation 4.2

For Arkansas City, KS, the water quality event is 1 inch.

Thus, $WQ_v = (1 \times 0.941 \times 1.5) / 12 = 0.12$ ac-ft

4.3.5.2 Pretreatment

Runoff that flows directly from an impervious area is likely to concentrate and cause erosion in the bioretention area. Thus, a pretreatment device is strongly suggested. Vegetated filter strips and vegetated swales work to reduce the velocity of runoff and promote settling of suspended sediments. In situations where area is limited, utilize underground proprietary devices to detain and slow runoff (MARC, 2008).

4.3.5.3 Planting Soil Bed and Ponding Area

Choose planting soil bed depth (d_f)

The planting soil bed depth is a design decision. Typical depths are from 3-5 feet. For this example, $d_f = 4$ feet.

Soil permeability (k)

An soil matrix (Appendix B.4) was utilized since the existing soil types are of the hydrologic group C with lower than average permeabilities. The soil matrix used has a permeability of 1 foot per day.

Maximum ponding depth (h_{max})

Ponding depths should range from 6 to 12 inches. To maximize infiltration and reduce the hydraulic load on soils, we will design for a conservative 6 inch ponding depth.

The value of h_{max} , should be in feet. Thus, $h_{max} = 0.5$ feet.

Average height of water above bioretention bed (h_{avg})

The average height of water above the bioretention bed is defined as half the ponding depth. $h_{avg} = h_{max} / 2 = 0.25$ feet

Filtration time (t_f)

Ideally, it should take three days for the WQV to filter through the planting soil bed. In this example, $t_f = 3$ days.

Filter bed surface area (A_f)

The required filter bed surface area is calculated using equation 4.10.

For this example, $A_f = (0.12 \text{ ac-ft} \cdot 4 \text{ ft}) / ((1 \text{ ft d}^{-1}) \cdot 3 \text{ d} \cdot (0.25 \text{ ft} + 4 \text{ ft})) = 0.04 \text{ acres}$.

Filter bed length (L_f)

At a minimum, the facility should be 40 feet long. Use equation 4.11 to determine the appropriate length.

For this example, $L_f = (87120 \text{ ft}^2 \text{ ac}^{-1} \cdot 0.04 \text{ ac})^{1/2} = 57 \text{ feet}$.

Filter bed width (W_f)

At a minimum, the facility should be 15 feet wide or approximately half the filter bed length. $W \text{ (feet)} = L \text{ (feet)} / 2 = 57 / 2 = 28.5 \text{ feet}$.

4.3.5.4 Underdrain**Pipe diameter (D_u)**

The underdrain pipe diameter should be at least 4 inches to prevent clogging. For this example, we will utilize the 4 inch diameter pipe.

Gravel depth (Z_g)

The depth of the gravel layer above the underdrain pipe should be at least 4 inches greater than the pipe diameter. Thus, the minimum depth for this example should be 8 inches.

Perforation diameter (D_p)

The recommended perforation diameter is 0.375 inches. We will use this recommendation for this example.

Perforation spacing (S_p)

The recommended longitudinal center to center perforation spacing is 6 inches. We will use this recommendation for this example.

Perforations per row (n_p)

A minimum of 4 perforations per row is recommended. We will use the minimum for this example.

Transverse collector pipe spacing (S_{tu})

When the facility width is greater than 20 feet, it will be necessary to install transverse collector pipes that run perpendicular to and connect to the main underdrain pipe. The center to center spacing of the transverse collector pipes should be less than or equal to 10 feet. For this example, we will choose a spacing of 10 feet.

Number of transverse collector pipes (N_{TU})

The number of transverse collector pipes is found using equation 4.12.

For this example, $N_{TU} = (57/10) = 5.7$. We will use 5 collector pipes.

Overall guidelines

Ensure that the slope for all underdrain pipes (G_{pipe}) is less than 0.5-percent and that one cleanout is provided at the end of each pipe run.

4.3.5.5 Overflow

If the 1-percent event is to pass through the facility, the maximum velocity shall be kept below 3 feet per second to avoid erosion of the soil matrix.

If facilities are designed with a bypass, it shall be designed to safely pass runoff flows from events up to and including the 1 percent event.

The overflow can be designed as a vegetated or stabilized channel or a yard inlet catch basin. Vegetated or stabilized channel overflows shall be designed using Manning's equation or a standard-step backwater method using the energy equation, as appropriate. Overflows designed as open channels shall conform to local agency design criteria for open channels. Overflow inlets shall conform to local agency design criteria for inlet design.

4.3.5.6 Vegetation

Determine the following specific for the bioretention site:

- Soil types (soil tests, soil maps in Appendix B)
- Annual precipitation with dates for wet/dry season (Maps in Appendix A)
- Ecoregion and corresponding vegetation (Map and table in Appendix C)
- Previous land use

Provide the soil type, precipitation, previous land use, and ecoregion information to a native vegetation expert for planting suggestions (vegetation types, seeding rates, establishment procedures, maintenance procedures). Use the "typical vegetation" listed in Appendix C as a guideline to check final list. Native vegetation contacts and links are listed in Appendix C.

4.3.6 Submittal Requirements

Figure 4-13 provides an example of a bioretention plan and profile. For review purposes prior to construction, the following minimum submittal requirements are recommended:

- Drainage area map, including drainage area to bioretention cell(s).

- Existing and proposed contour map of site (1-foot contours recommended). Additional spot elevations may be helpful.
- Geotechnical investigation of site (soil borings, water table location).
- In situ infiltration test of bioretention soil mixture demonstrating infiltration rate of 1 foot/day or higher.
- Stormwater plan/profile for site.
- Bioretention cell plan view and profile view. Components clearly labeled with dimensions.
- Hydrologic calculations (refer to Design Example). The designer should include necessary design calculations to show that flow is unconcentrated prior to entering the bioretention cell.
- Detail of any proposed underdrain and/or overflow structures with dimensions for construction. Include appropriate design calculations (refer to Design Example).
- Vegetation plan with schedule for installation and initial maintenance. Appropriate erosion control measures should be included.
- An as-built survey of the bioretention cell is recommended to confirm actual construction adheres to approved construction plans.
- Long-term inspection/maintenance plan.

4.3.7 References

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Section 4 Structural BMPs

4.4 Vegetated Swales

Vegetated swales are open vegetated channels with dense vegetation covering the side slopes and channel bottom. They are used to treat and convey stormwater runoff at a non-erosive velocity and can be used as a substitute for traditional pipe systems to convey roadway, parking lot and other site drainage (MARC, 2008). The vegetation covering the sides and bottom of the channel provide a filtration surface and slows runoff velocities, traps particulate pollutants, and promotes infiltration. Figure 4-15 is a photo of a grass swale located near a roadway.

Sections from this manual that may need to be referenced for additional information are: Section 2; Section 4.1; Section 5.

<i>Location characteristics (Slope, Soil Type)</i>	Slope: < 1-2% Soil Type: All
<i>Contributing drainage area</i>	< 5 acres
<i>Design size</i>	Varies
<i>Detention time for WQv treatment</i>	N/A
<i>Pollutant removal efficiencies¹</i>	60-85% TSS, 15-90% TP, 10-90% TN, 69-88% Zn, Cu 45-80%
<i>Potential for education and outreach</i>	Moderate (recreation, landscaping, wildlife habitat)
<i>Potential for use with other BMPs</i>	High Best when used as pretreatment for other BMPs such as bioretention
<i>Implementation Category</i>	Short Term: Easy Long Term: Easy
<i>Maintenance</i>	Low Sediment/debris removal, vegetation upkeep

¹CRWA, 2008

4.4.1 General Application

Grass swales are well suited for treating highway and residential road runoff and can serve as a drainage system to replace curb and gutter storm sewer systems (CASQA, 2003). Vegetated swales are best utilized in treating areas of 5 acres or less, and are only effective in conveying shallow concentrated flow for water quality benefits. Swales are especially effective when used with a series of stormwater BMP practices, such as when receiving water from a filter strip, or conveying water to a detention pond (See treatment train in Section 2).

Figure 4-15 Grass Swale Located Near a Roadway
(Source: US Army Corps)



4.4.2 Advantages and Disadvantages

Advantages	Disadvantages
Improves water quality by filtering stormwater through dense vegetation.	Provides effective water quality control in light to moderate runoff conditions, but control during large storms is limited
Generally less expensive construction costs than underground pipes	Requires a large area for highly developed sites with large amounts of impervious area
Conveys peak discharge and slows down runoff to surrounding streams and rivers	Is not effective in reducing bacteria levels in stormwater
Minimizes erosion when used with recommended slope requirements (see Section 4.3.4)	Require more maintenance than curb and gutter systems

4.4.3 Design Requirements and Considerations

4.4.3.1 General Guidelines

The main criteria to consider in the water quality design of a vegetated swale are channel capacity in relation to residence time and minimization of erosion (IA State, 2008):

- Runoff velocity shall not exceed 1 foot per second (fps) during the peak discharge associated with the water quality design rainfall event.
- The total length of the swale should provide at least 3 to 5 minutes residence time, with a minimum length of 100 feet.

4.4.3.2 Site Location and Soils

- Grass swales shall be used to treat drainage areas of less than 5 acres.
- The bottom of the channel shall be constructed at least three feet above groundwater to prevent the bottom from remaining moist or contamination of groundwater (Metro Council, 2001).
- In order to provide the best means for plant survival, vegetated swales cannot be constructed in gravelly and coarse sandy soils (MARC, 2008).
- Select vegetation that can withstand relatively high-velocity flows at entrances, and both wet and dry periods (MARC, 2008, Metro Council, 2001). Vegetation should achieve a minimum 70-percent density prior to putting the swale into service.
- Soil stabilization methods such as mulch, blankets or mats should be used prior to the establishment of vegetation (MARC, 2008).

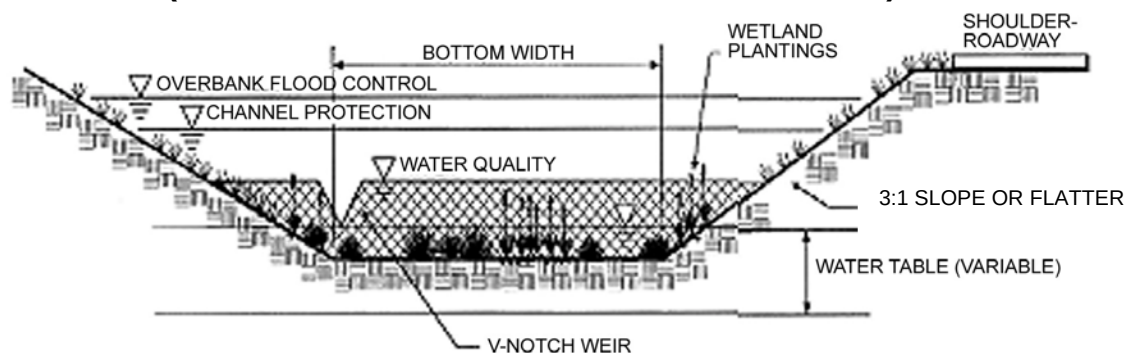
4.4.3.3 Slope, Shape, and Design

- It is recommended that swales be designed on longitudinal slopes of 1 to 2-percent. Channel slopes greater than 4-percent should not be permitted (IA State, 2008). Installation of check dams is recommended for slopes above 2-percent.
- The side slopes of the channel should be as flat as possible to aid in filtration of incoming flows. A maximum slope of 3:1 is recommended; a 4:1 slope is encouraged where space permits (MARC, 2008).
- Swales shall be parabolic or trapezoidal in shape (IA State, 2008; MARC, 2008; Metro Council, 2001). The trapezoidal shape is the easiest to construct and is a more efficient hydraulic configuration. The criteria presented in this section assume a trapezoidal cross-section; the same design principles will govern parabolic cross-sections, except for the cross-sectional geometry (IA State, 2008). Figure 4-16 shows a cross-section of a swale.
 - Size the bottom width between two and eight feet. Larger bottom widths may be used if separated by a dividing berm.
 - The bottom width is a dependent variable in the calculation of velocity based on Manning's equation (Iowa Stormwater Management Manual, 2008).

- Generally, swale length is a function of site drainage constraints (IA State, 2008). The minimum longitudinal length of a vegetated swale should be 100 feet to provide adequate water quality treatment (MARC, 2008).
- Identify the swale bottom width, depth, length and slope necessary to convey the water quality flow rate with a shallow ponding depth. The depth should relate to the height of the vegetation used in the swale, as increased water depth would provide conveyance rather than residency time needed for the water quality storm. This depth typically ranges from 1 to 4 inches.
- The Manning's roughness coefficient used to calculate width, depth and length of the swale for the water quality event should be based on sheet flow. If additional capacity is required in the swale for the conveyance of a defined design event (e.g. 10-year storm event), the Manning's roughness coefficient should be modified based on shallow concentrated flow. Typical Manning's roughness coefficients for sheet flow are:

	Manning's Roughness Coefficient "n" for Sheet flow
Short grass prairie	0.15
Dense grasses (weeping lovegrass, bluegrass, buffalo grass, blue grama grass, and native grass mixtures)	0.24
Bermuda grass	0.41

Figure 4-16 Example of a Swale Cross Section
(Source: Center for Watershed Protection, 2001)



4.4.4 Design Calculations

- **Step 1:** Find flow (Q) for tributary area to swale for water quality rainfall event using Rational Method.

$$\text{Equation 4.6 } Q = C \times i \times A$$

- **Step 2:** Solve Manning's equation for a specified variable. For this example, we will calculate bottom width of the swale. This step is most easily accomplished using a spreadsheet or solver program.
- **Step 3:** Solve $V = Q/A$ for velocity using calculated variable and Q calculated in Step 1. If V is greater than 1 ft/s, the width of channel, longitudinal slope of channel, or Manning's n value may need to be adjusted to obtain a velocity less than 1 fps, and therefore appropriate for shallow flow.
- **Step 4:** Calculate minimum swale length for required residency time using $L = VT$ where T is equal to minimum residency time. If the length calculated is less than 100 feet, a minimum length of 100 feet must be specified on construction plans.
- Note that an agency may require that a swale also be designed for conveyance of a defined design storm (e.g. 10-year storm event). The calculations presented in this manual are only applicable to design of a swale for a water quality rainfall event. Additional calculations may be necessary to size the swale for other larger events.

4.4.5 Design Example

A 5 acre site is being developed by a church ($C=0.75$) in Hutchinson. 0.25 acres of the site will be tributary to a proposed buffalo grass swale, with a Manning's n value of 0.25 and side slopes at 4:1. Assume a time of concentration of 10 minutes to the swale. Assume flow depth in the swale of 2 inches for the water quality event. Proposed longitudinal slope is 2.0-percent. Residency time required for stormwater in swale is a minimum of 5 minutes. Design the swale for the water quality rainfall event.

Step 1: Calculate the water quality rainfall event Q (assume 90-percent) using the Rational Method.

- $Q = (0.75) \times (1.47 \text{ in/hr}) \times (0.25 \text{ acre}) = 0.28 \text{ cfs}$

Step 2: Using Microsoft Excel solver, a bottom width was calculated using Manning's equation based on the Water Quality Storm Q.

Trapezoidal (4:1) Example Problem							
n	Depth (D) feet	Width (W) feet	Area (A) sqft	Wetted P (ft)	Hydraulic radius (ft)	Long Slope (ft/ft)	Iterated Q
0.25	0.166666667	6.350092724	1.17	7.72	0.15	0.020	0.28

This width was calculated as 6.35 feet. A width of 6.50 feet will be used.

Trapezoidal (4:1) Example Problem							
n	Depth (D) feet	Width (W) feet	Area (A) sqft	Wetted P (ft)	Hydraulic radius (ft)	Long Slope (ft/ft)	Iterated Q
0.25	0.166666667	6.5	1.19	7.87	0.15	0.020	0.29

Step 3: Calculate Velocity.

- $V = (0.28 \text{ cfs}) / (1.19 \text{ sq ft}) = 0.24 \text{ ft/s}$. This is less than 1 ft/s, and therefore meets the recommendations for the Water Quality Storm.

Step 4: Calculate minimum length of swale based on residence time.

- $L = (0.24 \text{ ft/s}) * (5 \text{ min}) * (60 \text{ sec/min}) = 70.6 \text{ feet}$. This is less than 100 feet, so $L = 100 \text{ feet}$.

Summary: To meet design requirements and recommendations for the Water Quality Storm and the site, a vegetated swale shall be constructed that is 100 feet in length and with a bottom width of 6.5 feet.

4.4.6 Submittal Requirements

For review purposes prior to construction, the following minimum submittal requirements are recommended:

- Drainage area map, including drainage area to swale.
- Existing and proposed contour map of site (1-foot contours recommended).
Compaction requirements should be stated, if required. Additional spot elevations may be helpful.
- Geotechnical investigation of site (soil borings, water table location).
- Stormwater plan/profile for site.
- Swale calculations, including WQv, depth of WQv in swale, and maximum velocity for WQv (refer to Design Example). A visual representation of the cross-section of the swale to be constructed should be provided, including bottom width and side slopes.
- Vegetation plan with schedule for installation and initial maintenance. Appropriate erosion control measures should be included.
- An as-built survey of the swale is recommended to confirm construction adheres to approved construction plans.
- Long-term inspection/maintenance plan.

4.4.7 References

CASQA. 2003. *California Stormwater Quality Association Stormwater Best Management Practice Handbook*. Available at www.dot.ca.gov/hq/construc/stormwater/manuals.htm

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Section 4

Structural BMPs

4.5 Filter Strips

A filter strip is an area of planted or indigenous dense vegetation that accepts sheet flow runoff from adjacent surfaces. When situated properly between a pollution source and a water body that receives runoff, filter strips slow runoff velocities and improve water quality. Filter strips improve water quality by reducing sediment load and filtering pollutants absorbed to sediments. Water treatment with filter strips is most effective when sheet flow is maintained. Runoff from adjacent impervious surfaces will often concentrate and form a channel, reducing the effectiveness of the filter strip (Muthukrishnan et al. 2006). These flows must be converted to sheet flow prior to entering a filter strip treatment area. In order to achieve this, grading and level spreaders are often necessary to create a uniformly sloping area to distribute the runoff evenly across the filter strip (IA State, 2008). Figure 4-17 provides an example of filter strips.

Sections from this manual that may need to be referenced for additional information are: Section 2; Section 5.

<i>Location characteristics (Slope, Soil Type)</i>	Slope: < 1-6% Soil Type: All
<i>Contributing drainage area</i>	< 2 acres
<i>Design size</i>	Minimum: L 15'
<i>Detention time for WQv treatment</i>	N/A
<i>Pollutant removal efficiencies¹</i>	90% TSS ¹ , 20% TN, 20% TP, 40% Heavy Metals ²
<i>Potential for education and outreach</i>	High (recreation, landscaping, wildlife habitat)
<i>Potential for use with other BMPs</i>	Best when used as pretreatment for other BMPs such as bioretention
<i>Implementation Category</i>	Short Term: Easy Long Term: Easy (See Section 5.4.1)
<i>Maintenance</i>	Low Sediment/debris removal, vegetation upkeep (See Section 5.4.1)

¹Gharabaghi et al., 2000, ²IAState, 2008

Figure 4-17 Filter Strip



4.5.1 General Application

A filter strip can be used to improve runoff quality by filtering stormwater runoff through dense vegetation. In rural settings, filter strips are most often utilized as an agricultural BMP to filter runoff from farm fields. In urban settings, filter strips are best utilized in treating runoff from roads and highways, roof downspouts, and small parking lots (USEPA, 2006). Filter strips are frequently used as a pretreatment system for stormwater destined for other BMPs such as an infiltration trench or bioretention systems (Metro Council, 2001). See Section 2 for information on BMPs in treatment trains.

4.5.2 Advantages and Disadvantages

Advantages	Disadvantages
Relatively easy and inexpensive to implement	Most effective when implemented with other BMPs (treatment train)
When implemented early in the development cycle can be used as erosion and sediment control	Applications of fertilizers, herbicides, and pesticides on FS may be a source of pollutants in runoff
Substantial capture of sediment and pollutants are adsorbed onto particles	Potential failure when concentrated flows with erosive velocities develop and “short circuit” the filter strip.

4.5.3 Design Requirements and Considerations

The following guidelines shall be considered when designing filter strips:

4.5.3.1 General Guidelines

- Filter strips shall be designed to accept sheet flow runoff from small drainage areas (1 to 2 acres). Concentrated flows must be redistributed or unconcentrated prior to entering the filter strip (Metro Council, 2001).
- Where applicable, vegetated filter strips should be utilized as a pre-treatment component for structural BMPs such as bioretention areas.
- Sheet flow runoff from paved surfaces shall be limited to maximum lengths shown in Table 4-6.
- Filter strips constructed in parking lots require special design attention to the spacing of parking blocks in order to maintain sheet flow. In these cases, the designer shall specify spacing between individual parking blocks as well as spacing between parking blocks and the beginning of the filter strip. A typical parking space width ranges from 8 to 10 feet, with typical parking block widths ranging from 6 to 8 feet. Parking blocks should be spaced to allow a minimum of 2 feet width between them. Where parking blocks are used, a minimum additional 2 feet of surface beyond the parking block is recommended for flow to unconcentrate prior to entering the filter strip. The additional surface required will vary based on the parking lot slope toward the filter strip.
- Curbs and curb cuts are not permitted adjacent to a filter strip.

4.5.3.2 Site Location and Soils

- Filter strips shall be positioned at least two feet above the water table. Filter strips should be separated from the groundwater by between two and four feet to prevent contamination (Muthukrishnan et al. 2001).
- Filter strips shall be located in an area where they will not remain wet between storms.
- Filter strips should not be used on soils that cannot sustain a dense grass cover with high retardance (IA State, 2008).
- Designers shall choose grasses that can withstand relatively high-flow velocities, and both wet and dry periods. Use of vegetation appropriate for the local climate is essential for plant survival.
- Allow vegetation used in the filter strip to reach a 70% density of the ground cover prior to making it part of the site's stormwater management program.

4.5.3.3 Slope

- Filter strip slopes shall be designed no less than 1 percent, but not greater than 6 percent. Greater slopes would encourage the formation of concentrated flow, and lesser slopes may result in standing water.
- An effective flow spreader is to use a pea gravel diaphragm (small trench) at the top of the slope. This trench will act as a pretreatment device and as a level spreader (IA State, 2008).
- Both the top and the toe of the slope should be as flat as possible to encourage sheet flow and prevent erosion (Muthukrishnan et al. 2001).
- A berm of sand and gravel can be designed at the toe of the slope to provide an area for temporary shallow ponding. This berm could include outlet pipes or an outflow weir.

4.5.3.4 Shape and Design

- The maximum length of pavement in the direction of flow draining to a filter strip can be determined using pavement slope and rainfall intensity, based on the 10-year storm. Refer to Table 4-6 for guidelines in determining pavement length.
- Filter strip length in the direction of flow shall be determined based on the slope of the filter strip and water quality event rainfall intensity, using the time of concentration for the drainage area to the filter strip. Refer to Table 4-7 for guidelines in determining filter strip length.
- The filter strip should stretch the entire length of the adjoining impervious surface where the stormwater originates (Muthukrishnan et al. 2001).
- Filter strips must be a minimum of 15 feet in length in the direction of flow to effectively treat run-off, greater lengths will enhance treatment (IA State, 2008).

4.5.4 Design Calculations

- **Step 1:** Calculate the time of concentration of the area draining to the filter strip using equation 4.8. This value should a minimum of 5 minutes.

Equation 4.8

$$T_I = \frac{1.8(1.1 - C)D^{1/2}}{S^{1/3}}$$

- **Step 2:** Find the 10-year rainfall intensity at the duration equal to the time of concentration using Appendix A.
- **Step 3:** Use Table 4-6 to find the maximum pavement length (PL_{max}) that can drain to the filter strip, based on intensity from Step 2 and proposed slope of the drainage area to the filter strip. Revise proposed length and area draining to the filter strip if necessary.

Table 4-6 Maximum Pavement Length in Feet (n=0.011) Allowable for a Given Pavement Slope

Drainage Area Slopes (%)	10 Year Rainfall Intensity (in/hr)*											
	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5	7.0	7.5
0.5	162	130	109	93	81	73	65	59	55	50	46	44
1.0	136	109	91	78	68	61	55	50	46	42	39	37
1.5	100	80	67	58	50	45	40	37	34	31	29	27
2.0	81	65	54	47	41	36	33	30	27	25	24	22
2.5	69	55	46	39	35	31	28	25	23	21	20	19
3.0	60	48	40	34	30	27	24	22	20	19	17	16
3.5	53	43	36	31	27	24	22	20	18	17	16	15
4.0	48	39	32	28	24	22	20	18	16	15	14	13

* The 10-year return frequency rainfall intensity should be used for a duration equal to the time of concentration for the pavement area.

Table 4-7 Minimum Filter Strip Length (n=0.24) for a Minimum Travel Time = 3 Minutes

Filter Strip Slopes (%)	WQ Event Rainfall Intensity (in/hr)*																	
	0.4	0.5	0.6	0.7	0.8	0.9	1	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2	2.1
0.5	12	13	15	17	18	20	21	22	24	25	26	27	28	30	31	32	33	34
1.0	16	19	21	23	25	27	29	31	33	35	37	38	40	42	43	45	46	48
1.5	20	23	26	28	31	34	36	38	41	43	45	47	49	51	53	55	57	59
2.0	23	26	30	33	36	39	41	44	47	49	52	54	56	59	61	63	65	68
2.5	25	29	33	37	40	43	46	49	52	55	58	60	63	66	68	71	73	76
3.0	28	32	36	40	44	47	51	54	57	60	63	66	69	72	75	77	80	83
3.5	30	35	39	43	47	51	55	58	62	65	68	71	75	78	81	84	86	89
4.0	32	37	42	46	50	54	58	62	66	69	73	76	80	83	86	89	92	95
4.5	34	39	44	49	53	58	62	66	70	74	77	81	84	88	91	95	98	101
5.0	36	41	46	51	56	61	65	69	74	78	81	85	89	93	96	100	103	107
5.5	37	43	49	54	59	64	68	73	77	81	85	89	93	97	101	104	108	112
6.0	39	45	51	56	62	66	71	76	80	85	89	93	97	101	105	109	113	117

*Water quality rainfall event intensity should be used with a duration equal to the time of concentration for the drainage area to the filter strip.

- **Step 4:** Find the water quality rainfall event intensity at the duration equal to the time of concentration, using the time of concentration calculated in Step 1, using Appendix A.
- **Step 5:** Use Table 4-7 to find the minimum filter strip length required, based on the intensity from Step 4 and the proposed slope of the filter strip area in the direction of flow. Compare to site plan. Revise proposed length of the filter strip to meet minimum requirement if necessary.

4.5.5 Design Example

A 1 acre site is being developed by a small business ($C=0.80$) in Winfield. Approximately 0.20 acres of the parking lot with no parking blocks will be tributary to a proposed filter strip. The slope of the parking lot is proposed to be 1.0-percent, and the slope of the proposed filter strip is 2-percent. Find the length of the filter strip.

Figure 4-18 Site Plan of 1 Acre Small Business Site in Winfield, KS.

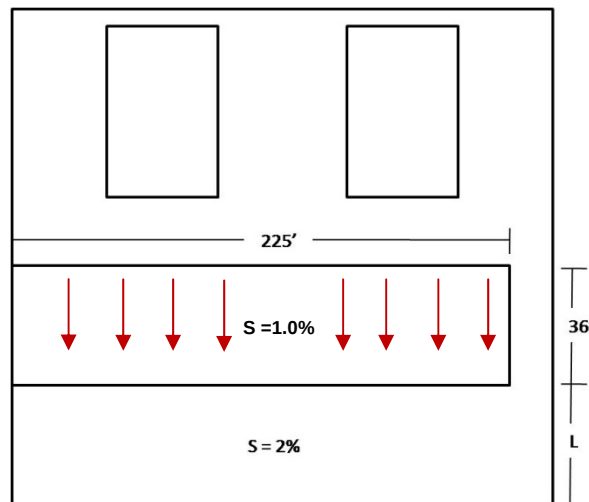


Figure 4-18 is the site plan for the proposed small business.

4.5.5.1 Time of Concentration (T_I)

T_I is found using Equation 4.8. $T_I = (1.8 * (1.1 - 0.8) * 36^{1/2}) / (1.5)^{1/3} = 2.8$ min. The minimum time of concentration should be 5 minutes. Therefore, for this example, use $T_I = 5$ minutes.

4.5.5.2 Ten Year Rainfall Intensity (I_{10})

I_{10} can be found using the graph of Rainfall Intensity Curves in Appendix A. For Winfield, KS at 5 minutes, this value is 7.5 inches per hour.

4.5.5.3 Maximum Pavement Length (PL_{MAX})

PL_{MAX} can be found using Table 4-6 and finding the maximum pavement length for a drainage area slope of 1.0-percent and a rainfall intensity of 7.5 inches per hour. For

this example, PL_{MAX} is 37 feet. Since proposed pavement length of 36 feet is less than PL_{MAX} , 36 feet can be used.

4.5.5.4 Water Quality Event Intensity (WQ_I)

WQ_I can be found using the Water Quality Event Curves for the 90-percent event. Using the duration of 5 minutes and the 90-percent plot, the WQ_I is 1.7 inches per hour.

4.5.5.5 Minimum Filter Length (FS_{MIN})

Use Table 4-7 to find the minimum length for a filter strip slope of 2-percent and a rainfall intensity of 1.7 inches per hour. For this example, FS_{MIN} is 59 feet. This length would need to be compared to the available area on the property for the filter strip. For this example the available area is 60 feet. The result is a 60 feet filter strip at 2 - percent.

4.5.6 Submittal Requirements

For review purposes prior to construction, the following minimum submittal requirements are recommended:

- Drainage area map, including drainage area to filter strip area.
- Existing and proposed contour map of site (1-foot contours recommended).
Compaction requirements should be stated, if required. Additional spot elevations may be helpful.
- Geotechnical investigation of site (soil borings, water table location).
- Stormwater plan/profile for site.
- Site plan view. Components clearly labeled with dimensions.
- Hydrologic calculations (refer to Design Example).
- Vegetation plan with schedule for installation and initial maintenance. Appropriate erosion control measures should be included.
- An as-built survey is recommended to confirm actual construction adheres to approved construction plans.
- Long-term inspection/maintenance plan.

4.5.7 References

CASQA. 2003. *California Stormwater Quality Association Stormwater Best Management Practice Handbook*. Available at www.dot.ca.gov/hq/construc/stormwater/manuals.htm

Gharabaghi, B., Rudra, R.P., Whiteley, H.R., and Dickinson, W.T. 2000. *Sediment Removal Efficiency of Vegetated Filter Strips*. Available at www.ubguelph.ca/GTI/00anrep/vegfilter.pdf

IAState-Iowa State University. 2008. *Iowa Stormwater BMP Manual*. Available at www.ctre.iastate.edu/PUBS/stormwater/index.cfm

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Section 4 Structural BMPs

4.6 Infiltration Trench

An infiltration trench is an excavated trench, typically between 3 and 12 feet deep, filled with coarse granular material, and lined with filter fabric (MARC, 2008).

Infiltration trenches are used to collect stormwater runoff for temporary storage and infiltration. Infiltration trenches can be constructed for conveyance and/or infiltration purposes. Trenches used for conveyance purposes receive runoff through pipes or trenches, while trenches collecting sheet flow are used for primarily infiltration purposes. In all infiltration trenches, runoff is stored in the spaces between the gravel and infiltrates through the bottom of the trench and into the soil matrix. By doing so, the trench not only treats the WQv, but also helps preserve the natural water balance on a site by recharging groundwater and preserving baseflow (IA State, 2008). Infiltration trenches are often combined with another BMP such as a filter strip, swale, or detention basin in a treatment train. These pre-treatment BMPs are highly recommended because they limit the amount of coarse sediment entering the trench. Sediments can clog the trench making it ineffective (IA State, 2008). Infiltration trenches can remove suspended solids, particulates, bacteria, organics, soluble metals, and nutrients through mechanisms of filtration, absorption, and microbial decomposition (MARC, 2008). Figure 4-19 is an example of the surface view of an infiltration trench.

Sections from this manual that may need to be referenced for additional information are: Section 2; Section 4.1; Section 5.

<i>Location characteristics (Slope, Soil Type)</i>	Slope: < 15% Soil Type: A
<i>Contributing drainage area</i>	< 5 acres
<i>Design size</i>	3-12' deep
<i>Detention time for WQv treatment</i>	1-3 days
<i>Pollutant removal efficiencies¹</i>	80% TSS, 60% TP and TN, 70-80% BOD
<i>Potential for education and outreach</i>	Low
<i>Potential for use with other BMPs</i>	High Pre-treatment Swale, Filter Strip
<i>Implementation Category</i>	Short Term: Easy Long Term: Difficult (See Section 5.4.1)
<i>Maintenance</i>	Medium Sediment/debris removal, potential clogging (See Section 5.4.1)

¹IA State, 2008.

**Figure 4-19 Surface View of an Infiltration Trench
(Photo: MARC, 2008)**



4.6.1 General Application

Infiltration trenches are best suited for use in residential subdivisions, small commercial lots, and parking lots. Infiltration trenches may be too space consuming for densely populated areas where underdeveloped land is scarce. They also cannot be used to treat highly contaminated runoff (MARC, 2008).

Infiltration trenches promote groundwater recharge, but the possibility for groundwater contamination must be considered where groundwater is a source of drinking water. In all circumstances, infiltration trenches should be located in areas with highly porous soils where the bedrock and/or water table are located at least four feet below the bottom of the trench (IA State, 2008). The main variable in determining trench depth is to avoid groundwater contamination.

Due to potential failure as a result of sediment clogging, infiltration trenches also need to be located at sites where upstream sediment control can be ensured (IA State, 2008).

4.6.2 Advantages and Disadvantages

Advantages	Disadvantages
Can remove up to 95-percent of suspended solids	Susceptible to clogging by sediment, necessitating frequent maintenance
Removes fine sediment, trace metals, bacteria, and oxygen-demanding substances	Risk of polluting groundwater depending on soil conditions and groundwater depth
Appropriate for small sites with porous soils	No natural components so no improvement with time
Provide groundwater recharge and preservation of stream baseflow	Cannot be used where soil infiltration rates are < 0.5 in/hr

Advantages	Disadvantages
Can be utilized below ground through pipes or channels	Restricted in karst areas (topography characterized by layers of soluble bedrock)
Fit in small spaces and can be utilized in retrofit situations	Little contribution to aesthetics and no contribution to wildlife habitat
Peak flow mitigation	

4.6.3 Design Requirements and Considerations

4.6.3.1 General Requirements

There are important site requirements to consider in the design of an infiltration trench. These include:

- Infiltration trenches should be designed to capture the WQ_V while the remaining runoff from large events bypasses the trench. The overall volume of the trench is dependent upon the water quality storm volume of runoff entering the trench from the contributing watershed (MARC, 2008). Soil infiltration rates will also be an important factor in determining trench volume.
- It is best to use multiple pretreatment techniques together with infiltration trenches to eliminate potential clogging and to extend the lifespan of the trench. It is recommended that a grass filter strip be installed upslope of the infiltration trench to help remove sediments before reaching the infiltration trench.
- Trenches shall be designed to provide a detention time of 6 to 24 hours for the water quality storm (MARC, 2008).
- The contributing drainage area to any infiltration trench should be less than five acres.
- Cold weather can limit the use of trenches. Winter sanding can clog trenches and winter salting increases the potential for chloride contamination of groundwater (IA State, 2008). In areas subject to freezing temperatures, designers shall ensure that part of the trench is constructed well below the frost line. Ensure that plowed snow is not stored on top of infiltration trench. Infiltration trenches can operate effectively in colder climates if effectively operated and maintained.
- Plans shall include a geotechnical evaluation at the site (EPA, 1999).

4.6.3.2 Location and Soils

- Infiltration trenches are suitable to capture sheet flow or function as an offline device. They can be situated in medium to high-density residential areas (IA State, 2008).

- When used in an offline configuration, the WQ_v shall be diverted to the infiltration trench through the use of a flow splitter (IA State, 2008).
- Trenches shall be located at least 150 feet away from drinking water wells in order to decrease the chance for groundwater contamination. In addition, they shall be 100 feet from building foundations (Metro Council, 2001).
- The underlying soils must meet the soil screening criteria with an infiltration rate of 0.5 in/hr or greater (EPA, 1999).
- Acceptable soil texture classes are: sand, loamy sand, sandy loam and loam. These soils are in the A or B hydrologic group. Trenches shall not be constructed on soils in the C or D hydrologic group (EPA, 1999).
- Soils reports from the Soil Conservation Service shall be used to identify soil type. Sufficient soil borings shall be taken to verify site conditions.
- The seasonally high water table must be at least four feet below the bottom of the infiltration trench (IA State, 2008).
- The drainage area (5 acres or less) must be fully developed and stabilized with vegetation prior to construction in order to avoid high sediment loads (EPA, 1999).

4.6.3.3 Slope

- The drainage area slope determines runoff velocity. Locate infiltration trenches where up-gradient slopes are 5-percent or less. The down-gradient slope should be less than 15-percent to minimize slope failure and seepage (IA State, 2008).
- The slope of the surrounding area should allow runoff to enter the trench as sheetflow. Runoff can be captured by depressing the surface of the trench or by placing a berm at the down-gradient side of the trench (IA State, 2008).

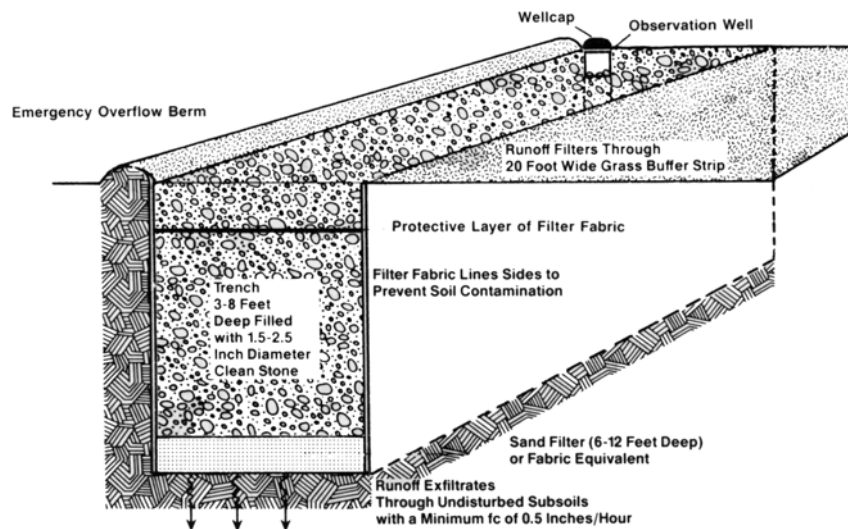
4.6.3.4 Design Specifications

- If stormwater is conveyed as channel flow, maximize the length of the trench parallel to the direction of flow.
- The storage volume of the trench shall be equal to the WQ_v . Infiltration trenches shall be designed to fully dewater within 24 hours following a rainfall event (IA State, 2008).
- The sides and bottom of the trench shall be lined with filter fabric. In addition, a layer of nonwoven filter fabric or sand shall be placed 6-12 inches below ground surface to prevent suspended solids from clogging the majority of the storage media (MARC, 2008).
- The bottom slope of the trench should be flat in order to evenly distribute flow and encourage uniform infiltration (IA State, 2008).

- Fill the infiltration trench with clean, washed stone with a diameter of 1.5 to 3 inches (void space of 38 to 42-percent). By washing stone prior to installation, fine particles are removed from the stone that could potentially cause clogging. Top the trench with stone aggregate, pea gravel, or large stones.
- Do not use limestone or shale as aggregate material in the trench as it may cement over time (MARC, 2008).
- An observation well must be located at the center of the trench to monitor water drainage from the system.
- The well can be a 4 to 6 inch diameter PVC pipe with a lockable cap. The well shall be either 6 inches above ground or flush with the ground (IA State, 2008).

Figure 4-20 provides a schematic of a typical infiltration trench.

Figure 4-20 Infiltration Trench Design (Source: Schueler, 1987)



*While the trench depth in this example is stated as 3-8 feet deep, overall trench depth may be a maximum of 12 feet deep. The aggregate used to fill the trench can vary between 1.5-3 inches. (IA State, 2008).

4.6.4 Design Example

This example outlines the design requirements of an infiltration trench in Dodge City, Kansas. The trench is constructed at ground surface and collects sheet flow from the neighboring drainage area. The total drainage area is 1.0 acres, 60-percent covered with an impervious parking lot. The high water table was found to be 9 feet below ground surface.

CRITERIA	SITE STATUS
Infiltration rate ≥ 0.5 in/hr	Infiltration rate is 0.5 in/hr, on Type A soil
Up-gradient slope $< 5\%$	Slope is 1-percent
High levels of pollution runoff should not be infiltrated	Not industrial land use
Infiltration prohibited in karst topography	Not in karst topography
Bottom of infiltration trench must be vertically separated from the high water table by 4 feet	The high water table was found to be 9 feet below ground surface. Thus, the maximum trench depth is 5 feet.
Maximum contributing area ≤ 5 acres	Contributing area is 3 acres
Infiltration trenches must be located 150 feet horizontally from any water supply well.	No water supply wells within 150 feet
Setback 100 feet from structures	Trench is 100 feet from the parking lot.

Step 1: Compute Water Quality Volume

Equation 4.1: $R_v = 0.05 + I (0.009)$

Therefore, for this example $R_v = 0.05 + 60.0 (0.009) = 0.59$

Step 2: Compute WQ_v

Equation 4.2: $WQ_v = \frac{P_{wQ} \times R_v \times A_T}{12}$

Therefore, for this example $WQ_v = (0.79\text{-inch}) \times (0.59) \times (1.0\text{ac}/12\text{-inch})$
 $WQ_v = 0.039 \text{ acre-feet} = 1698\text{ft}^3$

Step 3: Find the minimum infiltration trench volume (V_{TRMIN}) based on the WQ_v and the void space of the aggregate to be used in the trench (n). For this example n equals 40-percent.

$$V_{TRMIN} = \frac{WQ_v}{n} = \frac{1698 \text{ ft}^3}{0.40} = 4,245 \text{ ft}^3$$

This volume should be multiplied by a factor of 1.2 to account for possible loss of volume due to sedimentation.

$$V_{TR} = V_{TRMIN} * 1.2 = 4,245 * 1.2 = 5,094 \text{ ft}^3$$

Find the minimum surface area of the trench (A_{TR}).

$$A_{TRMIN} = \frac{12 \times WQ_V}{P_{SOIL} \times t}$$

Where:

P_{SOIL} = Percolation rate of soil (inch per hour)

t = Trench Retention Time (hour)

With P_{SOIL} equals 0.5 inch per hour for type A soils, and a desired infiltration time of 18 hours.

$$A_{TRMIN} = \frac{12 \times 1698}{0.5 \times 18} = 2,264 \text{ ft}^2$$

Find the minimum trench depth (D_{TRMIN}).

$$D_{TRMIN} = \frac{V_{TR}}{A_{TR}} = \frac{5094 \text{ ft}^3}{2264 \text{ ft}^2} = 2.25 \text{ ft}$$

For this example, the trench must be between 2.25 feet and 5 feet (based on the location of the water table.)

Based on the minimum surface area, a length and width for the trench can be established. Widths should not exceed 25 feet. For this example, we will assume a trench width of 6 feet.

$$L = A_{MIN} / W = \frac{2264}{6} = 377 \text{ ft}$$

Step 4: General Infiltration Trench Design Specifications

Filter Fabric

The sides and bottom of the trench shall be lined with filter fabric and a layer of filter fabric shall be added one foot below the trench surface. Filter fabric placed one foot below trench surface will maximize pollutant removal and decrease pollutant loading in the trench bottom (IA State, 2008).

Aggregate

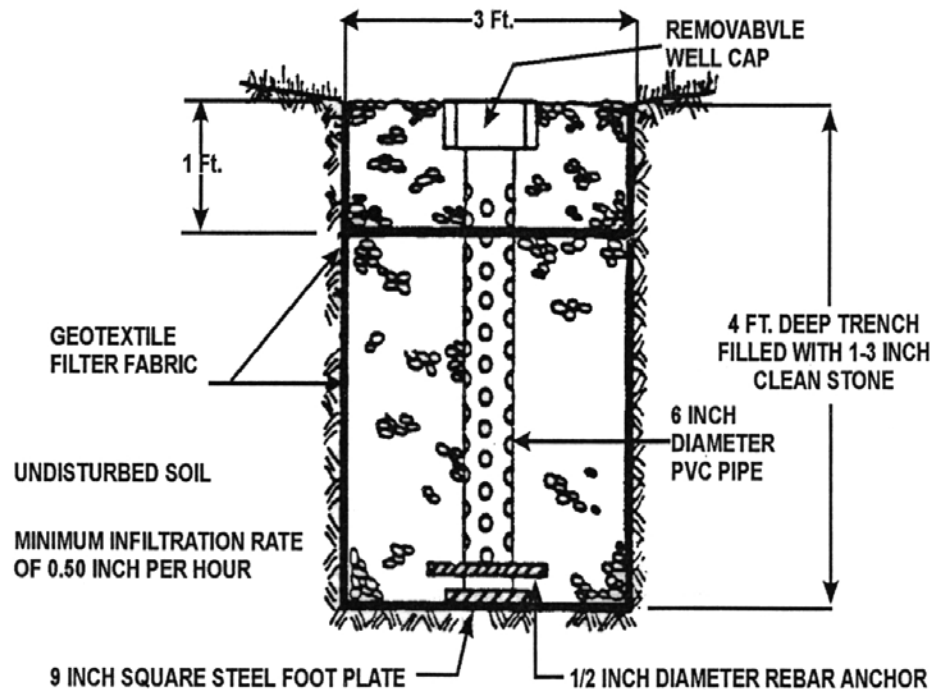
At the designer's discretion, a 4 to 6-inch layer of clean, washed sand or medium aggregate concrete sand can be placed in the bottom of the trench in lieu of filter fabric. The trench shall be filled with washed stone aggregate 1.5 to 3 inches in diameter. By washing aggregate/stone prior to installation, fine particles are removed from the stone that could potentially cause clogging. Limestone or shale should not be used. Pea gravel may be substituted for the top one foot of stone aggregate in the trench. Pea gravel shall be #8 to 3/8-inch (IA State, 2008).

Observation Well

An observation well should be installed. The well shall consist of a 4 to 6-inch diameter PVC tube with a screw-top lid and lockable cap. It shall be anchored to a footplate at the bottom of the trench, and shall be located at the longitudinal center of

the trench (Metro Council, 2001). Refer to Figure 4-21 for an example of observation well design.

Figure 4-21 Observation Well Details



Source: Southeastern Wisconsin Regional Planning Commission, 1991.

4.6.5 Submittal Requirements

For review purposes prior to construction, the following minimum submittal requirements are recommended:

- Drainage area map, including drainage area to infiltration trench.
- Existing and proposed contour map of site (1-foot contours recommended). Compaction requirements should be stated, if required. Additional spot elevations may be helpful.
- Geotechnical investigation of site (soil borings, water table location). Should include a percolation test at the total trench depth.
- Stormwater plan/profile for site.
- Site plan view. Components clearly labeled with dimensions.

- Cross section detail of proposed trench with dimensions for construction. Include appropriate design calculations (refer to Design Example). Include calculations and details for diversion structures if the trench will be used for conveyance.
- Erosion and sediment control measures.
- An as-built survey is recommended to confirm actual construction adheres to approved construction plans.
- Long-term inspection/maintenance plan.

4.6.6 References

EPA Office of Water, 1999. *Stormwater Technology Fact Sheet*.

Atlanta Regional Commission (ARC). 2001. *Georgia Stormwater Management Manual*. Available at www.georgiastormwater.com

IAState-Iowa State University. 2008. *Iowa Stormwater BMP Manual*. Available at www.ctre.iastate.edu/PUBS/stormwater/index.cfm

MARC and APWA. 2008. *Manual of Best Management Practices for Stormwater Quality*. Available at www.marc.org/environment/Water/bmp_manual.htm

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Schueler, T.R., 1987. *Controlling Urban Runoff: A Practical Manual for Planning and Designing Urban Best Management Practices*. Metropolitan Washington Council of Governments.

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Section 4 Structural BMPs

4.7 Extended Dry Detention

Extended dry detention basins (EDDBs) are designed to detain the stormwater water quality volume (WQv) for 40 hours to allow particles and associated pollutants to settle (UDFCD, 2005). This attenuation of stormwater reduces the peak stormwater runoff rate for all stormwater events. Unlike extended wet detention basins, these facilities do not maintain a permanent pool between storm events (CASQA, 2003). EDDBs may develop wetland vegetation and shallow pools in the bottom portions of the facilities (e.g., sediment forebays). Wetland vegetation may enhance the basin's soluble pollutant removal efficiency through biological uptake (UDFCD, 2005). Figure 4-22 shows an example of an extended dry detention basin.

Sections from this manual that may need to be referenced for additional information are: Section 2; Section 4.1; Section 5

<i>Location characteristics (Slope, Soil Type)</i>	Slope: < 15% Soil Type: All
<i>Contributing drainage area</i>	10-50 acres (75 acres absolute maximum) ²
<i>Design size</i>	Minimum: L:W 2:1-4:1, D 2 feet
<i>Detention time for WQv treatment</i>	40 hrs ¹
<i>Pollutant removal efficiencies¹</i>	50% TSS, 10% TN, TP ³
<i>Potential for education and outreach</i>	Low Not attractive, usually decentralized location
<i>Potential for use with other BMPs</i>	Moderate Pretreatment required for TSS removal
<i>Implementation Category</i>	Short Term: Easy Long Term: Easy (See Section 5.4.1)
<i>Maintenance</i>	Low Sediment/debris removal, vegetation upkeep (See Section 5.4.1)

¹MARC, 2008, ²IAState, 2008, ³EPA, 2006

Figure 4-22 Extended Dry Detention Basin Located at an Industrial Location



Source: NCDENR Stormwater BMP Manual

4.7.1 General Application

EDDBs can be used to improve stormwater runoff quality and reduce peak stormwater runoff rates. By providing extra storage above the required extended detention volume, an EDDB can also be used for flood control. Twenty-four hours or more of detention in an EDDB facility will remove 90-percent of the particulate pollutants (Muthukrishnan et al. 2006). Basins constructed early in the development cycle can be used to trap sediment from construction activities within the tributary drainage area (temporary sediment basins). The accumulated sediment should be removed after upstream land disturbances cease and the tributary area stabilized. The basin should be restored to design conditions for long term use (MARC, 2008). To enhance the removal of soluble nitrogen and phosphorus, it is recommended that a shallow permanent pool is maintained with wetland vegetation (Muthukrishnan et al. 2006).

EDDBs can be used to improve the quality of urban runoff coming from roads, parking lots, residential neighborhoods, commercial areas, and industrial sites given that there is adequate land space available (UDFCD, 2005). These facilities should not be used near stream corridors or stream buffer zones. EDDBs are more efficient when used in conjunction with other BMPs, such as upstream onsite source controls, downstream infiltration/filtration basins, or swales. If desired, additional volume can be provided in an EDDB for flood control benefits (UDFCD, 2005).

4.7.2 Advantages and Disadvantages

Advantages	Disadvantages
Simple design, construction, and maintenance	Moderate to low removal of soluble pollutants
High sediment and adsorbed pollutant removal	Large land requirements
Widespread application can reduce channel degradation caused by high sediment and runoff loads	Frequent maintenance removal of trash and debris
Potential for use as a flood control mechanism	
Opportunity for passive recreational and open space facilities	

4.7.3 Design Requirements and Considerations

Extended dry detention design shall be by a registered Professional Engineer in the State of Kansas. All design calculations and construction drawings shall be sealed and signed.

4.7.3.1 Site Requirements

EDDBs are very applicable to urban development and retrofit situations due to the low hydraulic head requirements that fit easily into existing drainage system constraints (Muthukrishnan et al. 2006). Guidelines for determining the appropriate location of an EDDB are outlined below.

Other infiltration BMPs should be considered in areas with high quality and/or well drained soils (Pennsylvania Stormwater Manual, 2006).

- EDDBs are appropriate in areas where pollutant removal and water quality are secondary to peak volume management.
- A maintenance ramp and perimeter access shall be included in the design to facilitate access to the basin for maintenance activities (CASQA, 2003).
- Public safety shall be considered in EDDB design. Fences and landscaping can be used to impede access to the facility, but should not impede sheet flow into the system. Limit access to outfall pipes (CASQA, 2003).
- The EDDB bottom should be 1 to 2 feet above the seasonal maximum groundwater table, as groundwater may surface within the basin or contribute baseflow to the basin (UDFCD, 2005).

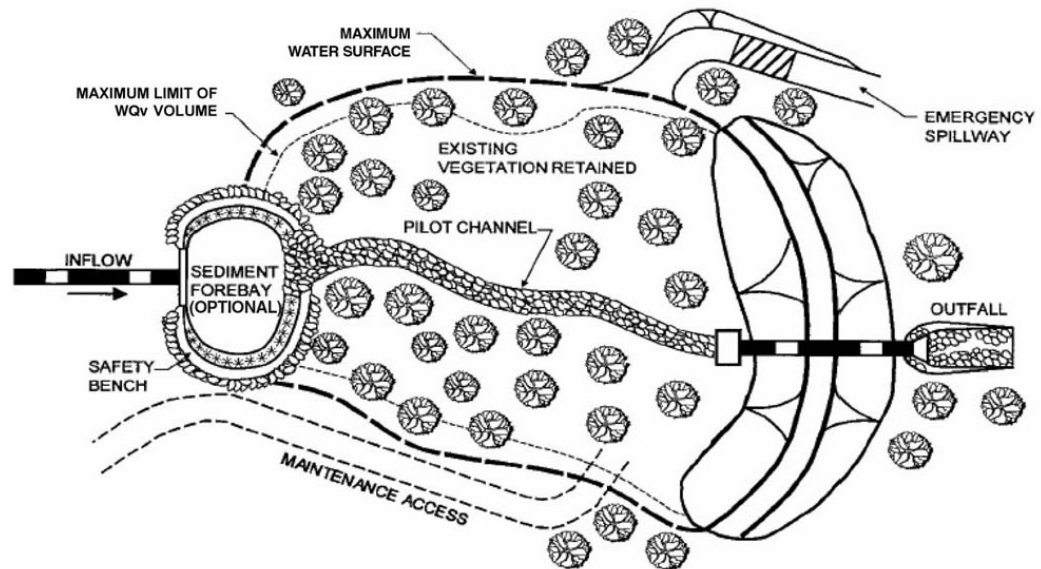
- Design EDDBs to deter large numbers of geese from gathering in the facility. Geese can add to the nutrient and fecal coli form loads entering and leaving the facility. Planting a buffer of trees, shrubs, and native ground cover around the EDDB can help discourage resident geese populations (MARC, 2008).

4.7.3.2 Basin Dimensions

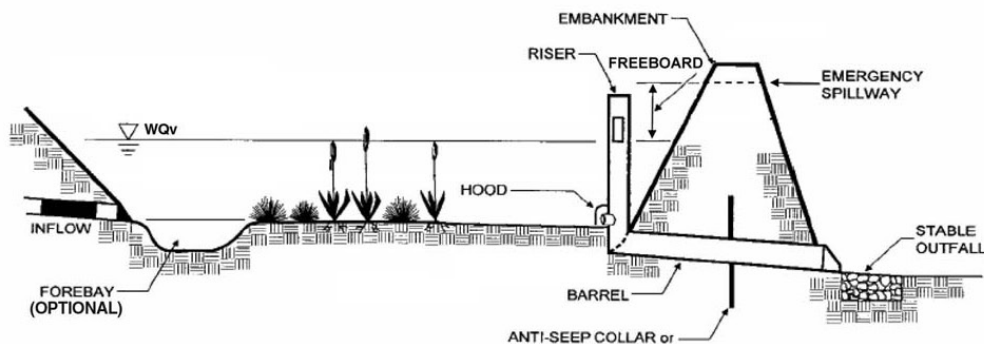
To determine the required storage volume of an EDDB, calculate the WQv based on the drainage area and add 20 percent to the result (See section 4.6.6.1). The basin shall be sized to treat this volume over 40 hours. The additional volume will promote silt and sediment deposition in the EDDB. This will allow a flow through velocity that is less than the settling velocity of pollutants (Muthukrishnan et al. 2006). Basin geometry is a function of the WQv calculated and other site characteristics. General guidelines are outlined below. Figure 4-23 shows a schematic of an extended dry detention basin.

- Basin depths shall be between 2 to 5 feet as a shallow basin with large surface area performs better than a deep basin with the same volume (Nashville, 2000).
- Side slopes should range from 20:1 to 4:1.
- The flow length to width ratio shall be at least 2:1 (Muthukrishnan et al. 2006), but 3:1 minimum is recommended. The width should gradually increase from the inlet area and then retract near the outlet area to ensure adequate detention time.
- Dams that are greater than 10 feet in height but do not fall into state or federal requirement categories shall be designed in accordance with the latest edition of SCS Technical Release No. 60, *Earth Dams and Reservoirs*, as Class C structures (KCMetro APWA, 2006).
- When flood storage for the 1 percent storm is included the EDDB design must provide protection for facility embankments. Each dam should be protected with an emergency spillway unless the principal spillway is large enough to pass the peak flow of the 1-percent storm without breaching the dam (NRCS, 2000).

Figure 4-23 Schematic of an Extended Detention Basin



Plan



Source: Maryland DOE, 2000

4.7.3.3 Basin Configuration

The inlet of the basin shall be designed to minimize runoff velocities into the basin to prevent sediment re-suspension. Runoff should flow through the inlet and into a forebay. The forebay exists to reduce sedimentation prior to runoff entry into the main basin and reduces overall maintenance. It is more cost-effective to remove sediments and trash from a small, easily accessed forebay than the large basin. The outlet should be designed to release the captured runoff over the 40 hour detention time.

Inlet

- Typical inlet structures include, but are not limited to, drop manholes, rundown chutes, baffle chutes, and pipe with impact basin (Muthukrishnan et al. 2006).
- All inlets should include some type of energy dissipater to reduce sediment re-suspension (MARC, 2008).

Forebay

- The forebay shall be a 4 to 6 foot deep cell delineated by a barrier and shall be sized to contain at least 10 percent of the WQ_v .
- The minimum length to width ratio shall be greater than 2:1 to prevent short-circuiting (Muthukrishnan et al. 2006).

Outlet

- Locate basin outlet as far away from basin inlet as possible to prevent water from short-circuiting the facility (Nashville, 2000).
- Outflow structures shall be protected by well screen, trash racks, grates, stone filters, or other approved devices to ensure that the outlet works will remain functional and not experience blockage or clogging (KC Metro APWA, 2006).
- No single outlet orifice shall be less than 4 inches in diameter (smaller orifices are more susceptible to clogging). If the calculated orifice diameter necessary to achieve a 40-hour drawdown is less than 4 inches, a perforated riser, orifice plate, or v-notch weir shall be used instead of a single orifice outlet (MARC, 2008).
- Keep perforations larger than 1 inch when using orifice plates or perforated risers. Smaller orifice sizes may be used if the weir plate is placed in a riser manhole in a sump-like condition (MARC, 2008) or is protected by a well screen.

4.7.3.4 Vegetation

Native vegetation should be used to reinforce all earthen structures and be planted along the basin perimeter to prevent erosion. Utilizing vegetation at the basin inlet will also filter incoming runoff and may initiate slower velocities. Vegetation surrounding the outlet may serve as a buffer for the BMP to reduce runoff impacts on downstream areas. Information about the establishment and maintenance of native vegetation is outlined in Section 5 of this manual.

4.7.4 Design Calculations

A short summary of the design calculations is presented below. A detailed design example is presented in Section 4.7.5.

- **Step 1** Determine WQ_v based on drainage area and regional precipitation information according to Equations 4.1 and 4.2.

Equation 4.1 $R_v = 0.05 + 0.009(I)$

Equation 4.2 $WQ_v = \frac{P_{wQ} \times R_v \times A_T}{12}$

Where:

To obtain basin design volume, V_{DESIGN} , multiply WQ_v by 1.2 to account for sedimentation (approximately 20-percent of the WQ_v)

- **Step 2** Determine the outlet type (single orifice, perforated riser, or v-notch weir), outlet loads, and required outlet dimensions. If the diameter calculated for a single orifice is less than 4 inches, use a perforated riser or v-notch weir outlet to prevent clogging. Use equation 4.16 to determine the outflow rate. Equations specific to the outlet type are presented in Appendix G.
- **Step 3** Size trash racks according to outlet type and size. Equations specific to the outlet type are presented in Appendix G.

Equation 4.16 Water Quality Outflow Rate

$$Q_{wQ} = \frac{43,560 \text{ ft}^2 \times WQ_v}{40 \text{ hrs} \times 3,600 \text{ s}}$$

Where:

Q_{wQ} = Average water quality outflow rate (cfs)

WQ_v = Water quality volume (acre feet)

- **Step 4** Design the forebay based on WQ_v and minimum depth requirements. The forebay volume should be greater than 10-percent of the WQ_v (Equation 4.22). The forebay surface area is calculated using Equation 4.23.

Equation 4.22 Forebay Volume

$$V_{FB} > 0.1 WQ_v$$

Equation 4.23 Forebay Surface Area

$$A_{FB} (ac) = \frac{V_{FB} (ac - ft)}{Z_{FB} (ft)}$$

- **Step 5** Determine basin shape, basin side slopes, and dam embankment side slopes.
- **Step 6** Install appropriate vegetation using methodology provided by local native vegetation experts.

4.7.5 Design Example

A single-family housing development (65-percent impervious) is being built on previously undeveloped land in Hays. The developer is required to design and build an EDDB to accept runoff from the 50 acre tributary drainage area and provide an outlet device that will release the WQ_v within 40 hours of the WQ event. The majority of soil in the development has high-clay content. The land slopes are less than 10-percent across the development area. Refer to Appendix G for example calculations.

4.7.5.1 Basin Water Quality Volume (Step 1)

Determine the tributary area to the EDDB (A_T)

The tributary area, A_T, is 50 acres. Due to the fact that the percent imperviousness is already known, we can utilize the Short-Cut Hydrology Method.

Calculate the R_v based on equation 4.1

The tributary area is 65-percent impervious. Thus, $R_v = 0.05 + 0.009(65) = 0.635$.

Calculate the WQ_v based on equation 4.2

For Hays, KS, the water quality event is 0.9 inches. $WQ_v = (0.9 \text{ inch} * 0.635 * 50 \text{ acre}) / 12 \text{ inches} = 2.38 \text{ acre feet}$.

$$V_{\text{DESIGN}} = (1.2) * WQ_v = 2.86 \text{ acre feet}$$

4.7.5.2 Water Quality Outlet (Step 2)

For this example, we will use a single orifice for an outlet structure. Equations associated with this outlet structure are presented in Appendix G. If the orifice diameter required to drain the excess to the permanent pool is less than 4 inches, a perforated riser or v-notch weir should be used (MARC, 2008).

Water quality depth (Z_{WQ})

Set the depth above the WQ_v outlet (Z_{WQ}) based on facility dimensions for surface area and desired depth.

$$Z_{WQ} = 3 \text{ feet}$$

Average WQ_v head (H_{WQ})

The average head is half of the depth above the WQ_v outlet.

For this example, $H_{WQ} = 0.5(3 \text{ ft}) = 1.5 \text{ feet}$.

Outflow rate (Q_{WQ})

Calculate the average outflow rate that results from the WQ_v exiting the system over 40 hours using Equation 4.16.

For this example, $Q_{WQ} = ((2.38 \text{ acre feet}) * 0.3025) = 0.72 \text{ cubic feet per second (cfs)}$

Orifice discharge coefficient (C_o)

Set orifice coefficient (C_o) depending on orifice plate shape. For this example $C_o = 0.62$.

Orifice Diameter (D_o)

Calculate the diameter using the Equation G.1 and assuming a $C_o = 0.62$.

$D_o = 24 * ((0.72 \text{ cfs}) / (0.62 * \pi * (2 * 32.2 \text{ (ft}^2/\text{s)} * 1.5 \text{ ft})^{1/2})^{1/2}) = 4.7 \text{ inches}$. Due to the fact that this diameter is greater than 4 inches, a single orifice outlet will provide adequate drawdown configurations.

4.7.5.3 Flood Control

If designing the EDDB for flood control, follow local agency guidelines for detention basins.

4.7.5.4 Trash Racks (Step 3)

The trash racks protect outlet structures from damage resulting from trash and debris. Calculations are based on the outlet type used. Reference Appendix G for outlet type specific equations.

Outlet Area (A_{OT})

Calculate the water quality outlet area based on the orifice diameter using equation G.9.

For this example, $A_{OT} = (\pi/4) * (4.7 \text{ inches})^2 = 17.0 \text{ inches}^2$.

Open Area (A_T)

Calculate the required trash rack open area from the total outlet area based on outlet structure type for equations see Appendix G.

For this example, we used a single orifice outlet and thus will use equation G.10.

$$A_T = (17.0 \text{ inches}^2) * 77e^{-0.124 * 4.7} = 732 \text{ square inches}.$$

4.7.5.5 Basin Shape

- The flow path through the facility shall be made as long as possible to increase stormwater runoff residence time in the basin (UDFCD, 2005).
- A pilot channel can be constructed through the main part of the facility to convey low flows from the forebay to the bottom stage. A minimum 4 inch depth is required if concrete lined sides are used and 8 inches if buried riprap sides are used. At a minimum, provide conveyance capacity equal to twice the release capacity at the upstream forebay outlet (UDFCD, 2005).
- The top stage is defined as the basin bottom adjacent to the pilot channel on either side. It shall be at least 1 foot deep (D_t s) with its bottom sloped 1 percent to 2 percent toward the pilot channel (S_t s) (UDFCD, 2005).

- The bottom stage is defined as the deep portion of the EDDB around the outlet structure. This part of the basin shall be 1.25 to 3.0 feet deeper than the top stage. The bottom stage shall store 10 percent to 25 percent of the WQ_V that is stored below the top stage.

4.7.5.6 Forebay (Step 4)

Forebay volume (V_{FB})

The forebay volume should be greater than 10-percent of the WQ_V (Equation 4.22).

For this example, V_{FB} must be greater than $0.1 \times (2.38 \text{ acre feet}) = 0.2 \text{ acre feet}$.

Forebay depth (Z_{FB})

The forebay depth should be at least 4 feet deep.

Minimum forebay surface area (A_{FB})

For this example using equation 4.23, $A_{FB} = 0.2/4 = 0.1 \text{ acre}$.

4.7.5.7 Basin Side Slopes (Step 5)

The basin side slopes should be at least 4:1 (H:V) to ensure public safety and maintenance access. Stabilize side slopes with native vegetation.

4.7.5.8 Dam Embankment Side Slopes (Step 5)

- Dam embankment side slopes should not exceed 3:1 (H:V) for public safety.
- Embankment soils should be compacted to at least 95 percent of their maximum density according to ASTM D 698-70 (Modified Proctor).

4.7.5.9 Vegetation (Step 6)

To facilitate stabilization and biological filtration, the basin berms and side slopes should be planted with native vegetation.

To determine the appropriate native species, gather the following information about the EDDB site:

- Soil types (soil tests, soil maps in Appendix B)
- Annual precipitation with dates for wet/dry season (Maps in Appendix A)
- Ecoregion and corresponding vegetation (Map and table in Appendix C)
- Previous land use

Provide the soil type, precipitation, previous land use, and ecoregion information to a native vegetation expert for planting suggestions (vegetation types, seeding rates, establishment procedures, maintenance procedures). Use the “typical vegetation” listed in Appendix C as a guideline to check final list. Native vegetation contacts and links are listed in Appendix C.

4.7.5.10 Inlet Protection

Dissipate flow energy at basin's inflow point(s) to limit erosion and promote particle sedimentation.

4.7.5.11 Access

For maintenance purposes, there must be an all-weather access to the bottom and forebay (UDFCD, 2005). Slopes should not exceed 3:1.

4.7.6 Submittal Requirements

For review purposes prior to construction, the following minimum submittal requirements are recommended:

- Drainage area map, including drainage area to detention basin.
- Existing and proposed contour map of site (1-foot contours recommended).
Compaction requirements should be stated, if required. Additional spot elevations may be helpful.
- Geotechnical investigation of site (soil borings, water table location).
- Stormwater plan/profile for site.
- Detention basin plan view. Components clearly labeled with dimensions.
- Hydrologic calculations (refer to Design Example).
- Detail of control structure (orifice/weir) with dimensions for construction. Include appropriate design calculations (refer to Design Example).
- Velocity downstream of control structure. Appropriate armoring should be specified.
- Vegetation plan with schedule for installation and initial maintenance. Appropriate erosion control measures should be included.
- An as-built survey of the detention basin is recommended to confirm actual construction adheres to approved construction plans.
- Long-term inspection/maintenance plan.
- Other requirements as required by local jurisdiction for flood storage beyond water quality event.

4.7.7 References

CASQA. 2003. *California Stormwater Quality Association Stormwater Best Management Practice Handbook*. Available at www.dot.ca.gov/hq/construc/stormwater/manuals.htm

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IAState-Iowa State University. 2008. *Iowa Stormwater BMP Manual*. Available at www.ctre.iastate.edu/PUBS/stormwater/index.cfm

KCMetro APWA. 2006. *Division V Section 5600 Storm Drainage Systems and Facilities*. Available at kcmetro.apwa.net/kcmetro/specs/APWA5600.pdf

MARC and APWA. 2008. *Manual of Best Management Practices for Stormwater Quality*. Available at www.marc.org/environment/Water/bmp_manual.htm

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NCDNER. 2007. *NCDENR Stormwater Best Management Practices Manual*. Available at www.h20.enr.state.nc.us/su/manuals_factsheets.htm.

NRCS- Maryland Natural Resources Conservation Service. 2000. *Code No. 378 Pond Standards/Specifications*.

UDFCD. 2005. *Urban Storm Drainage Criteria Manual – Volume 3: Best Management Practices*. Denver, Colorado.

Section 4

Structural BMPs

4.8 Extended Wet Detention

Extended wet detention basins (EWDBs) are designed to reduce pollutants from stormwater runoff via removal mechanisms in the permanent pool and decrease peak runoff rates with an extended storage capacity (UDFCD, 2005, IDEQ, 2005). The primary removal mechanism is settling as stormwater runoff resides in this pool, but pollutant uptake, particularly of nutrients, also occurs to some degree through biological and chemical activity in the pond (CASQA, 2003). In addition, a temporary detention volume is provided above this permanent pool to capture the water quality volume (WQv) and enhance sedimentation (UDFCD, 2005). EWDBs differ from traditional wet ponds in that the WQv is split between the permanent pool and the extended detention volume that is provided above the pool (IAState, 2008). The influent water mixes with the permanent pool water as it rises above the permanent pool level. The temporary detention volume above the permanent pool provides additional time for sedimentation. The surcharge captured volume above the permanent pool is then released over 40 hours (UDFCD, 2005). EWDBs have similar levels of pollutant removal as a traditional wet detention basin, but require less land area (Iowa Stormwater Manual, 2008). EWDBs are similar in function to constructed wetlands but differ primarily in that they have a greater average depth (CASQA, 2003). EWDBs can be very effective in removing pollutants, and, under the proper conditions, can satisfy multiple objectives, including water quality improvement, flooding and erosion protection, creation of wildlife and aquatic habitats, and recreational and aesthetic provision (UDFCD, 2005). Figure 4-24 is a photograph of an extended detention basin.

Sections from this manual that may need to be referenced for additional information are: Section 2; Section 4.1; Section 5

<i>Location characteristics (Slope, Soil Type)</i>	Slope: < 10% ¹ Soil Type: All
<i>Contributing drainage area</i>	Site specific; requires water budget calculations – rule of thumb is at least 10 acres per acre of permanent pool surface area ¹
<i>Design size</i>	Tributary area from 2 to 1,000 acres
<i>Detention time for WQv treatment</i>	40 hrs
<i>Pollutant removal efficiencies¹</i>	80% TSS, 65% TP 35-65% TN ²
<i>Potential for education and outreach</i>	High Lot level private gardens can be part of your NPDES outreach activities
<i>Potential for use with other BMPs</i>	Moderate Pretreatment required for TSS removal
<i>Implementation Category</i>	Short Term: Easy Long Term: Easy (See Section 5.4.1)
<i>Maintenance</i>	High Sediment/debris removal, vegetation upkeep (See Section 5.4.1); Permanent pool depth inspection/ maintenance

¹Mid-America Regional Council, 2008, ²IAState, 2008

Figure 4-24 Extended Wet Detention Basin with Landscaping and Recreational Components



Source: MARC, 2008

4.8.1 General Application

EWDBs can be used to improve stormwater runoff quality and reduce peak stormwater runoff rates and peak stages from roads, parking lots, residential

neighborhoods, commercial areas, and industrial sites. An EWDB can also be designed to provide flood control benefits. An EWDB is more applicable to treat larger tributary areas than other BMPs, and can be utilized as a second BMP in a treatment train. An EWDB may be used for a smaller site if the drainage area is sufficient for sustaining a permanent pool. An EWDB works well in conjunction with other BMPs such as upstream onsite source controls and downstream filter basins or wetland channels (UDFCD, 2005). See Section 2 for applicability of an EWDB in a treatment train.

4.8.2 Advantages and Disadvantages

Advantages	Disadvantages
Moderate pollutant removal ¹ 80% TSS ² , 65% TP ² 35-65% TN ³	Low volume reduction (+/- 10%)
Peak flow mitigation ¹	Potential outflow impacts on downstream quality
Potential for use as a flood control mechanism ¹	Increases in surface water temperature
Opportunity for recreational and open space facilities ¹	May attract unwanted wildlife such as geese
Widespread application can reduce channel degradation caused by high sediment and runoff loads ¹	Can be a source of odor if not properly maintained, which includes maintaining the permanent pool depth
Wildlife habitat	

¹MARC, 2008, ²IDEQ, 2005, ³Iowa, 2008

4.8.3 Design Requirements and Considerations

Extended dry detention design shall be by a registered Professional Engineer in the State of Kansas. All design calculations and construction drawings shall be sealed and signed.

4.8.3.1 Site Requirements

EWDBs are very applicable for the management of runoff from large drainage areas. EWDB facilities should be designed as off-line entities outside of stream corridors and buffer areas (MARC, 2008). Due to their ability to serve larger drainage areas, EWDBs can be designed for recreational and wildlife preservation purposes in mind. Guidelines for determining the appropriate location of an EWDB are outlined below.

- EWDBs shall have between 2 and 1,000 acres tributary to the facility (KC Metro APWA, 2006).
- Do not locate EWDBs on fill sites or on or near steep slopes. Depending on soils, bottom modifications can include compaction, incorporating clay into the soil, or an artificial liner (Nashville, 2006).

- A maintenance ramp and perimeter access should be included in the design to facilitate access to the basin for maintenance activities (CASQA, 2003).
- The maximum water surface that the facility is designed for shall be a minimum distance of 20 feet from property lines and building structures or per agency specification. A greater distance may be necessary when the detention facility might compromise foundations or slope stability (KC Metro APWA, 2006).
- Public safety shall be considered in EWDB design. Fences and landscaping can be used to impede access to the facility. The facility shall be contoured so as to eliminate any drop-offs or other hazards.
- When possible, terraces or benches shall be used to transition into the permanent pool. In some cases there is not sufficient room for grading of this type and the pond may require a perimeter fence (Nashville, 2006).

4.8.3.2 Basin Dimensions

Basin geometry is a function of the WQ_v calculated and other site characteristics. To determine the required storage volume of an EWDB, calculate the WQ_v based on the drainage area and add 20 percent to the result. This will provide the basin size necessary to treat this volume over 40 hours. The additional volume will account for silt and sediment deposition in the EWDB. This volume allows a flow through velocity that is less than the settling velocity of pollutants (Muthukrishnan et al. 2006). General guidelines are outlined below.

- Side slopes above the littoral bench (see Figure 4-25) shall be 4:1 (H:V) or flatter unless retaining walls are used. Side slopes below the littoral bench can be as steep as 3:1 to maximize permanent pool volumes where needed (Nashville, 2006).
- To maintain a permanent pool, the tributary area to the EWDB should be at least 5.5 acres for each acre-foot of permanent pool volume and at least 10.3 acres for each acre of permanent pool surface area. Table 4-8 presents threshold tributary areas for different Rational C values. These are general guidelines. Water budget calculations are recommended for most designs.
- Design of the permanent pool volume should allow for 14 days hydraulic residence time to allow for particulate settling and nutrient uptake. This is accomplished by sizing the pool using regional precipitation data and characteristics of the tributary area to the EWDB. These considerations are illustrated in the design example at the end of this section.
- The EWDB shall be designed to detain the WQ_v above the permanent pool and shall release the WQ_v over a 40 hour period. Additional flood control volume can also be provided above the permanent pool (UDFCD, 2005). Refer to local stormwater detention for design specifications if flood control is to be incorporated into the design of the EWDB.

- Dams that are greater than 10 feet in height but do not fall into state or federal requirement categories shall be designed in accordance with the latest edition of SCS Technical Release No. 60, *Earth Dams and Reservoirs*, as Class C structures (KC Metro APWA, 2006).

Table 4-8 Threshold Tributary Areas to EWDB (MARC, 2008)

	Rational Runoff Coefficient							
	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1
Minimum Tributary Area per Acre-Foot of Volume	18.4	13.8	11	9.2	7.9	6.9	6.1	5.5
Minimum Tributary Area per Acre of Surface Area	34.2	25.7	20.5	17.1	14.7	12.8	11.4	10.3

Reproduced from MARC, 2008

4.8.3.3 Basin Configuration

The inlet of the basin shall be designed to minimize runoff velocities to prevent sediment re-suspension. Runoff will flow through the inlet and into a forebay. The forebay exists to collect sedimentation prior to runoff entry into the main basin, therefore reducing overall maintenance. It is more cost-effective to remove sediments and trash from a small, easily accessed forebay than the large basin. The permanent pool depth should be designed to limit sedimentation and vegetation encroachment into the open water surface. The outlet should be designed to release the captured runoff over the 40 hour detention time without erosion. It is recommended to install a trash rack at the outlet to aid in maintenance. Figure 4-25 offers guidance for basin configurations.

Inlet

- Typical inlet structures include, but are not limited to, drop manholes, rundown chutes, baffle chutes, and pipe with impact basin (Muthukrishnan et al. 2006).
- All inlets should include some type of energy dissipater to reduce sediment re-suspension (MARC, 2008).

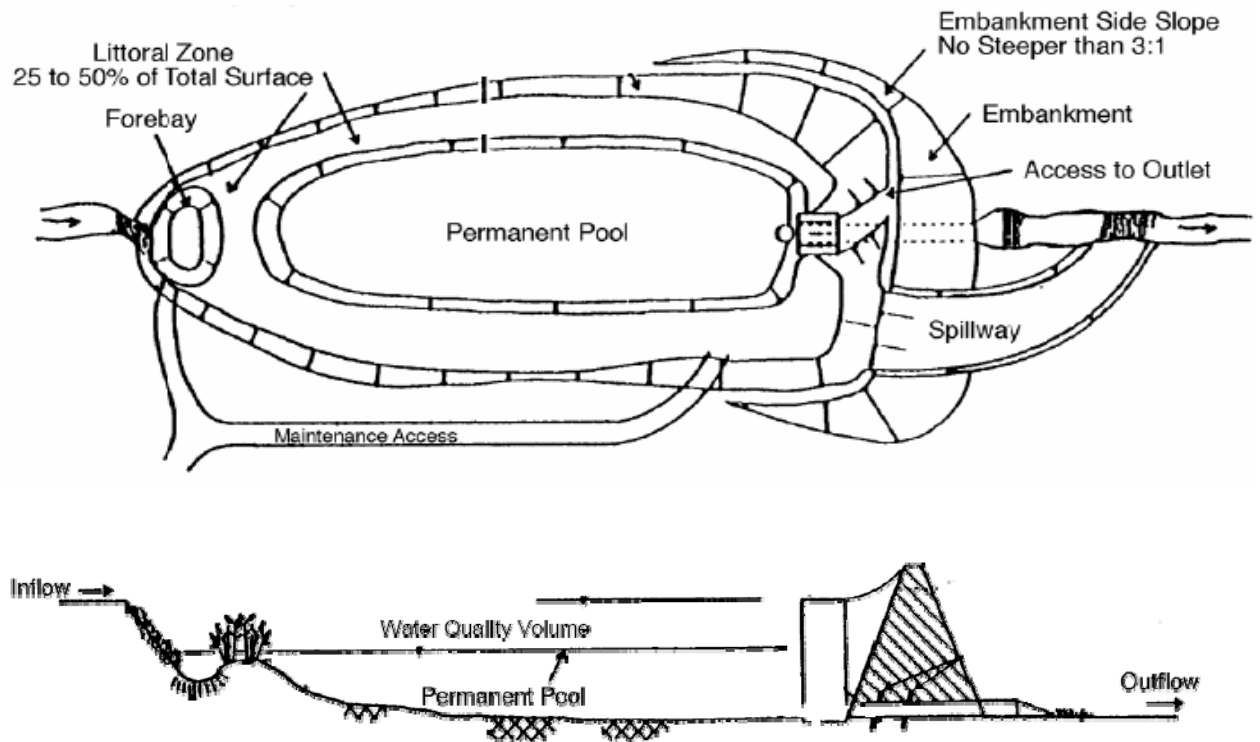
Forebay

- The forebay shall be a 4 to 6 feet deep cell delineated by a barrier and shall be sized to contain at least 10 percent of the WQv.
- The minimum length to width ratio shall be a minimum of 2:1 (3:1 recommended) to prevent short-circuiting (Muthukrishnan et al. 2006).

Permanent Pool

- The permanent pool shall include a littoral bench, or shelf, around the pool's perimeter which serves as both a safety feature and a planting surface for wetland vegetation.

Figure 4-25 Cross Sectional View of Extended Wet Detention Basin



Source: MARC, 2008

- The littoral bench shall extend inward at least 10 feet from the perimeter of the permanent pool and shall be between 6 inches to 12 inches below the permanent pool surface (CASQA, 2003, UDFCD, 2005).
- The slope of the littoral bench shall not exceed 6:1. The bench shall be planted with native wetland vegetation to promote biological uptake of nutrients and dissolved pollutants and reduce the formation of algal mats. To maximize biological uptake but prevent plants from encroaching on the open water surface, the vegetated littoral bench shall comprise 25 percent to 50 percent of the permanent pool surface area (Nashville, 2006).
- Permanent pool depths optimally range from 4 feet to 6 feet, and shall be no greater than 12 feet (CASQA, 2003). The minimum depth of 4 feet shall be provided in addition to an estimated depth of sediment accumulation from 5 years of EWDB service. Permanent pool depth should be verified annually. If EWDB is used as a siltation basin prior to a BMP, bottom elevation within the EWDB may need to be modified to attain the required permanent pool depth. This can be verified by requiring an as-built survey of the basin post construction.
- If the facility is to contain fish, at least one-quarter of the area of the permanent pool must have a minimum depth of 10 feet plus a sedimentation allowance (KC Metro APWA, 2006).

- In very dry climates, an impermeable liner may be required to maintain an adequate permanent pool level (CASQA, 2003).

Outlet

- The outlet shall be designed to discharge the WQv over a period of 40 hours (UDFCD, 2005).
- Locate basin outlet as far away from basin inlet(s) as possible to prevent water from short-circuiting the facility. The flow path(s) should have a minimum length of two times the facility width, as measured across the center of the facility in the smallest dimension at the permanent pool elevation (Nashville, 2006).
- No single outlet orifice shall be less than 4 inches in diameter (smaller orifices are more susceptible to clogging).
- If the calculated orifice diameter necessary to achieve a 40-hour drawdown is less than 4 inches, a perforated riser, orifice plate, or v-notch weir shall be used instead of a single orifice outlet. Keep perforations larger than 1 inch when using orifice plates or perforated risers. Smaller orifice sizes may be used if the weir plate is placed in a riser manhole in a sump-like condition or protected by a well screen.
- A reverse-slope pipe can be used to prevent outlet clogging from debris. A reverse-slope pipe draws from below the permanent pool extending in a reverse angle up to the riser and establishes the water elevation of the permanent pool. Because these outlets draw water from below the level of the permanent pool, they are less likely to be clogged by floating debris (CASQA, 2003).
- The facility shall have a separate drain pipe with a manual valve that can completely drain the pond for maintenance purposes. To allow for possible sediment accumulation, the submerged end of the pipe shall be protected, and the drain pipe shall be sized to drain the pond within 24 hours (CASQA, 2003).

4.8.3.4 Vegetation

Native vegetation should be used to reinforce all earthen structures and be planted along the basin perimeter to prevent erosion. Utilizing vegetation at the basin inlet will also filter incoming runoff and may initiate slower velocities. Vegetation surrounding the outlet may serve as a buffer for the BMP to reduce runoff impacts on downstream areas. Information about the establishment and maintenance of native vegetation is outlined in section 5 of this manual.

4.8.3.5 Potential Treatment Train Options

These basins work well in conjunction with BMPs that are designed primarily for sediment reduction. EWDBs are also effective when combined with BMP's that effectively reduce runoff volumes. EWDBs can be used as a flood mitigation facility. EWDBs can also be used for recreation, open space, or wildlife habitat if wetlands or shallow pools are incorporated into the design (UDFDC, 2008).

4.8.4 Design Calculations

A short summary of the design calculations is presented below. A detailed design example is outlined in 4.8.6.

- **Step 1** Determine WQ_V based on drainage area and regional precipitation information according to Equations 4.1 and 4.2.

$$\text{Equation 4.1} \quad R_v = 0.05 + 0.009(I)$$

$$\text{Equation 4.2} \quad WQ_V = \frac{P_{WQ} \times R_v \times A_T}{12}$$

Where:

To obtain basin design volume, V_{DESIGN} , multiply WQ_V by 1.2 to account for sedimentation (approximately 20-percent of the WQ_V)

- **Step 2** Size the permanent pool volume based on the 14 day retention time requirement and desired sedimentation rates. First calculate the rational runoff coefficient according to Equation 4.5. Compare the volumes calculated in Equation 4.24 and Equation 4.26. The larger of the two is the permanent pool volume, which is then multiplied by 1.2 to account for sedimentation.

Equation 4.5 Rational Runoff Coefficient

$$C = 0.3 + 0.6 * \left(\frac{I}{100} \right)$$

Where:

C = Rational Runoff Coefficient
I = Percent impervious area (%)

Equation 4.24 14 day permanent pool volume (acre feet)

$$V_{P1} (ac - ft) = \frac{C * A_T * R_{14}}{12}$$

Where:

V_{P1} = 14 day permanent pool volume (acre feet)
C = Rational Runoff Coefficient
 A_T = Tributary area (acre)
 R_{14} = 14-day wet season rainfall depth (inch) (Table 4-9)

Equation 4.25 Impervious tributary area (acre)

$$A_{T,I} = A_T * \frac{I}{100}$$

Where:

$A_{T,I}$ = Impervious tributary area (acre)
 A_T = Tributary area (acre)
 I = Percent impervious area (%)

Equation 4.26 Sedimentation permanent pool volume

$$V_{P2} = \frac{V_{B/R} * S_d * A_{T,I}}{12}$$

Where:

V_{P2} = Sedimentation permanent pool volume (acre feet)
 $V_{B/R}$ = Runoff volume ratio from Figure 4-26.
 S_d = Mean storm depth (inch) (Table 4-9)
 $A_{T,I}$ = Impervious tributary area (acre)

Equation 4.27 Surface area of permanent pool

$$A_P = \frac{V_P}{Z_d}$$

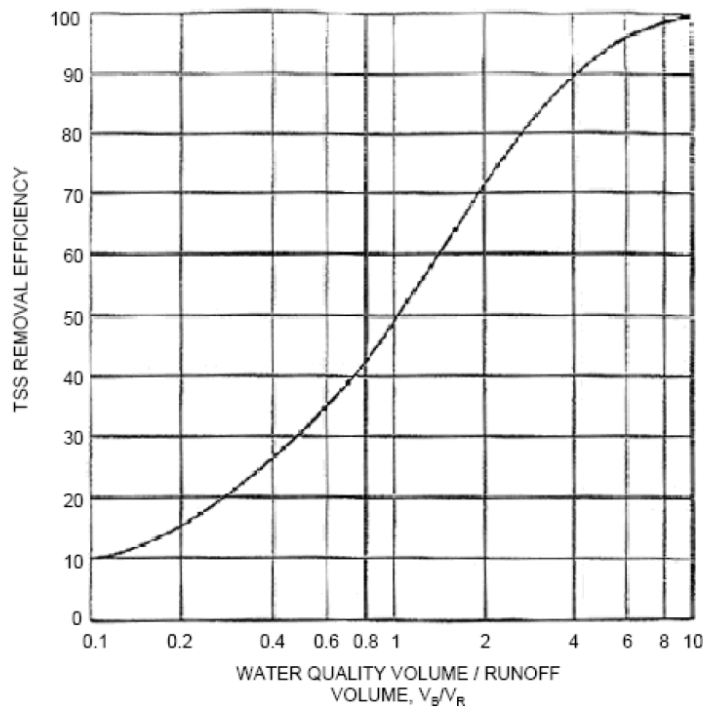
Where:

A_P = Surface area of permanent pool (acre)
 V_P = Permanent pool volume that accounts for 20 percent sedimentation (acre feet)
 Z_d = Average permanent pool depth (feet)

Table 4-9 Fourteen Day Wet Season Rainfall Depth (R_{14}) and Mean Storm Depth (S_d) for Phase II Kansas Cities

City	County	KS Region	S_d	R_{14}
Dodge City	Ford	West	0.29	0.80
Garden City	Finney	West	0.34	0.74
Hays	Ellis	West	0.36	1.34
Great Bend	Barton	Central	0.40	1.38
Manhattan	Riley	Central	0.44	1.78
Newton	Harvey	Central	0.46	1.86
Salina	Saline	Central	0.40	1.23
Arkansas City	Cowley	Central	0.44	1.61
Hutchinson	Reno	Central	0.46	1.86
Winfield	Cowley	Central	0.44	1.61
Coffeyville	Montgomery	East	0.57	1.97
Lawrence	Douglas	East	0.46	1.98
Ottawa	Franklin	East	0.46	1.99
Emporia	Lyon	East	0.46	1.99

Figure 4-26 Relationship Between TSS Removal and the Ratio of WQ_v to Runoff Volume ($V_{B/R}$)



Source: FHWA, 1989

- **Step 3** Determine the outlet type (single orifice, perforated riser, or v-notch weir), outlet loads, and required outlet dimensions. If the diameter calculated for a single orifice is less than 4 inches, use a perforated riser or v-notch weir outlet to prevent clogging. Use equation 4.16 to determine the outflow rate. Equations for each outlet type are presented in Appendix G.
- **Step 4** Size trash racks according to outlet type and size. These calculations will vary depending on outlet structure type (See Appendix G).
- **Step 5** Design the forebay based on WQ_v and minimum depth requirements. The forebay volume should be greater than 10-percent of the WQ_v (Equation 4.22) and the forebay surface area is calculated using Equation 4.23.

Equation 4.22 Forebay Volume

$$V_{FB} > 0.1 WQ_v$$

Where:

V_{FB} = Forebay volume (acre feet)

WQ_v = Water quality volume (acre feet)

Equation 4.23 Forebay Surface Area

$$A_{FB} = \frac{V_{FB}}{Z_{FB}}$$

Where:

A_{FB} = Forebay surface area (acre)
 V_{FB} = Forebay volume (acre feet)
 Z_{FB} = Forebay depth (feet)

- **Step 6** Calculate the littoral bench dimensions according to Equations 4.34 and 4.35.

Equation 4.34 Littoral Bench Surface Area

$$0.25 A_p \leq A_{LB, MIN / MAX} \leq 0.5 A_p$$

Where:

A_p = Permanent pool surface area (acre)
 A_{LB} = Littoral bench surface area (acre)

Equation 4.35 Littoral bench width

$$W_{LB, MIN / MAX} = \frac{1}{2} \sqrt{\frac{4}{\pi} A_{LB, MIN / MAX} (43560 \text{ft}^2 / \text{ac})}$$

Where:

W_{LB} = Littoral bench width (feet)
 A_{LB} = Littoral bench surface area (acre)

- **Step 7** Determine basin shape, basin side slopes, and dam embankment side slopes.
- **Step 8** Install appropriate vegetation using methodology provided by local native vegetation experts.

4.8.5 Design Example

A commercial shopping area is being built on previously undeveloped land in Lawrence. The designer would like to build an extended wet detention basin to treat the runoff from a tributary area of 50 acres, including the facility roofs and parking lots (85-percent impervious). The majority of soil in the development is type D and has high-clay content. The land slope is less than 5-percent across the development. Example calculation spreadsheet can be found in Appendix G.

4.8.5.1 Basin Water Quality Volume (Step 1)

Determine the tributary area to the EWDB (A_T)

The tributary area, A_T , is 50 acres. Due to the fact that $A_T = 50$ acres and the percent imperviousness is already known, we shall utilize the Short-Cut Hydrology Method.

Calculate the R_v based on equation 4.1

The tributary area is 85-percent impervious. Thus, $R_v = 0.05 + 0.009(85) = 0.815$

Calculate the WQv based on equation 4.2

For Lawrence, the water quality event is 1.18 inches. The WQv is
 $WQ_v = (1.18 \text{ in}) * (0.815) * (50 \text{ ac.}) / 12 \text{ in} = 4.0 \text{ ac-ft}$

4.8.5.2 Permanent Pool Volume (Step 2)

Fourteen day Volume (V_{P1})

This method calculates the volume required in the permanent pool to detain water for the minimum 14 days. This allows time for algae uptake of phosphorus and sedimentation where phosphorus may be concentrated.

Enter the 14-day wet season rainfall R_{14} from Table 4-9 or Appendix A.

For Lawrence, the R_{14} is 1.98 in.

Determine the Rational Runoff Coefficient (C) for the tributary area based on equation 4.5.

For this site, $C = 0.3 + 0.6(85/100) = 0.81$

Calculate the permanent pool volume (V_{P1}) from equation 4.24.

*For this example, $V_{P1} = (0.81 * 50 * 1.98) / 12 = 6.7 \text{ ac-ft}$.*

Sedimentation Volume (V_{P2})

This method calculates the volume required to settle out the suspended solids in the permanent pool.

Select the WQv to runoff volume ratio ($V_{B/R}$) from Figure 4-26 based on the desired TSS removal efficiency. This ratio must be greater than 4 (MARC, 2008).

For this example, choose a $V_{B/R} = 4$ to meet minimum requirements.

Determine the mean storm depth (S_d) for your region from Table 4-9 or Appendix A.

For Lawrence, $S_d = 0.46 \text{ in}$.

Calculate the total impervious tributary area ($A_{T,I}$) in acres based on equation 4.25.

*For Lawrence, $A_{T,I} = 50 * 0.85 = 42.5 \text{ ac}$.*

Calculate the permanent pool volume (V_{P2}) using equation 4.26.

*For this example, $V_{P2} = (4 * 0.46 * 42.5) / 12 = 6.5 \text{ ac-ft}$*

Permanent Pool Volume (V_{P2})

Choose the volume that is largest between V_{P1} and V_{P2} . This value is the design volume (V_P) for the permanent pool. Add 20-percent to account for sedimentation (multiply V_P by 1.2).

*In this example, $V_p = 1.2 * 6.7 = 8.0$ acre feet.*

Set the desired average permanent pool depth (Z_d) which should be between 4 and 6 feet for non-fish pond. The estimated depth of sediment accumulation over a 5 year period must also be accounted for when specifying total depth during design.

For this pond, the depth will be set at the minimum 4 feet due to the fact that the tributary area is quite small and the pool should maintain a shallow depth to initiate sedimentation and filtration processes.

Calculate the required permanent pool surface area (A_P) using equation 4.27.

The $A_P = (8.0 \text{ ac-ft}) / (4 \text{ ft}) = 2.0 \text{ ac}$

4.8.5.3 Outlet (Step 3)

There are three possible outlet types to use with detention basins. They include single orifice, perforated riser or plate, and V-notch weir. For this example, we will use a perforated riser. If the orifice diameter required to drain the excess to the permanent pool is less than 4 inches, a perforated riser or v-notch weir should be used (MARC, 2008). Refer to Appendix G for equations associated with these calculations.

Water quality depth (Z_{WQ})

Set the depth above the WQ_V outlet (Z_{WQ}) based on facility dimensions for surface area and desired depth.

$Z_{WQ} = 3 \text{ ft}$

Maximum outlet area (A_O) per row of perforations

Calculate the recommended maximum outlet area per row of perforations (A_O) based on the WQ_V and the depth at the basin outlet. A Manning's value (n) of 0.013 was used for this calculation; this will vary by agency. Use equation G.2.

*For this example, $A_O = (4.0 \text{ ac-ft}) / (0.013 * 3^2 + 0.22 * 3 - 0.1) = 5.9 \text{ in}^2$*

Outlet pipe diameter (D_1)

Assume a single column of perforations and calculate the diameter of a single circular perforation (D_1) for each row based on A_O . Use equation G.3.

*$D_1 = ((4 * 5.9 \text{ in}^2) / \pi)^{1/2} = 2.8 \text{ in}$*

Column Number (n_C)

The optimal number of columns of perforations is 1. However, if $D_1 > 2$ inches, then design for more than one column. Keep this number as low as possible.

For this example, D_1 is greater than 2 inches, thus we will design for two columns of perforations.

Perforation diameter (D_{perf})

The circular perforation diameter is found using equation G.4.

For this example, $D_{perf} = ((4 \times 5.9) / (\pi \times 2))^{1/2} = 1.9$ inches.

Horizontal column spacing (S_C)

When $n_C > 1$, the center to center column spacing of perforations, S_C , is 4 inches.

Perforation rows (n_F)

The number of rows is determined using equation G.5 assuming 4 inch center to center vertical spacing between perforations.

In this example, $n_f = (3 \times 12 / 4) = 9$

4.8.5.4 Trash Racks (Step 4)

A trash rack protects outlet structures from damage resulting from trash and debris (4-27 and 4-28 the end of this section). This calculation is based on the outlet type used. For equations see Appendix G.

Outlet Area (A_{OT})

Calculate the outlet area based on the outlet area per perforation row (A_O) and the number of rows (n_F) and number of columns (n_C). Use equation G.11.

For this example, $A_{OT} = (5.9 \text{ in}^2) \times (9 \text{ rows}) \times (2 \text{ columns}) = 106 \text{ in}^2$.

Open Area (A_T)

Calculate the required trash rack open area from the A_{OT} depending on outlet structure type.

For this example, we used a perforated riser and thus will use equation G.12.

$A_T = (106 \text{ in}^2 / 2) \times 77 \times e^{(-0.124 \times 2.8)} = 2911 \text{ square inches}$

4.8.5.5 Forebay (Step 5)

Forebay volume (V_{FB})

The forebay volume should be greater than 10-percent of the WQ_v . Use Equation 4.22.

For this example, V_{FB} must be greater than $0.1 \times (4.0 \text{ ac-ft}) = 0.4 \text{ ac-ft}$.

Forebay depth (Z_{FB})

The forebay depth should be at least 4 feet deep.

Minimum forebay surface area (A_{FB})

Use Equation 4.23 to calculate the minimum surface area of the forebay.

For this example, $A_{FB} = 0.40/4 = 0.10$ ac.

4.8.5.6 Littoral Bench (Step 6)

Littoral bench surface area (A_{LB})

The littoral bench surface area should be between 25-50-percent of the total permanent pool surface area (A_P from Step 2) using *equation 4.34*.

For this example, $A_{LB,MIN} = 0.25(1.98) = 0.5$ acres

$A_{LB,MAX} = 0.5(1.98) = 1.0$ ac.

Littoral bench width (W_{LB})

The minimum and maximum widths can be estimated using *equation 4.35*.

$W_{LB,MIN} = (1/2)((4/\pi)*0.5*43560)^{1/2} = 83.4$ ft $W_{LB,MAX} = (1/2)*((4/\pi)*1*43560)^{1/2} = 118$ ft.*

The bench width, W_{LB} should be within this range of values. For this example, we will choose the average value of 100 feet.

Bench depth (Z_{LB})

The littoral bench depth should be between 6 to 12 inches below the permanent pool surface.

4.8.5.7 Basin Side Slopes (Step 7)

The basin side slopes should be at least 3:1 (H:V) to ensure public safety and maintenance access. Stabilize side slopes with native vegetation.

4.8.5.8 Dam Embankment Side Slopes (Step 7)

- Dam embankment side slopes should be at least 3:1 (H:V) for public safety.
- Embankment soils should be compacted to at least 95 percent of their maximum density according to ASTM D 698-70 (Modified Proctor).
- Embankment slopes should be planted with turf forming grasses.

4.8.5.9 Vegetation (Step 8)

To facilitate stabilization and biological filtration, the basin berms, side slopes, and the littoral bench should be planted with native vegetation.

To determine the appropriate native species, gather the following information about the EWDB site:

- Soil types (soil tests, soil maps in Appendix B)
- Annual precipitation with dates for wet/dry season (Maps in Appendix A)
- Ecoregion and corresponding vegetation (Map and table in Appendix C)
- Previous land use

Provide the soil type, precipitation, previous land use, and ecoregion information to a native vegetation expert for planting suggestions (vegetation types, seeding rates, establishment procedures, maintenance procedures). Use the “typical vegetation” listed in Appendix C as a guideline to check final list. Native vegetation contacts and links are listed in Appendix C.

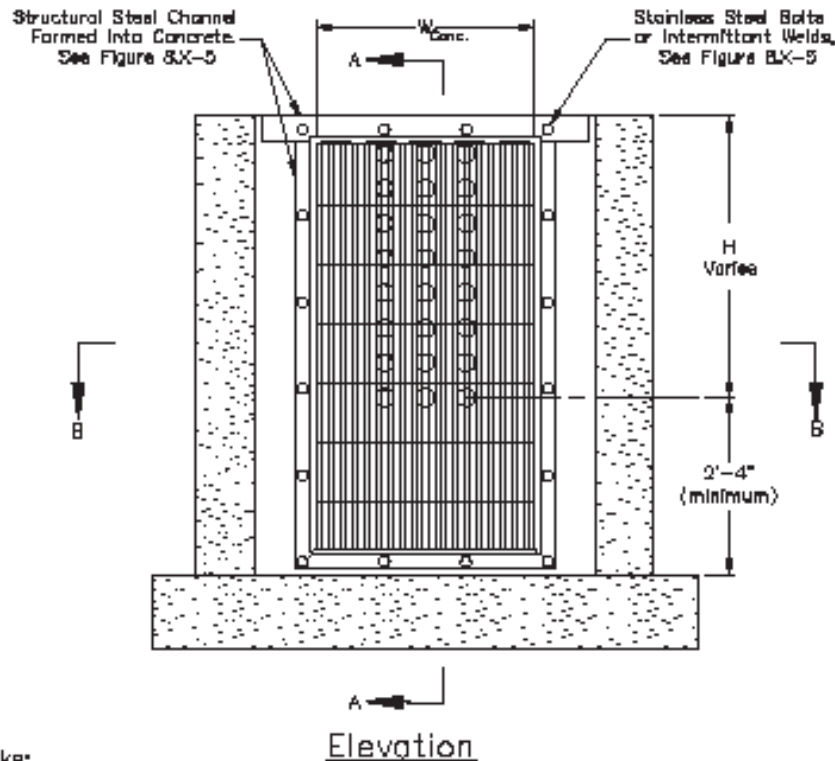
4.8.5.10 Inlet Protection

Dissipate flow energy at basin’s inflow point(s) to limit erosion and promote particle sedimentation.

4.8.5.11 Access

For maintenance purposes, there must be an all-weather access to the bottom, forebay, and littoral bench (UDFCD, 2005). Slopes should not exceed 3:1.

Figure 4-27 WQv Outlet Trash Rack Design (UDFCD, 2005)



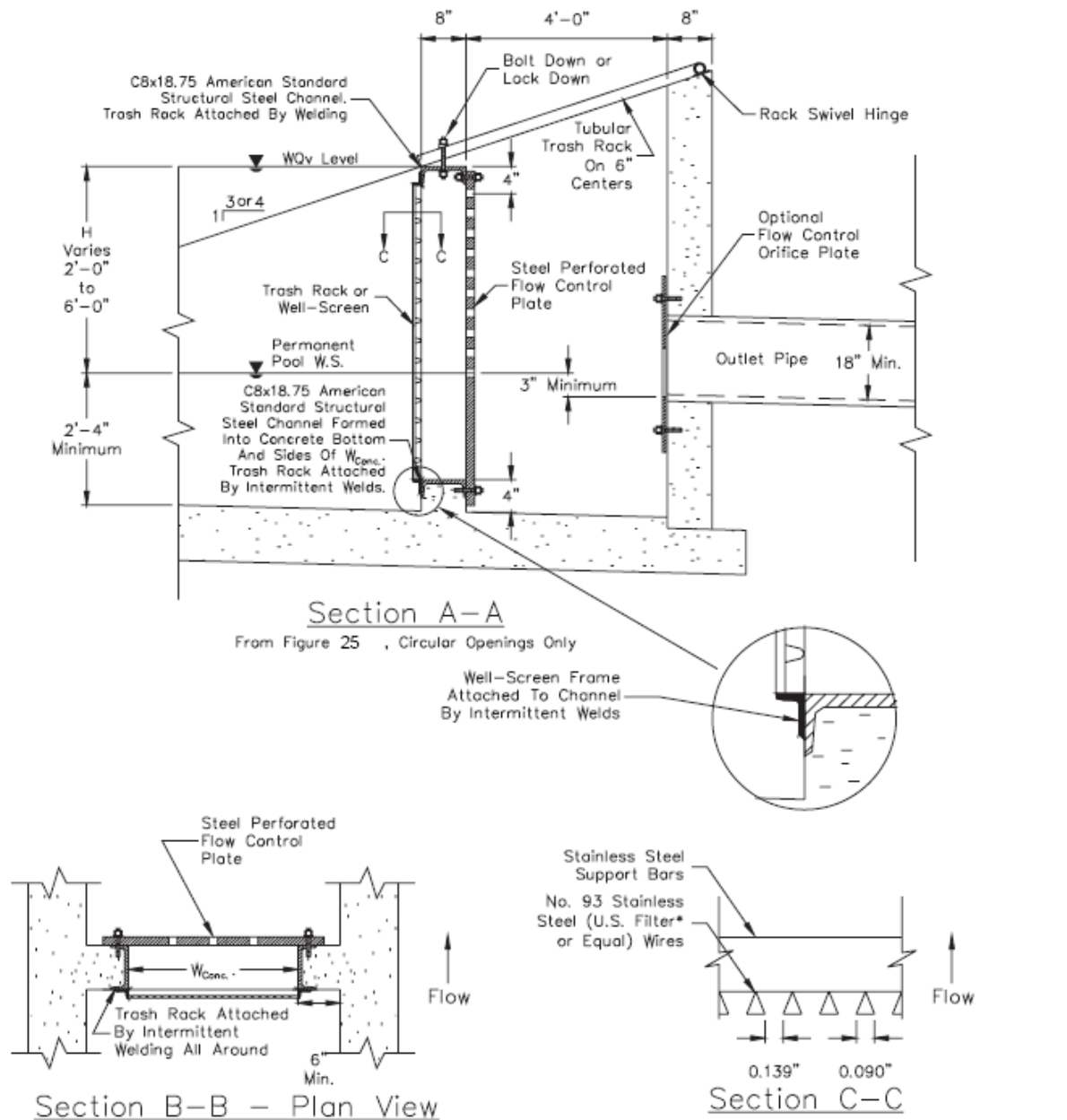
WQv Trash Racks:

1. Well-screen trash racks shall be stainless steel and shall be attached by intermittent welds along the edges of the mounting frame.
2. Bar grate trash racks shall be aluminum and shall be bolted using stainless steel hardware.
3. Trash Rack widths are for specified trash rack material. Finer well-screen or mesh size than specified is acceptable, however, trash rack dimensions need to be adjusted for materials having a different open area/gross area ratio (R value)
4. Structural design of trash rack shall be based on full hydrostatic head with zero head downstream of the rack.

Overflow Trash Racks:

1. All trash racks shall be mounted using stainless steel hardware and provided with hinged and lockable or boltable access panels.
2. Trash racks shall be stainless steel, aluminum, or steel. Steel trash racks shall be hot dip galvanized and may be hot powder painted after galvanizing.
3. Trash Racks shall be designed such that the diagonal dimension of each opening is smaller than the diameter of the outlet pipe.
4. Structural design of trash rack shall be based on full hydrostatic head with zero head downstream of the rack.

Figure 4-28 Alternative WQv Outlet Trash Rack Design (UDFCD, 2005)



Limits for this Standardized Design:

1. All outlet plate openings are circular.
2. Maximum diameter of opening = 2 inches.

*U.S. Filter, St. Paul, Minnesota, USA

$$R \text{ Value} = (\text{net open area}) / (\text{gross rack area}) = 0.60$$

4.8.6 Submittal Requirements

For review purposes prior to construction, the following minimum submittal requirements are recommended:

- Drainage area map, including drainage area to detention basin.
- Existing and proposed contour map of site (1-foot contours recommended).
Compaction requirements should be stated, if required. Additional spot elevations may be helpful.
- Geotechnical investigation of site (soil borings, water table location).
- Stormwater plan/profile for site.
- Detention basin plan view. Components clearly labeled with dimensions.
- Hydrologic calculations (refer to Design Example).
- Detail of control structure (orifice/weir) with dimensions for construction. Include appropriate design calculations (refer to Design Example).
- Velocity downstream of control structure. Appropriate armoring should be specified.
- Vegetation plan with schedule for installation and initial maintenance. Appropriate erosion control measures should be included.
- An as-built survey of the detention basin is recommended to confirm actual construction adheres to approved construction plans. An as-built survey should be required if the detention basin area was also used as a sedimentation basin during the project.
- Long-term inspection/maintenance plan. Permanent pool depth should be inspected annually by survey, with maintenance performed as needed.

4.8.7 References

CASQA. 2003. *California Stormwater Quality Association Stormwater Best Management Practice Handbook*. Available at www.dot.ca.gov/hq/construc/stormwater/manuals.htm

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OMOE-Ontario Ministry of the Environment. 2003. *Stormwater Management Planning and Design Manual*. Queen's Printer for Ontario. Available at www.ene.gov.on.ca/envision/gp/4329eindex.htm

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Section 4 Structural BMPs

4.9 Infiltration Basin

An infiltration basin is a shallow, impounded area designed to collect the WQv for temporary storage and infiltration. Runoff that enters the basin filters through the vegetation and soil, contributing to groundwater recharge. An infiltration basin has components of an extended dry detention basin (EDDB) and an infiltration trench (See Sections 4.4 and 4.9). An infiltration basin is constructed similar to an EDDB, with the exception of that there is no outlet structure to release the WQv. An infiltration basin should be designed for existing site soils and should not be constructed in areas that require an engineered infiltration media. To encourage infiltration and prevent clogging, an infiltration basin utilizes native vegetation. It can also be designed for flood control by providing additional depth above the WQv for detention storage. Key design requirements include location, basin bottom and drainage area slopes, soil types, and basin surface area for infiltration.

Sections from this manual that may need to be referenced for additional information are: Section 2; Section 4.1; Section 5

<i>Location characteristics (Slope, Soil Type)</i>	Drainage Area Slope: < 15% Basin Slope: $\approx$ 0% Soil Type: A, B (Infiltration rate minimum of 0.25 in/hr)
<i>Contributing drainage area</i>	< 5 acres ¹
<i>Design size</i>	Basin dimensions are based on WQv, 3:1 side slopes
<i>Detention time for WQv treatment</i>	48 hrs maximum ²
<i>Pollutant removal efficiencies</i>	90% TSS, 60-90% TP, 55-60% TN ³
<i>Potential for education and outreach</i>	Low
<i>Potential for use with other BMPs</i>	High Should be last BMP in train, pretreatment recommended to reduce sedimentation and dissipate energy
<i>Implementation Category</i>	Short Term: Easy Long Term: Moderate (See Section 5.4.1)
<i>Maintenance</i>	Moderate Sediment/debris removal, vegetation upkeep (See Section 5.4.1)

¹Nashville, 2000, ²CASQA, 2003, ³IA State, 2008

4.9.1 General Application

An infiltration basin treats the WQv by infiltrating stormwater into the subsurface which helps preserve the natural water balance on a site by recharging groundwater and preserving baseflow (IA State, 2008). Infiltration basins are best suited for use in residential subdivisions, small commercial lots, and parking lots. They should not be used to treat highly contaminated runoff or polluted industrial runoff that could pollute groundwater. Any pretreatment technique that induces settling and reduces sedimentation is recommended to prevent clogging. An infiltration basin should be the last stage of a treatment train because it is an infiltration BMP (MARC, 2008). The depth to groundwater must be considered. The base of the infiltration basin must be separated by a minimum of 3 feet from the seasonally high water table or bedrock layer (Metro Council, 2001).

Figure 4-29 shows a typical infiltration basin.

Figure 4-29 Example of an Infiltration Basin



Source: CDM

4.9.2 Advantages and Disadvantages

Advantages	Disadvantages
Simple design, construction, and maintenance	Susceptible to clogging in areas with high sediment load
High suspended solids removal (~90%)	Risk of polluting groundwater if influent is highly contaminated.
Removes fine sediment, trace metals, bacteria, and oxygen-demanding substances	Should not be used where soil infiltration rates are < 0.25 in/hr (Soil Types C, D)
Provides groundwater recharge and preservation of stream baseflow	Cannot treat back-to-back runoff events because of the time to infiltrate the WQv.
Can be designed for flood control	

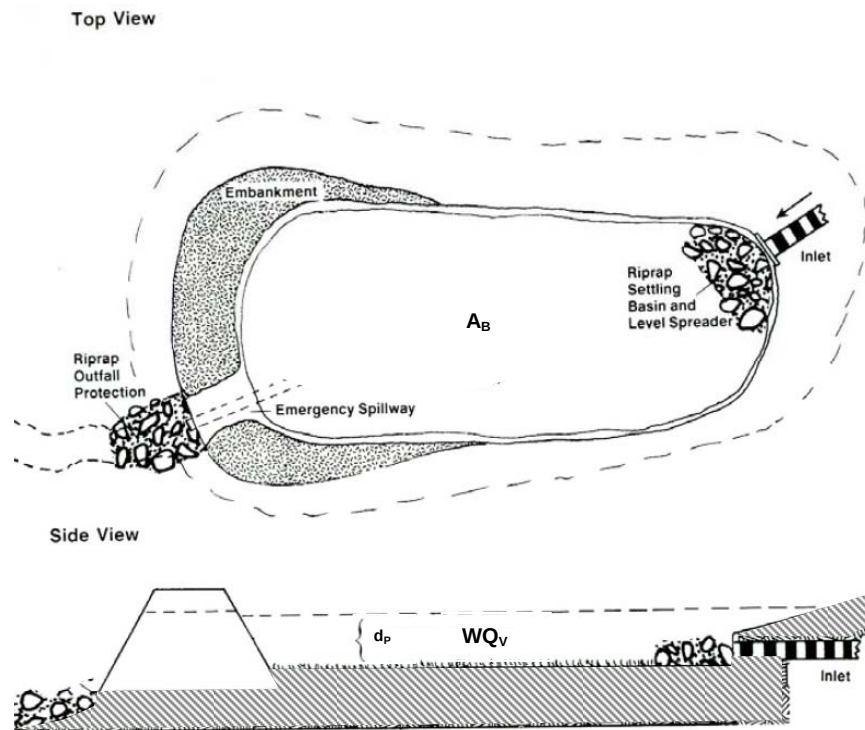
4.9.3 Design Requirements and Considerations

4.9.3.1 Location and Soils

- Infiltration basins should only be constructed in fully developed or stabilized watersheds where potential sediment loads are low.
- Sites constructed of fill, with a baseflow, or with a drainage area slope greater than 15-percent should not be considered for infiltration basins (CASQA, 2003).
- The contributing drainage area to any infiltration basin should be less than five acres to maintain a natural hydrologic balance. It is difficult to infiltrate the runoff from a large drainage area to a small localized area without excessive ponding, therefore increasing risk of infiltration basin failure (Metro Council, 2001).
- Basins shall be located at least 100 feet away from drinking water wells and 25 feet down gradient from buildings (IAState, 2008).
- A geotechnical evaluation of the infiltration basin site should be required prior to construction to verify soil matrix, depth to rock, and depth to water table.
- The underlying soils must have an infiltration rate of at least 0.25 inches per hour. Acceptable soil texture classes are: sand, loamy sand, sandy loam and loam. These soils are in the A or B hydrologic soil group. Basins shall not be constructed on soils in the C or D hydrologic group.
- Site soils should have no greater than 20-percent clay content and less than 40-percent silt/clay content (MDE, 2000).

- The infiltration basin should be at least 3 feet above the seasonal maximum groundwater table or bedrock layer. This minimum distance is required to trap or treat pollutants before they reach the groundwater or bedrock and to maintain vegetation in the basin (Metro Council, 2001).

Figure 4-30 Typical Infiltration Basin Schematic



Adapted from Schueler, 1987

4.9.3.2 Basin Configuration

Pretreatment

- Discharge velocities from inlet or pretreatment devices should be less than 5 feet per second and non-erosive.
- Filtration and settling pretreatment techniques will reduce the clogging potential of the infiltration basin. This pretreatment will help ensure proper functioning of the infiltration basin and allow for larger periods between maintenance (Metro Council, 2001). Such techniques include a vegetated swale, filter strip, sedimentation basin, forebay, settling basin.

Inlet

- Flow into the basin should be unconcentrated to allow even dispersion in the infiltration area. If inlet flow is concentrated, a level spreader or dispersion device is recommended prior to the flow entering the infiltration area.

- Concentrated flow from inflow pipes shall be dissipated by using a rip-rap rock apron or a similar energy dissipation device.
- Incoming velocities should be non-erosive and less than 5 feet per second. Ideally, this velocity should be about 1 foot per second. Use an energy dissipater in high velocity situations.

Basin

- The basin floor should be graded to have a slope near zero to maintain a uniform ponding depth (EPA, 2006).
- A maximum bank side slope of 3:1 is recommended to maintain vegetation (IAState, 2008).
- Basin dimensions should be determined based on the WQv and the maximum ponding depth, d_p . A minimum freeboard of 1 foot is recommended between the maximum ponding depth, d_p , and the top of the bank.
- Provide an emergency overflow spillway to discharge flow above the maximum ponding depth, d_p .
- The maximum infiltration time should be 48 hours or less to maintain aerobic conditions, facilitate plant growth, and prevent mosquito breeding. There should be no permanent pool.
- A maximum ponding depth, d_p , of 3 feet is recommended to maximize soil-water contact and infiltration capacity (IAState, 2008).

Emergency Spillway

Provide an emergency overflow spillway to discharge flow above the maximum ponding depth, d_p . A minimum freeboard of 1 foot is recommended between d_p and the top of the bank.

4.9.3.3 Vegetation

Native vegetation should be used to promote infiltration and reinforce and prevent erosion of basin side slopes and bottom. Utilizing vegetation for pretreatment will filter incoming runoff and may initiate slower velocities. Information about the establishment and maintenance of native vegetation is outlined in Section 5 of this manual.

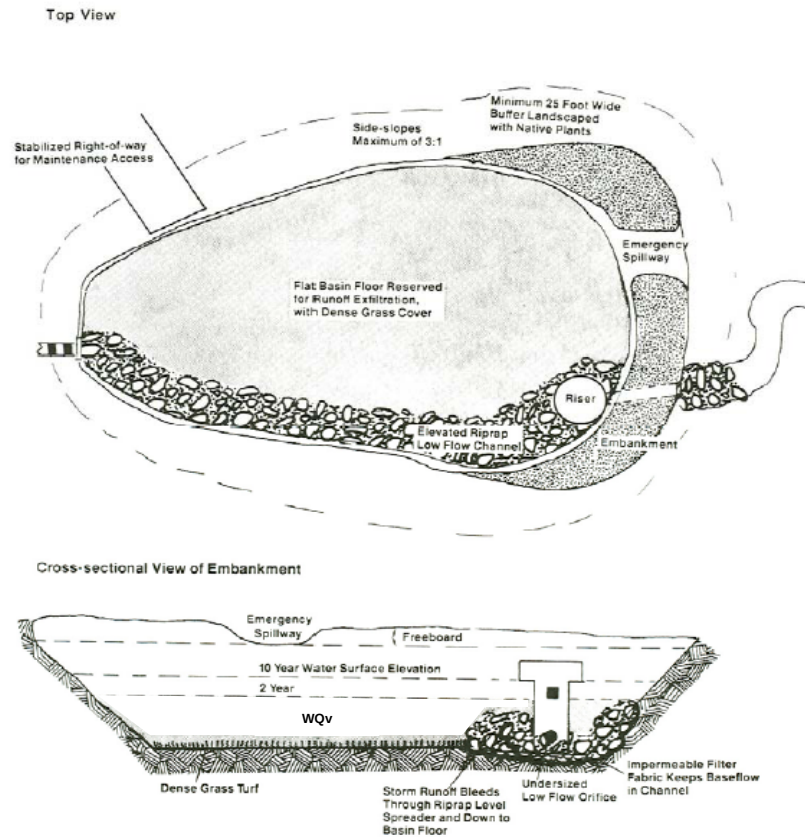
4.9.3.4 Flood Control Design

If designing an infiltration basin for flood control in addition to water quality purposes, follow local agency guidelines for detention basins.

Figure 4-31 is an example design of an infiltration basin that is also used for flood control. When an infiltration basin is designed for water quality and flood control,

consideration must be given to routing events larger than the water quality event through the infiltration basin. A multi stage outlet structure shall be used with the lowest outlet opening set above the WQ_v .

Figure 4-31 Infiltration Basin Designed for Flood Control



Adapted from Schueler, 1987

4.9.4 Design Calculations

A short summary of the design calculations is presented below. A detailed design example is presented in Section 4.9.5.

- **Step 1** Determine WQ_v based on drainage area and regional precipitation information according to Equations 4.1 and 4.2. The WQ_v is the volume of water that must infiltrated into the basin bottom in 48 hours or less.

$$\text{Equation 4.1} \quad R_v = 0.05 + 0.009(I)$$

$$\text{Equation 4.2} \quad WQ_v = \frac{P_{wQ} \times R_v \times A_T}{12}$$

- **Step 2** The minimum basin volume is equal to the WQ_v . Multiply the WQ_v by 1.2 as a factor of safety to account for sedimentation over the design life of the basin as shown in Equation 4.36.

Equation 4.36 Infiltration Basin Design Volume

$$V_B = 1.2 \times WQ_v$$

- **Step 3** Determine the minimum required surface area of the basin bottom using Equation 4.37. All calculations assume infiltration only through the basin bottom.

Equation 4.37 Infiltration Basin Bottom Surface Area

$$A_B = \frac{12 \times V_B}{f \times T_i}$$

Where:

$$\begin{aligned} f &= \text{Soil infiltration rate (inches per hour)} \\ T_i &= \text{Maximum ponding time (hours)} \end{aligned}$$

- **Step 4** Check that the ponding depth, d_p , is within the depth constraints (≤ 3 feet) using Equation 4.38.

Equation 4.38 Infiltration Basin Ponding Depth

$$d_p = \frac{WQ_v}{A_B}$$

- **Step 5** Check that the basin will fit on the given site by calculating the basin length with Equation 4.39. Finalize basin dimensions.

Equation 4.39 Infiltration Basin Length

$$L = \frac{A_B}{W}$$

Where:

$$W = \text{Basin width defined by BMP site location}$$

- **Step 6** Check that inflow to the basin is unconcentrated and non-erosive. If flow is concentrated, a rip-rap apron, level spreader or other flow dispersion device must be used. Energy dissipation is required for sites where velocities will exceed 5 feet per second.
- **Step 7** Provide an emergency overflow spillway to discharge flow above the maximum ponding depth, d_p . A minimum freeboard of 1 foot is recommended between d_p and the top of the bank.

- **Step 8** Install appropriate vegetation using methodology provided by local native vegetation experts. Information about the establishment and maintenance of native vegetation is outlined in Section 5 of this manual.

4.9.5 Design Example

A grocery store in Dodge City, Kansas would like to construct an infiltration basin in the 50 feet by 70 feet area to treat stormwater from a 0.5 acre parking lot (100-percent impervious). The parking lot drains to the area on a 3-percent slope. Soils in this area are classified as B, sandy-loam soils with an average infiltration rate of 0.3 inches per hour. The store owners would like all water infiltrated within 48 hours. A geotechnical investigation determined that the depth to bedrock at the proposed site is 10 feet.

4.9.5.1 Basin Water Quality Volume (Step 1)

Calculate the R_v based on equation 4.1

The tributary area is 100-percent impervious. Thus, $R_v = 0.05 + 0.009(100) = 0.95$.

Calculate the WQ_v based on equation 4.2

For Dodge City, KANSAS, the water quality event is 0.79 inches. $WQ_v = (0.79 \text{ inches} \times 0.95 \times 0.5 \text{ acre}) / 12 \text{ inches} = 0.0313 \text{ acre feet}$.

4.9.5.2 Basin Volume (Step 2)

The minimum basin volume is the WQ_v . To account for possible sedimentation, multiply the WQ_v by a factor of safety of 1.2 using Equation 4.36. $V_B = 1.2 \times 0.0313 \text{ acre feet} = 0.0375 \text{ acre feet}$.

4.9.5.3 Basin Surface Area (Step 3)

Find the minimum required bottom surface area of the basin using Equation 4.37. $A_B = ((12 \text{ inches/foot}) \times (0.0375 \text{ acre feet})) / ((0.3 \text{ inches/hour}) \times (48 \text{ hours})) = 0.03125 \text{ acres}$.

4.9.5.4 Ponding Depth (Step 4)

Use Equation 4.38 to calculate the maximum ponding depth, check that this value is less than 3 feet. $D_p = 0.0313 \text{ acre feet} / 0.03125 \text{ acre} = 1.0 \text{ feet}$.

4.9.5.5 Check Basin Size (Step 5)

Check that the basin will fit onto the site with Equation 4.39. Assume a width of 70 feet. $L = (0.03125 \text{ acre} / 70 \text{ feet}) \times (43560 \text{ square feet/acre}) = 19.5 \text{ feet}$. The basin will fit on the 50 feet x 70 feet site.

4.9.5.6 Inlet (Step 6)

Check that inflow is unconcentrated and non-erosive. If flow is concentrated, a rip-rap apron, level spreader or other flow dispersion device must be used. Energy dissipation is required for sites where velocities will exceed 5 feet per second.

4.9.5.7 Emergency Spillway (Step 7)

Provide an emergency overflow spillway to discharge flows above the maximum ponding depth, d_p . A minimum freeboard of 1 foot is recommended between d_p and the top of the bank.

4.9.5.8 Vegetation (Step 8)

To facilitate stabilization and biological filtration, the basin berms and side slopes should be planted with native vegetation.

To determine the appropriate native species, gather the following information about the infiltration basin site:

- Soil types (soil tests, soil maps in Appendix B, geotechnical evaluation reports)
- Annual precipitation with dates for wet/dry season (Maps in Appendix A)
- Ecoregion and corresponding vegetation (Map and table in Appendix C)
- Previous land use

Provide the soil type, precipitation, previous land use, and ecoregion information to a native vegetation expert for planting suggestions (vegetation types, seeding rates, establishment procedures, maintenance procedures). Use the “typical vegetation” listed in Appendix C as a guideline to check final list. Native vegetation contacts and links are listed in Appendix C.

4.9.6 Submittal Requirements

For review purposes prior to construction, the following minimum submittal requirements are recommended:

- Drainage area map, including drainage area to infiltration basin.
- Existing and proposed contour map of site (1-foot contours recommended).
Restriction of compaction areas should be defined for infiltration basin bottom.
Additional spot elevations may be helpful.
- Geotechnical investigation of site (soil borings, water table location, depth to bed rock).
- Stormwater plan/profile for site (if applicable).
- Infiltration basin plan view. Components clearly labeled with dimensions.
- Hydrologic calculations (refer to Design Example).

- Velocity of stormwater at inlet of infiltration basin, with appropriate details on energy dissipation. If flow is concentrated, details on a level spreader or flow dispersion device should be submitted.
- Vegetation plan with schedule for installation and initial maintenance. Appropriate erosion control measures should be included.
- An as-built survey of the infiltration basin is recommended to confirm actual construction adheres to approved construction plans.
- Long-term inspection/maintenance plan.
- Other requirements as required by local jurisdiction for flood storage beyond water quality event.

4.9.7 References

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Section 5

BMP Inspection and Maintenance

5.1 Importance of BMP Maintenance

Stormwater BMPs are just one component in an agency's infrastructure. Like any other infrastructure installed, continual maintenance is required. Routine pothole repairs on a street are similar to the routine cleaning, weeding and replanting tasks required to maintain a BMP. However, the required skills of field crews are significantly different. A BMP is the water quality component of an agency's stormwater system, and to maintain and improve the quality of stormwater runoff, proper functioning of these BMPs is a necessity.

To aid an agency in inspection and maintenance of their BMP infrastructure, the following subsections have been included in this manual:

- 5.2 Fitting BMPs into the Development "Box"
- 5.3 Delegation of BMP Maintenance Tasks
- 5.4 BMP Maintenance Tasks (schedule, checklists)

5.2 Fitting BMPs into the Development "Box"

Stormwater BMPs are not a typical component of infrastructure. Unlike a street, storm, water, or sanitary installation, a BMP is not a hard-engineered element and thus BMPs do not fit within a defined development process. Typical inspection, acceptance practices, and timelines used by agencies to incorporate infrastructure into their system do not always complement BMP installation processes.

Though each agency will be different, there are two key milestones that are typical to the construction and acceptance process of infrastructure associated with development:

- Final Inspection and Acceptance of Infrastructure Construction (issuance of building and/or occupancy permits)
- Performance and Maintenance Bond Period (typically 2-years)

The definition of these processes may deviate to meet the unique needs of stormwater BMP installation and maintenance.

5.2.1 BMP Construction Timing and Acceptance

A BMP should be the last piece of infrastructure constructed on a site. This is difficult for many development situations because the completion of other infrastructure and/or building construction may not correspond to time periods for optimal

vegetation establishment. Vegetation is a critical component to BMP function, and thus an agency needs to take this into account when looking at a project's schedule. The project schedule should consider that the planting and establishment of vegetation will be most successful in early spring (optimally March-April), resulting in an appropriate vegetation density for withstanding stormwater runoff in the early summer.

Initially, a BMP will require continual inspection and maintenance, similar to what is required for good erosion and sediment control stabilization practices to be successful. Unlike traditional infrastructure acceptance, a BMP cannot be accepted as infrastructure immediately after construction and then left alone. The first three months of vegetation establishment is critical, and this vegetation maintenance on a minimum of a bi-annual basis is key to both short and long-term BMP success. Inspection and maintenance practices, both short and long-term, should be defined by each agency using ordinances and construction specifications. Acceptance requirements of a BMP into an agency's infrastructure system should consist of the completion of the design and construction requirements (Section 4), completion of the three month vegetation establishment period (Section 5.4), and an established schedule for future inspection and maintenance procedures (Section 5.4).

5.2.2 Performance and Maintenance Agreements

An agency also may choose to utilize the practice of requiring a contractor to issue a performance and maintenance bond specifically for BMP construction. This is a very common practice for other types of infrastructure construction. A bond is typically issued for the construction cost of the improvement or a percentage of the construction cost of the improvement. Typically, a contractor can obtain a bond but a developer cannot. An advantage to a bond is it is more in the form of insurance – a separate agency is insuring that the contractor is good for the amount of the bond. A disadvantage to the bonding process is it can be a difficult and lengthy process for an agency to actually get the money defined by the bond, if required. The dollar amount and length of time for a performance and maintenance bond should be determined by an individual agency.

Another option that could be considered to ensure performance and maintenance of a BMP is the establishment of an escrow account. An escrow account can be set up by either a contractor or a developer. An advantage to an escrow account is it provides immediate funding for an agency to draw on should a BMP fail during the defined maintenance period, and if the designated party(s) responsible does not satisfactorily address the issues. A disadvantage is the defined dollar amount of the escrow account must be provided to an agency upfront – this may be difficult financially for a developer or contractor.

Either a maintenance bond or escrow account provides a method for an agency to obtain funds for BMP maintenance should the developer and/or contractor not properly establish or maintain a BMP. What method used and whether an agency

chooses to use this practice are dependent on the ordinances, design criteria, and construction specifications of that particular agency.

5.3 Delegating BMP Maintenance Tasks

Like any piece of public infrastructure, an agency should enact policy ensuring access to and maintenance of a BMP, if needed. An agency should record all inspection and maintenance activities for a BMP, regardless of who is performing it, either using a standard agency issued form, or utilizing a database or infrastructure inventory software package.

5.3.1 Developer/Contractor Responsibilities

It is critical that an agency work with a developer and contractor to ensure proper short-term maintenance of a BMP. Specific details of BMP installation, as well as a short-term maintenance should be defined as part of the construction plan submittal process for agency review. A vital component to short-term maintenance is the prevention and removal of sedimentation that is a result of any adjacent construction that has impacted the BMP prior to the site being fully established.

5.3.2 Non-Professional/Professional

Routine maintenance includes tasks such as weeding, pruning, litter removal, sediment removal, and mowing can be completed by nonprofessionals and may overlap with standard landscaping demands (MARC, 2008). BMP maintenance tasks can be a great way to involve and educate the community to their purpose and function. BMPs have the potential to create a highly interactive environment for community members and volunteers to get involved.

Although a nonprofessional can undertake many maintenance tasks of a BMP effectively, a professional should be consulted periodically to ensure that all needs of the BMP facility are met (NCDENR Stormwater BMP Manual, 2007). This includes inspection of structural components, including outlets and embankments, by a professional engineer and inspection of vegetated components by an appropriate plant professional. Any construction modifications to the BMP should be completed by a trained professional.

Emergency maintenance of a BMP may be required after floods or other extreme wet weather events. These maintenance issues will require coordination between an agency and design professionals to ensure that the BMP infrastructure continues to function as designed.

5.4 BMP Maintenance Tasks

BMP maintenance tasks vary depending on whether the BMP is vegetated. This section will present maintenance task checklists and maintenance and inspection scheduling information for both vegetated BMPs (Section 5.4.1) and non-vegetated BMPs (Section 5.4.2).

BMPs with natural components (vegetation and soils) require a maintenance schedule that evolves with time. Over a course of two to three years, natural components will become established and BMP maintenance tasks will become less frequent and more routine. BMPs without natural components, such as an infiltration trench, require a different maintenance schedule. BMP maintenance tasks are divided into two phases: (1) short-term maintenance and (2) long-term maintenance. Both phases are equally important for the long-term success and function of a BMP.

- **Short-Term Maintenance.** Short-term maintenance tasks are to be completed during construction of the area surrounding the BMP, during construction and establishment of the BMP itself, and approximately the first three months after the BMP is brought online. (Sections 5.4.1.1 and 5.4.2.1)
- **Long-Term Maintenance.** Long-term maintenance tasks should occur bi-annually for the lifetime of the BMP. (Sections 5.4.1.2 and 5.4.2.2)

An example of how BMP construction and initial inspection would be incorporated into a project construction and inspection schedule is shown in Table 5-1. This table also gives a visual representation of continuing bi-annual maintenance inspections that should be completed on each BMP and an approximate time frame in which inspection and maintenance work should occur.

It is important for an agency to document installation, inspection, and maintenance activities on each BMP in their stormwater system. A construction record is recommended (Figure 5-1 and Appendix D.4). This construction record can be formatted similar to Figure 5-1, but key components should include installation date, designer and installer contact information, key inspection and maintenance dates, and any performance and maintenance bond information. Similarly, maintenance inspections should also be documented.

An agency should record all maintenance activities for a BMP, regardless of who is performing it, either using a standard agency issued form, or utilizing a database or infrastructure inventory software package.

Table 5-1 Sample Construction and Long-Term Schedule for Project Construction, BMP Installation, and BMP Maintenance

	Example Construction Schedule												Long Term Schedule											
	Month of Year												Month of Year											
	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8
Project site/Building Construction																								
Project site Stabilization																								
Temporary Stormwater Control at BMP Site																								
BMP Installation & Veg. Establishment																								
Post Wet-Weather Checks																								
Annual Key Milestones-BMP																								
Fall Bi-annual Inspection/Maintenance																								
Spring Bi-annual Inspection/Maintenance																								



Indicates inspection and/or Maintenance Activity (See corresponding checklist)

Figure 5-1 Sample BMP Construction Record

BMP Construction Record	
BMP Number	_____
BMP Type	_____
Designed By	_____
Installation Date	_____
Scheduled 3 Month Inspection Date:	_____ Actual 3 Month Inspection Date: _____
Installed By	_____
Phone	_____
Email	_____
Maintenance Bond or Escrow Account?	_____ Number: _____
Date of Expiration:	_____
Final Inspection	_____
Added to Agency Maintenance Schedule?	_____

Inspection for First Two Growing Seasons:	
1st Fall Inspection Scheduled	_____ Actual 1st Fall Inspection Date: _____
1st Fall Maintenance Completed	_____
1st Spring Inspection Scheduled	_____ Actual 1st Spring Inspection Date: _____
1st Spring Maintenance Completed	_____
2nd Fall Inspection Scheduled	_____ Actual 2nd Fall Inspection Date: _____
2nd Fall Maintenance Completed	_____
2nd Spring Inspection Scheduled	_____ Actual 2nd Spring Inspection Date: _____
2nd Spring Maintenance Completed	_____

5.4.1 Vegetated BMPs

Bioretention facilities, native grass swales, filter strips, and extended wet and dry detention facilities rely on vegetation to improve their hydraulic function. These practices are considered “vegetated BMPs” and have different maintenance requirements than BMPs without vegetation.

5.4.1.1 Short-term

These tasks are to be completed during construction of the area surrounding the BMP, during construction and establishment of the BMP itself, and approximately the first three months after the BMP is brought online. Short-term maintenance tasks are listed on Table 5-2.

Prior to and During Installation and Establishment of BMP

During construction of the areas surrounding the BMP site, take preventative action to limit disturbances such as compacting, land exposure, or pollution. This may be achieved through phased construction to limit the amount of bare soil exposed to erosion and decrease need for erosion control devices. Prior to BMP construction, development of the surrounding areas must be complete. This is to reduce potential for sediment influx to BMP and consequent clogging. For infiltration BMPs such as

bioretention facilities it is critical that excess sediment be removed and measures be taken to prevent excess sediment from entering BMP.

Install BMP vegetation in the early spring (March-April) or according to the guidelines provided by a vegetation expert. Several methods can be utilized to augment grass establishment such as mulching and cover crops to reduce competition for resources and prevent weed growth. Prevent other disturbances, such as human/animal foot traffic, through signage and fencing. Signage can also be used to raise public interest and provide education (see Section 2). Stormwater runoff should be routed away from the BMP for the minimum establishment period of 45 days in order to prevent damage. This will prevent nascent (young) grasses and expensive BMP components from being overwhelmed and/or damaged in wet weather events. Irrigate vegetation as necessary during period that stormwater is routed away from BMP to aid in establishment.

During Three Months Post-Installation

This period is to monitor BMP function during the initial three months after the BMP begins to receive stormwater. Within 24 hours of every stormwater event which results in precipitation of 0.5 inches or greater, inspect BMP to ensure that vegetation and other erosion control mechanisms are intact. Check structures for stability and remove trash and debris. This three month time frame is an opportunity to begin community involvement – they will see the evolution of the BMP. Help establish “green teams” or other community groups to help maintain BMP with weeding and trash removal. During this time it is critical that vegetation be monitored and that dead plants are replaced. Try to maintain at least a 70-percent vegetation density to ensure stability. Continue irrigation to supplement rainfall during dry summer months.

Table 5-2 Short-Term Maintenance Tasks for Vegetated BMP

Short Term Vegetated BMP Maintenance	
Prior to and During Installation and Establishment of BMP	
Task	Explanation
Encourage phased construction of development surrounding BMP	Utilize staged construction to limit erosion potential of land exposed
Provide temporary stormwater control	Stormwater runoff shall be routed around facility until vegetation is established (generally 2-3 months)
Provide site stabilization	Utilize erosion control during construction and until facility is established
Protection from foot traffic and BMP education through signage	Use fencing and signage to prevent damage from animal and human foot traffic and to initiate public interest and education
Planting of native vegetation	Optimum planting window depends on location in KS; For seeding rates and other assistance contact local NRCS
Mulching	Use mulch made from native hay or native plants to reduce potential competition for resources
Fertilization	Typically with native vegetation fertilization is not required, however consult local NRCS for fertilizing suggestions after soils test
Irrigation/Watering	Watering schedule must be established for upkeep of vegetation
During 3 Months Post-Installation	
Post wet-weather event (Precipitation > 0.5")	Ensure that vegetation and other erosion stabilizing mechanisms are intact and check inlet/outlet structures and surrounding area for signs of erosion or instability
Protection from foot traffic and BMP education through signage	Use fencing and signage to prevent damage from animal and human foot traffic and to encourage BMP education and interest
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Irrigation/Watering	Watering schedule must be established for upkeep of vegetation
Weeding	Particularly important during initial growth to reduce competition for moisture, nutrients, and sunlight
Replacement of dead plants	All dead plants should be removed, the cause of their death investigated, and If the cause is the BMP environment, attempt growth of new plant type
Establish "Green Teams" or other community groups	Encourage community involvement and establish maintenance crews to perform routine clean out of trash and debris and to maintain appearance of BMP

5.4.1.2 Long-term

These tasks are to be completed bi-annually according to the vegetation growing season. Tasks to be carried out during these bi-annual inspections will be routine for each year of the BMP's life. Native grasses typically become fully established in two to three growing seasons. The main purpose of these inspections is to assess the BMP condition, and remedy functional and vegetation issues identified. Long-term maintenance tasks are listed on Table 5-3.

Fall Inspection - End of Growing Season (August-September)

The timing of this inspection should correspond to the tapering of vegetation growth in early fall. At this time, the vegetation should be harvested to retain the maximum nutrient value. Clip or mow vegetation to a minimum of 4-6 inches. Retain 4-6 inches of stalk to ensure winter survival and maintenance of the root systems. General clean up of the plant bed should also occur at this time to remove dead plants and invasive species. Other landscaping may be required to maintain the aesthetic condition of the BMP over the winter.

Spring Inspection-Beginning of Growing Season (March-April)

The Spring Inspection should occur at the beginning of the spring season before vegetation growth. Landscaping duties include replacing and augmenting existing vegetation. Winter weather will warrant a general clean up of the BMP to maintain aesthetics. Clean out trash and debris and clean up educational signs. This would be an optimum time for "Green teams" and active community members to help tidy the BMP site.

Common Inspection Items for Both Fall and Spring

A professional inspection should occur once a year at either the Fall or Spring inspection to assess the functional condition of the BMP. BMP structures such as dams, embankments, inlets, and outlets should be assessed for stability and function. Ways to assess BMP function include checking for standing water, sediment accumulation, and signs of erosion. Sediment should be removed from the BMP when the ground surface is completely dry. Removing sediment when the BMP is wet may cause compaction.

Check areas surrounding the BMP for signs of erosion or instability. Also make sure that aesthetics are maintained throughout the BMP footprint. Trees and other large vegetation should be removed to prevent lateral damage to the BMP via root growth. Shade-producing vegetation is not desirable in a BMP with grasses.

Table 5-3 Long-Term Maintenance Tasks for Vegetated BMP

Long Term Vegetated BMP Maintenance	
End of Growing Season (August - September)	
Task	Explanation
General Inspection	Check for standing water, slope stability, sediment accumulation, trash and debris, presence of burrows and erosion, and integrity of inlet/outlet, dam, and other engineered structures
Clean out sediments and debris	Clean out sediments and debris from inlet, outlet, the BMP and for detention basins, remove sediment when accumulation reduces the permanent pool by 10-percent or the forebay by 50-percent and dispose of appropriately
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Mowing/Harvest	Native grasses should be trimmed to 4-6" to provide adequate biomass for regrowth the following year
Maintain BMP Signage	Repairs should be made to signage, walkways, picnic tables, or any other public recreation equipment as necessary
Winter stabilization	May be necessary to establish erosion prevention practices to maintain BMP over the winter when plants are dormant
Continue to support and educate "Green Teams" or other community groups	It is important to maintain community involvement and provide education and opportunities for service
Beginning of Growing Season (March-April)	
General Inspection	Check for standing water, slope stability, sediment accumulation, trash and debris, presence of burrows and erosion, and integrity of inlet/outlet, dam, and other engineered structures
Clean out sediments and debris	Clean out sediments and debris from inlet, outlet, the BMP and for detention basins, remove sediment when accumulation reduces the permanent pool by 10-percent or the forebay by 50-percent and dispose of appropriately
Provide site stabilization	Ensure that vegetation and other erosion stabilizing mechanisms are intact
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Weeding/Pruning	Remove invasive and excess biomass and dispose of appropriately.
Replace/augment vegetation	Augment existing plants by same planting procedure as during construction if necessary and dead plants should be removed and replaced
Continue to support and educate "Green Teams" or other community groups	It is important to maintain community involvement and provide education and opportunities for service

5.4.2 Non-Vegetated BMPs

Infiltration trenches and other non-vegetated BMPs have no living components. These BMPs are similar to traditional stormwater systems, and thus don't require as much maintenance as vegetated BMPs. However, their stormwater capacity will be the best on the first day, whereas vegetated BMPs have the potential to become more efficient systems with time. The use of pretreatment BMPs will significantly reduce maintenance requirements of non-vegetated BMPs (Barr Engineering, 2001). Non-vegetated BMPs can be put into service right after construction (assuming tributary drainage area is stabilized) because no time is needed to establish BMP vegetation.

For practical purposes, non-vegetated maintenance tasks are broken down into two main phases similar to vegetated BMPs: (1) short-term maintenance and (2) long-term maintenance. Both phases are equally important for the long-term success and function of a BMP.

5.4.2.1 Short-term

These tasks are to be completed during construction of the area surrounding the BMP, during construction of the BMP itself, and approximately the first three months after the BMP is brought online. Short-term maintenance tasks are listed on Table 5-4.

Prior to and During Installation of BMP

During construction of the areas surrounding the BMP site, take preventative action to limit disturbances such as compacting, land exposure, or pollution. This may be achieved through phased construction, which limits the amount of bare soil exposed to erosion. Prior to BMP construction, all tributary area must be stabilized. This is to reduce potential for sediment influx to BMP and consequent clogging. For infiltration BMPs such as infiltration trenches, it is critical that the excess sediment load be eliminated.

During Three Months Post-Installation

Once the BMP has gone online, inspections should occur within 24 of every storm event which results in precipitation of 0.5 inches or greater to ensure proper stabilization and function. Water levels in observation wells should be checked at these times to ensure infiltration through the BMP matrix profile. Ponding within the trench or high levels of water in the observation well may indicate clogging in the trench bottom. Failure in infiltration trenches is most often caused by clogging in the BMP surface and is indicated by visible ponded water. When ponding occurs at the surface or in the trench, corrective maintenance is required immediately. Structures should be checked for stability and any trash and debris removed.

This three month time frame is an opportunity to begin community involvement – they will see the evolution of the BMP. Help establish “green teams” or other community groups to help maintain BMP with weeding and trash removal.

Table 5-4 Short-Term Maintenance Tasks for Non-Vegetated BMP

Short Term Non-Vegetated BMP Maintenance	
Prior to and During Installation of BMP	
Task	Explanation
Encourage phased construction of development surrounding BMP	Utilize staged construction to limit erosion potential of land exposed
Provide site stabilization	Utilize erosion control during construction and until facility is established
Encourage infiltration through BMP bottom into surrounding soil	Roto-till the bottom soil to increase potential for deep percolation
Protection from foot traffic and BMP education through signage	Use fencing and signage to prevent damage from animal and human foot traffic and to initiate public interest and education
During 3 Months Post-Installation	
Post wet-weather event (Precipitation > 0.5")	Ensure erosion stabilizing mechanisms are intact and check inlet/outlet structures and surrounding area for signs of erosion or instability
Prevent surface clogging	Remove surface debris (grass clippings, sediment, etc.) and monitor ponding
Monitor internal clogging	Check levels of well to ensure proper infiltration from BMP to surrounding soil
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Protection from foot traffic and BMP education through signage	Use fencing and signage to prevent damage from animal and human foot traffic and to encourage BMP education and interest
Establish "Green Teams" or other community groups	Encourage community involvement and establish maintenance crews to perform routine clean out of trash and debris and to maintain appearance of BMP

5.4.2.2 Long-Term

For non-vegetated BMPs the long-term maintenance schedule should follow the same schedule as for vegetated BMPs. Tasks to be carried out during these bi-annual inspections will be routine for each year of the BMPs life. The main purpose of these inspections is to assess the BMP condition and remedy functional issues. Functional issues are typically caused by clogging. Long-term maintenance tasks are listed on Table 5-5.

Fall Inspection - End of Growing Season (August-September)

A professional inspection should occur to assess the condition of the BMP. The inspector should check for standing water, slope stability, sediment accumulation, trash and debris, and signs of erosion. Sediment should be removed from the surface of the BMP when the surrounding ground surface is completely dry. Removing sediment when the BMP is wet may cause compaction.

At this time, check for signs of clogging. Internal clogging can be observed via an observation well. Ponding of surface water 24 hours after a rain event could indicate surface clogging. If the clogging appears to be only at the surface, it may be necessary to remove surface material and replace filter material. Clogging inside the trench (water in observation well for longer than 24 hours) may require complete excavation and replacement of bed material. Remove sediment accumulated at the bottom of BMP, repair base as necessary, and then replace filter material.

Check areas surrounding the BMP for signs of erosion or instability. Also make sure that aesthetics are maintained throughout the BMP footprint. Trees and other large vegetation should be removed to prevent lateral damages caused by roots. At this time it may be necessary to establish erosion prevention practices to maintain the BMP when soils become frozen and surface materials may freeze

Spring Inspection-Beginning of Growing Season (March-April)

A professional inspection should be completed during the spring maintenance period if the annual professional inspection was not fulfilled during the fall maintenance period. Winter weather will warrant a general clean up of the BMP and surrounding areas to maintain aesthetics. Clean out trash and debris and clean up educational signs. This would be an optimum time for “Green Teams” and active community members to help tidy the BMP site.

Check areas surrounding the BMP for signs of erosion or instability. Also make sure that aesthetics are maintained throughout the BMP footprint. Trees and other large vegetation should be removed to prevent lateral damages.

Table 5-5 Long-Term Maintenance Tasks for Non-Vegetated BMP

Long Term Non-Vegetated BMP Maintenance	
End of Growing Season (August - September)	
Task	Explanation
General Inspection	Check for standing water, slope stability, sediment accumulation, trash and debris, presence of burrows and erosion, and integrity of inlet/outlet, dam, and other engineered structures
Clean out sediments and debris	Clean out sediments and debris from surface and check for signs of ponding or clogging
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Maintain BMP Signage	Repairs should be made to signage, walkways, picnic tables, or any other public recreation equipment as necessary
Winter stabilization	May be necessary to establish erosion prevention practices to maintain BMP when soils become frozen and surface materials may freeze
Continue to support and educate "Green Teams" or other community groups	It is important to maintain community involvement and provide education and opportunities for service
Beginning of Growing Season (March-April)	
General Inspection	Check for standing water, slope stability, sediment accumulation, trash and debris, presence of burrows and erosion, and integrity of inlet/outlet, dam, and other engineered structures
Prevent surface clogging	Remove surface debris (grass clippings, sediment, etc.) and monitor ponding
Monitor internal clogging	Check levels of well to ensure proper infiltration from BMP to surrounding soil
Clean out sediments and debris	Clean out sediments and debris from surface and check for signs of ponding or clogging
Provide site stabilization	Ensure that BMP media and other erosion stabilizing mechanisms are intact
Maintain aesthetics	General clean up of the BMP and surrounding areas to maintain aesthetics
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint,
Continue to support and educate "Green Teams" or other community groups	It is important to maintain community involvement and provide education and opportunities for service

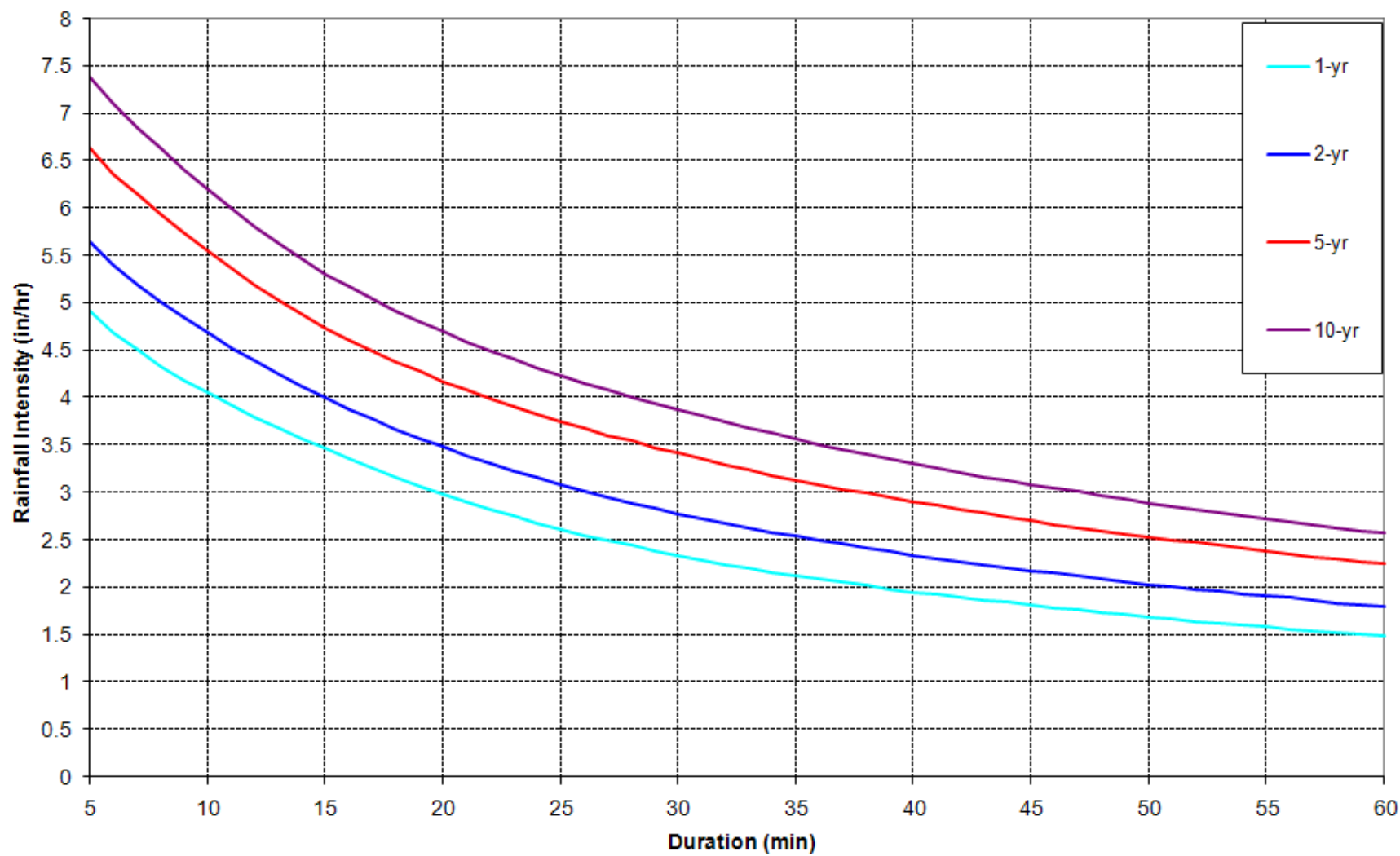


Arkansas City, Kansas									
Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.27	1.66	4.91	5.64	6.64	7.38	8.48	9.34	10.2
6	1.27	1.66	4.69	5.4	6.37	7.1	8.17	9.01	9.84
7	1.25	1.63	4.5	5.19	6.15	6.85	7.89	8.71	9.53
8	1.21	1.58	4.33	5.01	5.94	6.63	7.64	8.43	9.22
9	1.17	1.53	4.18	4.84	5.74	6.41	7.39	8.16	8.93
10	1.13	1.47	4.05	4.68	5.56	6.2	7.15	7.9	8.64
11	1.09	1.42	3.92	4.53	5.38	6	6.92	7.64	8.36
12	1.05	1.38	3.79	4.39	5.2	5.81	6.69	7.39	8.09
13	1.02	1.33	3.68	4.25	5.04	5.63	6.49	7.16	7.83
14	0.99	1.29	3.56	4.12	4.89	5.46	6.3	6.95	7.61
15	0.96	1.25	3.46	4	4.75	5.31	6.12	6.76	7.4
16	0.93	1.21	3.35	3.88	4.62	5.17	5.96	6.59	7.21
17	0.90	1.17	3.25	3.77	4.5	5.04	5.82	6.43	7.05
18	0.87	1.14	3.16	3.67	4.39	4.91	5.69	6.29	6.89
19	0.85	1.11	3.06	3.57	4.28	4.8	5.56	6.16	6.75
20	0.83	1.08	2.98	3.48	4.18	4.7	5.44	6.03	6.61
21	0.81	1.05	2.9	3.39	4.09	4.59	5.33	5.91	6.49
22	0.79	1.02	2.82	3.31	4	4.5	5.23	5.8	6.37
23	0.77	1.00	2.75	3.23	3.92	4.41	5.13	5.69	6.25
24	0.75	0.98	2.68	3.16	3.83	4.32	5.03	5.59	6.14
25	0.73	0.95	2.61	3.08	3.76	4.24	4.94	5.49	6.04
26	0.71	0.93	2.55	3.02	3.68	4.16	4.86	5.4	5.94
27	0.70	0.91	2.49	2.95	3.61	4.09	4.77	5.31	5.84
28	0.68	0.89	2.44	2.89	3.55	4.01	4.69	5.22	5.74
29	0.67	0.88	2.38	2.84	3.48	3.94	4.61	5.13	5.65
30	0.66	0.86	2.34	2.78	3.42	3.88	4.53	5.05	5.56
31	0.64	0.84	2.29	2.73	3.36	3.81	4.46	4.97	5.47
32	0.63	0.83	2.24	2.68	3.3	3.75	4.39	4.89	5.39
33	0.62	0.81	2.2	2.63	3.25	3.69	4.32	4.81	5.3
34	0.61	0.80	2.16	2.58	3.19	3.63	4.25	4.74	5.22
35	0.60	0.78	2.12	2.54	3.14	3.57	4.19	4.67	5.14
36	0.59	0.77	2.09	2.5	3.09	3.51	4.12	4.6	5.07
37	0.58	0.75	2.05	2.46	3.04	3.46	4.06	4.53	4.99
38	0.57	0.74	2.02	2.42	3	3.41	4	4.46	4.92
39	0.56	0.73	1.98	2.38	2.95	3.36	3.94	4.4	4.85
40	0.55	0.72	1.95	2.34	2.91	3.31	3.89	4.34	4.78
41	0.54	0.71	1.92	2.31	2.87	3.26	3.83	4.28	4.72
42	0.53	0.70	1.89	2.27	2.83	3.22	3.78	4.22	4.65
43	0.53	0.69	1.86	2.24	2.79	3.17	3.73	4.16	4.59
44	0.52	0.68	1.84	2.21	2.75	3.13	3.68	4.1	4.53
45	0.51	0.67	1.81	2.18	2.71	3.09	3.63	4.05	4.47
46	0.50	0.66	1.78	2.15	2.67	3.05	3.58	4	4.41
47	0.50	0.65	1.76	2.12	2.64	3.01	3.54	3.95	4.36
48	0.49	0.64	1.73	2.09	2.6	2.97	3.49	3.9	4.3
49	0.48	0.63	1.71	2.06	2.57	2.93	3.45	3.85	4.25
50	0.48	0.62	1.69	2.03	2.54	2.89	3.4	3.8	4.2
51	0.47	0.62	1.67	2.01	2.51	2.86	3.36	3.76	4.15
52	0.47	0.61	1.64	1.98	2.48	2.82	3.32	3.71	4.1
53	0.46	0.60	1.62	1.96	2.45	2.79	3.28	3.67	4.05
54	0.45	0.59	1.6	1.93	2.42	2.76	3.25	3.63	4.01
55	0.45	0.59	1.58	1.91	2.39	2.73	3.21	3.59	3.96
56	0.44	0.58	1.56	1.89	2.36	2.69	3.17	3.55	3.92
57	0.44	0.57	1.54	1.86	2.33	2.66	3.14	3.51	3.87
58	0.43	0.57	1.52	1.84	2.31	2.63	3.1	3.47	3.83
59	0.43	0.56	1.51	1.82	2.28	2.6	3.07	3.43	3.79
60	0.42	0.55	1.49	1.8	2.26	2.58	3.04	3.39	3.75

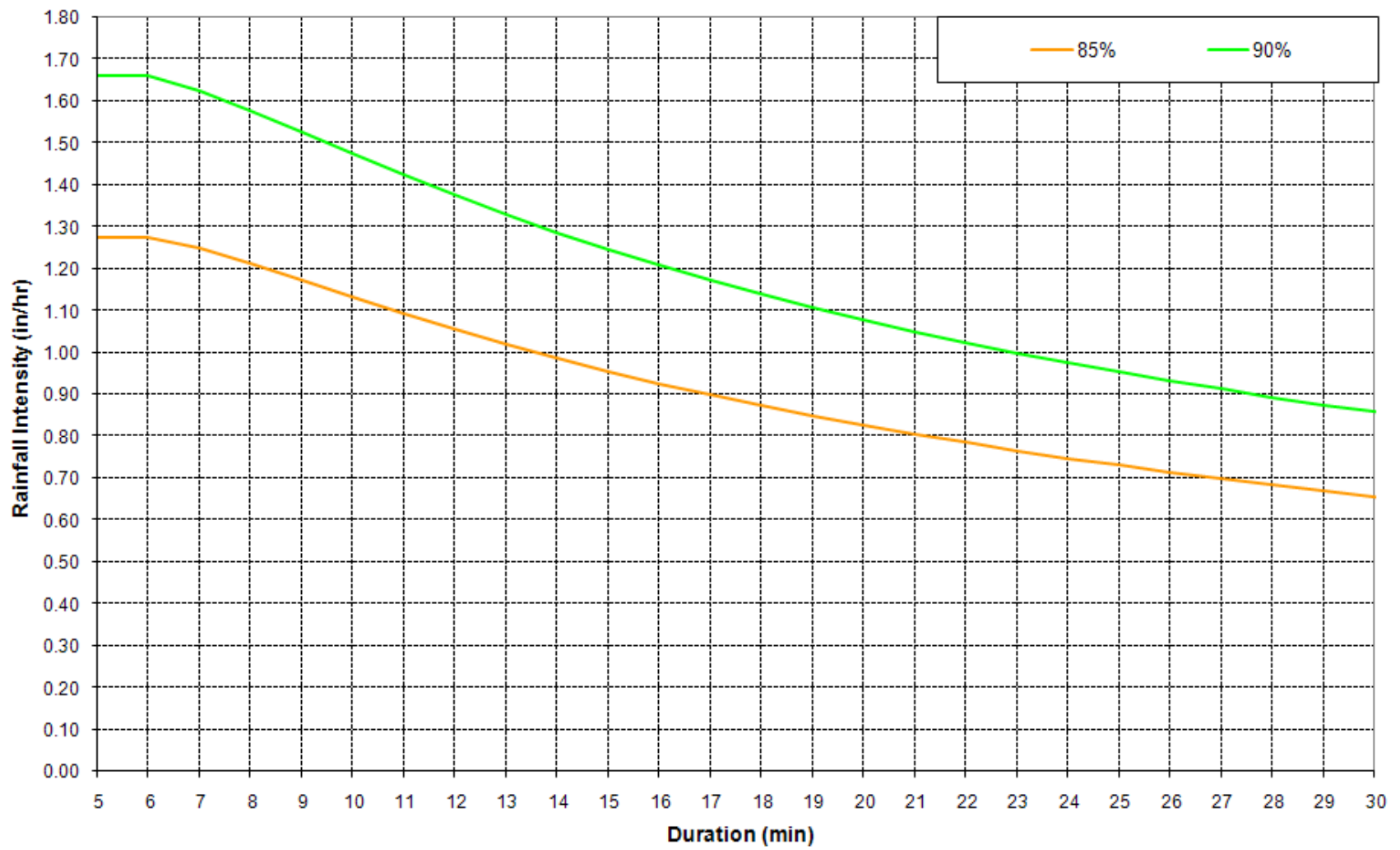
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Arkansas City, Kansas



Arkansas City, Kansas

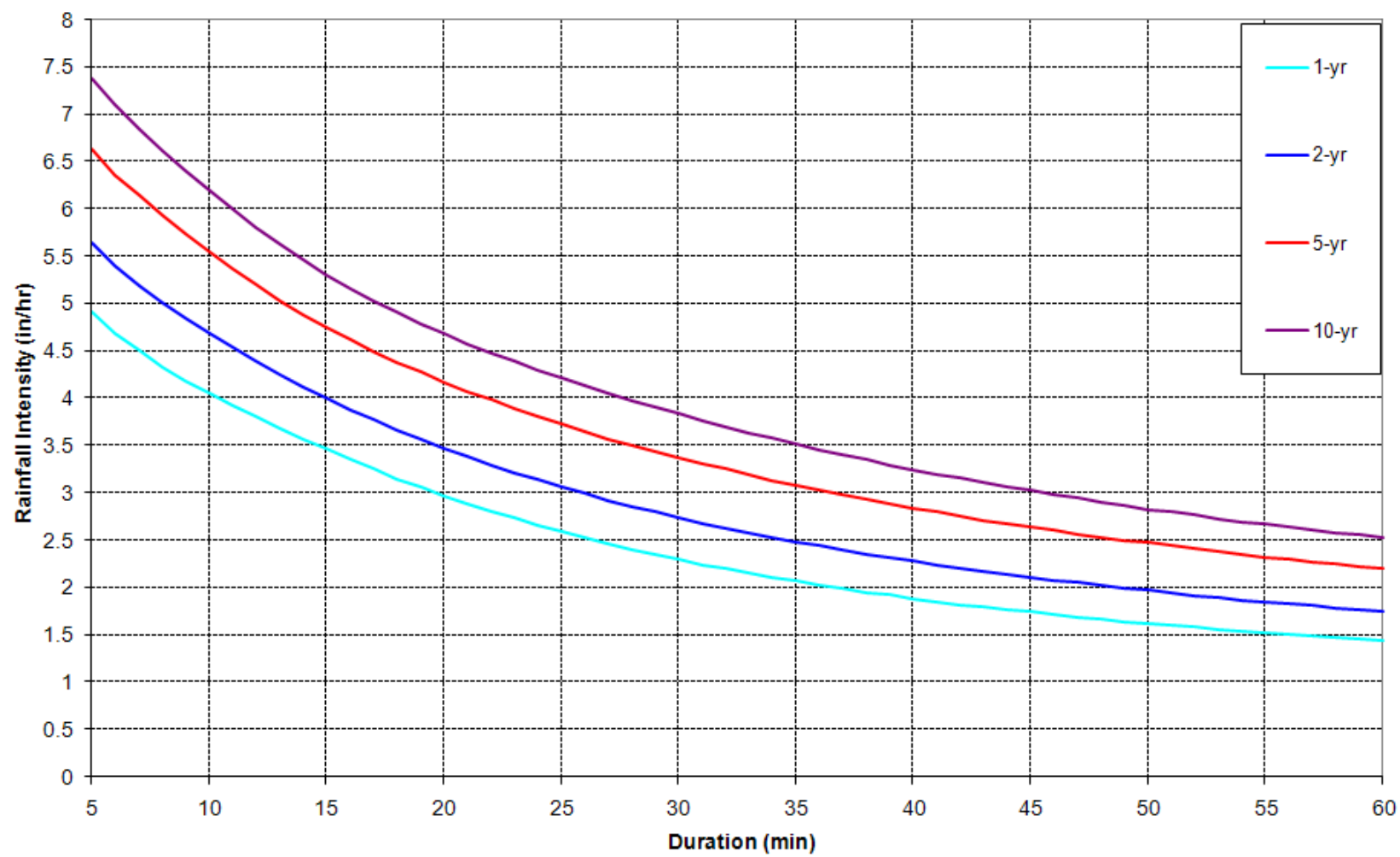


Coffeyville, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.52	2.08	4.91	5.64	6.64	7.38	8.48	9.34	10.2
6	1.52	2.08	4.69	5.4	6.37	7.1	8.17	9.01	9.84
7	1.49	2.03	4.5	5.19	6.15	6.85	7.89	8.71	9.52
8	1.45	1.97	4.33	5.01	5.94	6.62	7.64	8.43	9.22
9	1.40	1.91	4.18	4.84	5.74	6.41	7.39	8.16	8.93
10	1.35	1.84	4.05	4.68	5.56	6.2	7.15	7.9	8.64
11	1.31	1.78	3.92	4.53	5.38	6	6.92	7.64	8.36
12	1.26	1.72	3.8	4.39	5.21	5.81	6.7	7.39	8.09
13	1.22	1.66	3.68	4.25	5.04	5.63	6.49	7.16	7.84
14	1.18	1.61	3.57	4.12	4.89	5.46	6.3	6.95	7.61
15	1.14	1.56	3.46	4	4.75	5.31	6.12	6.76	7.4
16	1.11	1.51	3.35	3.88	4.62	5.16	5.96	6.59	7.21
17	1.07	1.47	3.25	3.77	4.5	5.03	5.82	6.43	7.04
18	1.04	1.42	3.15	3.67	4.38	4.91	5.68	6.28	6.88
19	1.02	1.38	3.06	3.57	4.28	4.79	5.55	6.15	6.74
20	0.99	1.35	2.97	3.47	4.17	4.69	5.43	6.02	6.6
21	0.96	1.31	2.89	3.38	4.08	4.58	5.32	5.9	6.47
22	0.94	1.28	2.81	3.29	3.99	4.48	5.21	5.78	6.35
23	0.92	1.25	2.73	3.21	3.9	4.39	5.11	5.67	6.23
24	0.89	1.22	2.66	3.14	3.81	4.3	5.01	5.57	6.12
25	0.87	1.19	2.59	3.06	3.73	4.22	4.92	5.47	6.01
26	0.85	1.17	2.52	2.99	3.66	4.14	4.83	5.37	5.91
27	0.84	1.14	2.46	2.92	3.58	4.06	4.74	5.27	5.8
28	0.82	1.12	2.4	2.86	3.51	3.98	4.66	5.18	5.71
29	0.80	1.09	2.35	2.8	3.45	3.91	4.57	5.09	5.61
30	0.79	1.07	2.3	2.74	3.38	3.84	4.5	5.01	5.52
31	0.77	1.05	2.24	2.68	3.32	3.77	4.42	4.93	5.43
32	0.76	1.03	2.2	2.63	3.26	3.7	4.35	4.85	5.34
33	0.74	1.01	2.15	2.58	3.2	3.64	4.27	4.77	5.26
34	0.73	0.99	2.11	2.53	3.14	3.58	4.2	4.69	5.18
35	0.72	0.98	2.07	2.48	3.09	3.52	4.14	4.62	5.09
36	0.70	0.96	2.03	2.44	3.04	3.46	4.07	4.55	5.02
37	0.69	0.94	1.99	2.4	2.99	3.41	4.01	4.48	4.94
38	0.68	0.93	1.95	2.35	2.94	3.35	3.95	4.41	4.87
39	0.67	0.91	1.92	2.31	2.89	3.3	3.89	4.34	4.8
40	0.66	0.90	1.88	2.28	2.85	3.25	3.83	4.28	4.73
41	0.65	0.88	1.85	2.24	2.81	3.2	3.77	4.22	4.66
42	0.64	0.87	1.82	2.2	2.76	3.16	3.72	4.16	4.6
43	0.63	0.86	1.79	2.17	2.72	3.11	3.67	4.1	4.53
44	0.62	0.85	1.76	2.14	2.68	3.07	3.62	4.05	4.47
45	0.61	0.83	1.74	2.11	2.65	3.03	3.57	3.99	4.41
46	0.60	0.82	1.71	2.08	2.61	2.99	3.52	3.94	4.35
47	0.59	0.81	1.69	2.05	2.57	2.95	3.48	3.89	4.3
48	0.59	0.80	1.66	2.02	2.54	2.91	3.43	3.84	4.24
49	0.58	0.79	1.64	1.99	2.51	2.87	3.39	3.79	4.19
50	0.57	0.78	1.62	1.97	2.48	2.83	3.35	3.74	4.14
51	0.56	0.77	1.6	1.94	2.45	2.8	3.31	3.7	4.09
52	0.56	0.76	1.58	1.92	2.42	2.77	3.27	3.65	4.04
53	0.55	0.75	1.56	1.89	2.39	2.73	3.23	3.61	4
54	0.54	0.74	1.54	1.87	2.36	2.7	3.19	3.57	3.95
55	0.54	0.73	1.52	1.85	2.33	2.67	3.15	3.53	3.9
56	0.53	0.72	1.5	1.83	2.31	2.64	3.12	3.49	3.86
57	0.52	0.71	1.49	1.81	2.28	2.61	3.08	3.45	3.82
58	0.52	0.71	1.47	1.79	2.26	2.58	3.05	3.42	3.78
59	0.51	0.70	1.45	1.77	2.23	2.56	3.02	3.38	3.74
60	0.51	0.69	1.44	1.75	2.21	2.53	2.99	3.34	3.7

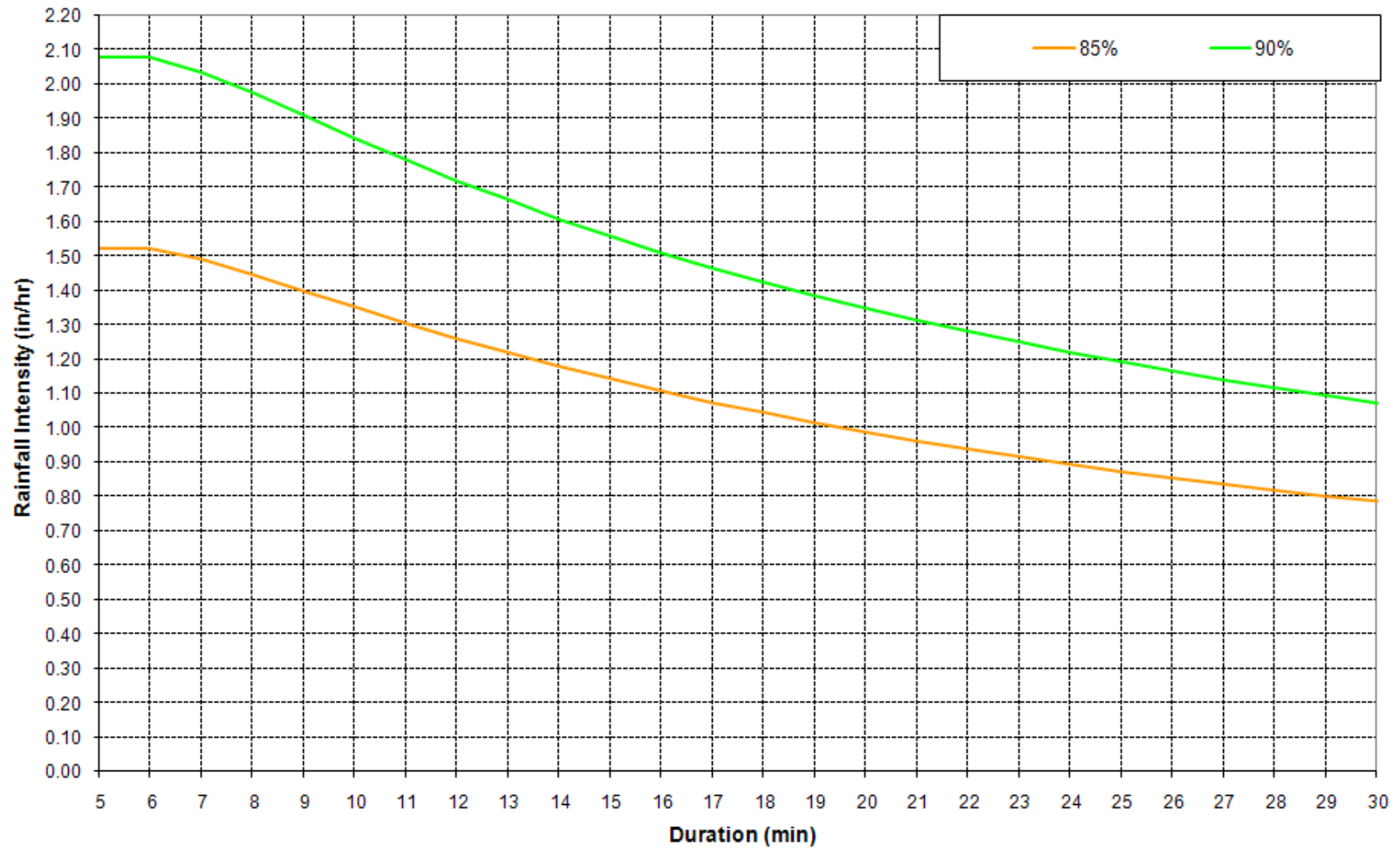
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² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Coffeyville, Kansas



Coffeyville, Kansas

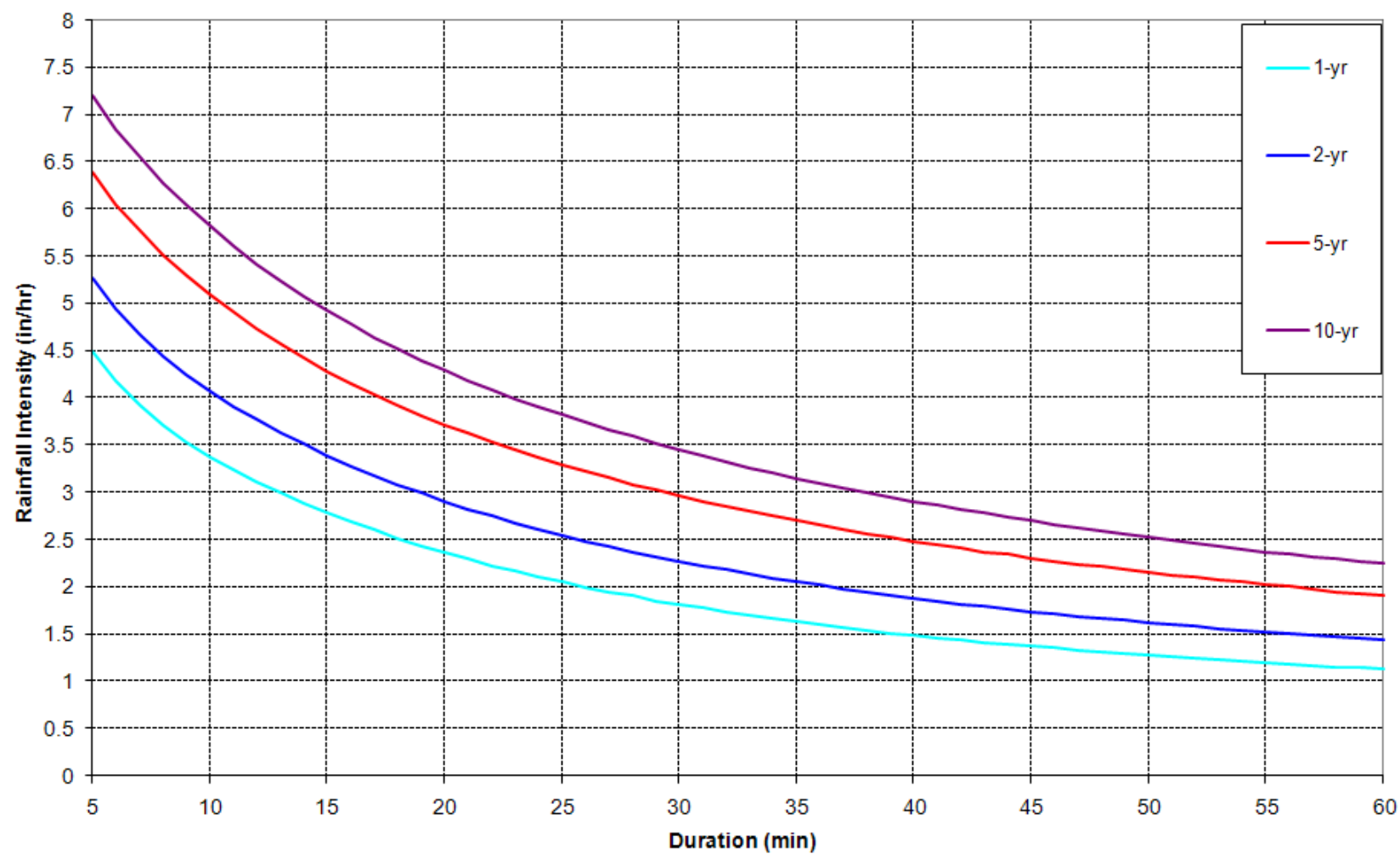


Dodge City, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	0.80	1.09	4.49	5.28	6.39	7.2	8.37	9.29	10.2
6	0.80	1.09	4.18	4.95	6.05	6.84	7.99	8.88	9.77
7	0.79	1.07	3.92	4.68	5.77	6.55	7.66	8.54	9.41
8	0.76	1.04	3.71	4.45	5.52	6.28	7.37	8.23	9.07
9	0.74	1.01	3.54	4.26	5.3	6.04	7.11	7.94	8.76
10	0.71	0.97	3.38	4.08	5.1	5.82	6.86	7.66	8.46
11	0.69	0.94	3.24	3.92	4.91	5.61	6.62	7.4	8.17
12	0.66	0.91	3.12	3.78	4.74	5.42	6.39	7.15	7.9
13	0.64	0.88	3	3.64	4.58	5.24	6.19	6.92	7.65
14	0.62	0.85	2.89	3.52	4.43	5.07	5.99	6.71	7.42
15	0.60	0.82	2.79	3.4	4.29	4.92	5.81	6.51	7.2
16	0.58	0.80	2.7	3.29	4.16	4.78	5.65	6.33	7
17	0.57	0.77	2.61	3.19	4.04	4.64	5.49	6.16	6.81
18	0.55	0.75	2.52	3.09	3.93	4.52	5.35	6	6.64
19	0.54	0.73	2.44	3	3.82	4.4	5.21	5.85	6.48
20	0.52	0.71	2.37	2.91	3.72	4.29	5.09	5.71	6.33
21	0.51	0.69	2.3	2.83	3.63	4.18	4.97	5.58	6.18
22	0.50	0.67	2.23	2.76	3.54	4.08	4.85	5.45	6.05
23	0.48	0.66	2.17	2.69	3.46	3.99	4.75	5.33	5.92
24	0.47	0.64	2.11	2.62	3.38	3.9	4.64	5.22	5.79
25	0.46	0.63	2.06	2.55	3.3	3.82	4.55	5.11	5.68
26	0.45	0.61	2	2.49	3.23	3.74	4.45	5.01	5.57
27	0.44	0.60	1.95	2.44	3.16	3.66	4.36	4.91	5.46
28	0.43	0.59	1.91	2.38	3.09	3.59	4.28	4.82	5.35
29	0.42	0.58	1.86	2.33	3.03	3.52	4.2	4.73	5.26
30	0.41	0.56	1.82	2.28	2.97	3.45	4.12	4.64	5.16
31	0.41	0.55	1.78	2.23	2.91	3.38	4.04	4.56	5.07
32	0.40	0.54	1.74	2.19	2.86	3.32	3.97	4.48	4.98
33	0.39	0.53	1.7	2.14	2.81	3.26	3.9	4.4	4.89
34	0.38	0.52	1.67	2.1	2.76	3.2	3.84	4.33	4.81
35	0.38	0.51	1.64	2.06	2.71	3.15	3.77	4.25	4.73
36	0.37	0.51	1.61	2.03	2.66	3.1	3.71	4.18	4.66
37	0.36	0.50	1.58	1.99	2.62	3.05	3.65	4.12	4.58
38	0.36	0.49	1.55	1.96	2.57	3	3.59	4.05	4.51
39	0.35	0.48	1.52	1.92	2.53	2.95	3.54	3.99	4.44
40	0.35	0.47	1.49	1.89	2.49	2.9	3.48	3.93	4.38
41	0.34	0.47	1.47	1.86	2.45	2.86	3.43	3.87	4.31
42	0.34	0.46	1.45	1.83	2.42	2.82	3.38	3.82	4.25
43	0.33	0.45	1.42	1.8	2.38	2.78	3.33	3.76	4.19
44	0.33	0.45	1.4	1.78	2.35	2.74	3.28	3.71	4.13
45	0.32	0.44	1.38	1.75	2.31	2.7	3.24	3.66	4.07
46	0.32	0.43	1.36	1.73	2.28	2.66	3.19	3.61	4.02
47	0.31	0.43	1.34	1.7	2.25	2.62	3.15	3.56	3.97
48	0.31	0.42	1.32	1.68	2.22	2.59	3.11	3.51	3.92
49	0.31	0.42	1.3	1.66	2.19	2.56	3.07	3.47	3.87
50	0.30	0.41	1.28	1.63	2.16	2.52	3.03	3.43	3.82
51	0.30	0.40	1.27	1.61	2.13	2.49	2.99	3.38	3.77
52	0.29	0.40	1.25	1.59	2.11	2.46	2.96	3.34	3.72
53	0.29	0.39	1.23	1.57	2.08	2.43	2.92	3.3	3.68
54	0.29	0.39	1.22	1.55	2.06	2.4	2.89	3.26	3.64
55	0.28	0.39	1.2	1.53	2.03	2.37	2.85	3.22	3.59
56	0.28	0.38	1.19	1.52	2.01	2.35	2.82	3.19	3.55
57	0.28	0.38	1.18	1.5	1.99	2.32	2.79	3.15	3.51
58	0.27	0.37	1.16	1.48	1.96	2.3	2.76	3.12	3.47
59	0.27	0.37	1.15	1.47	1.94	2.27	2.73	3.08	3.44
60	0.27	0.36	1.14	1.45	1.92	2.25	2.7	3.05	3.4

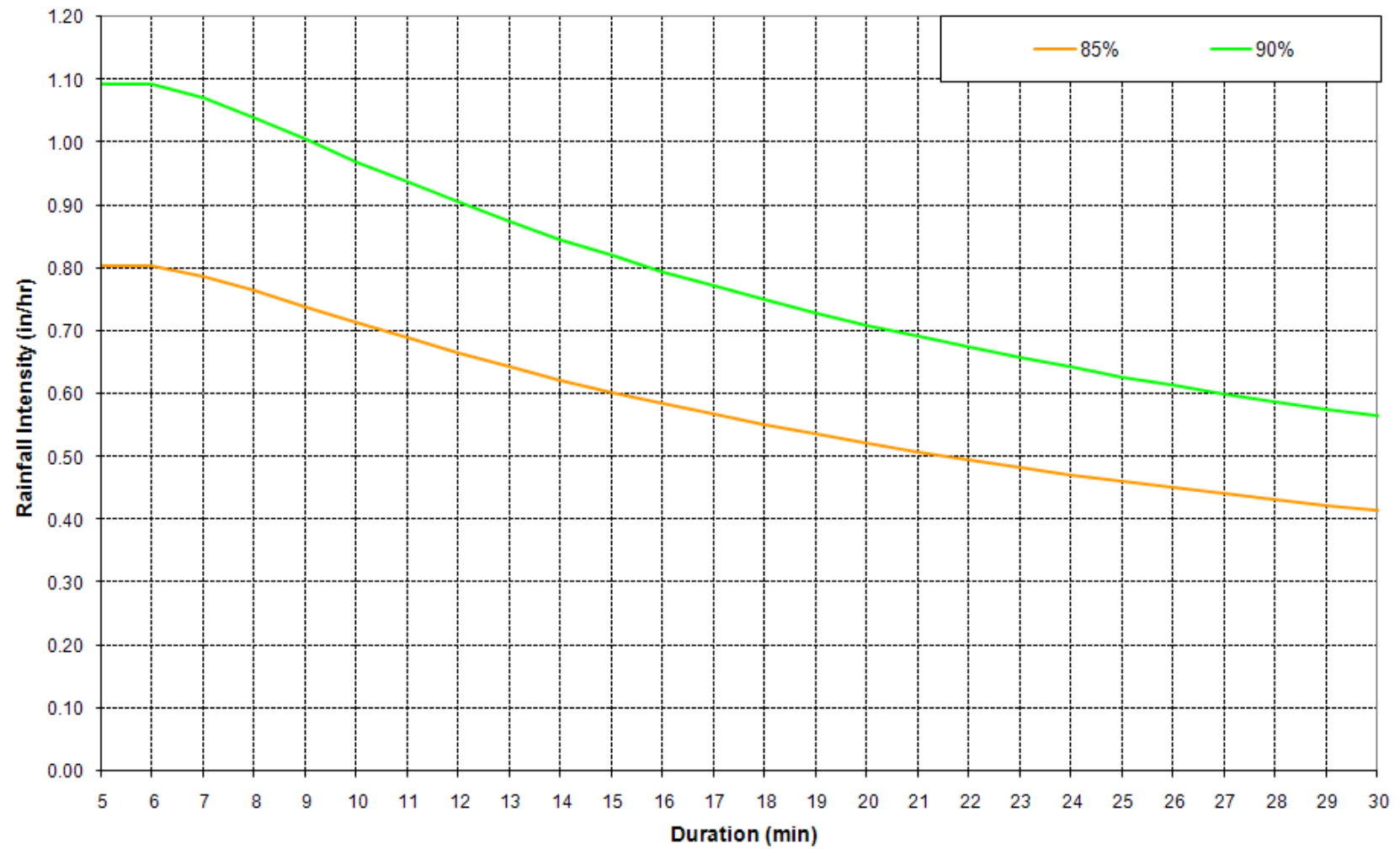
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Dodge City, Kansas



Dodge City, Kansas

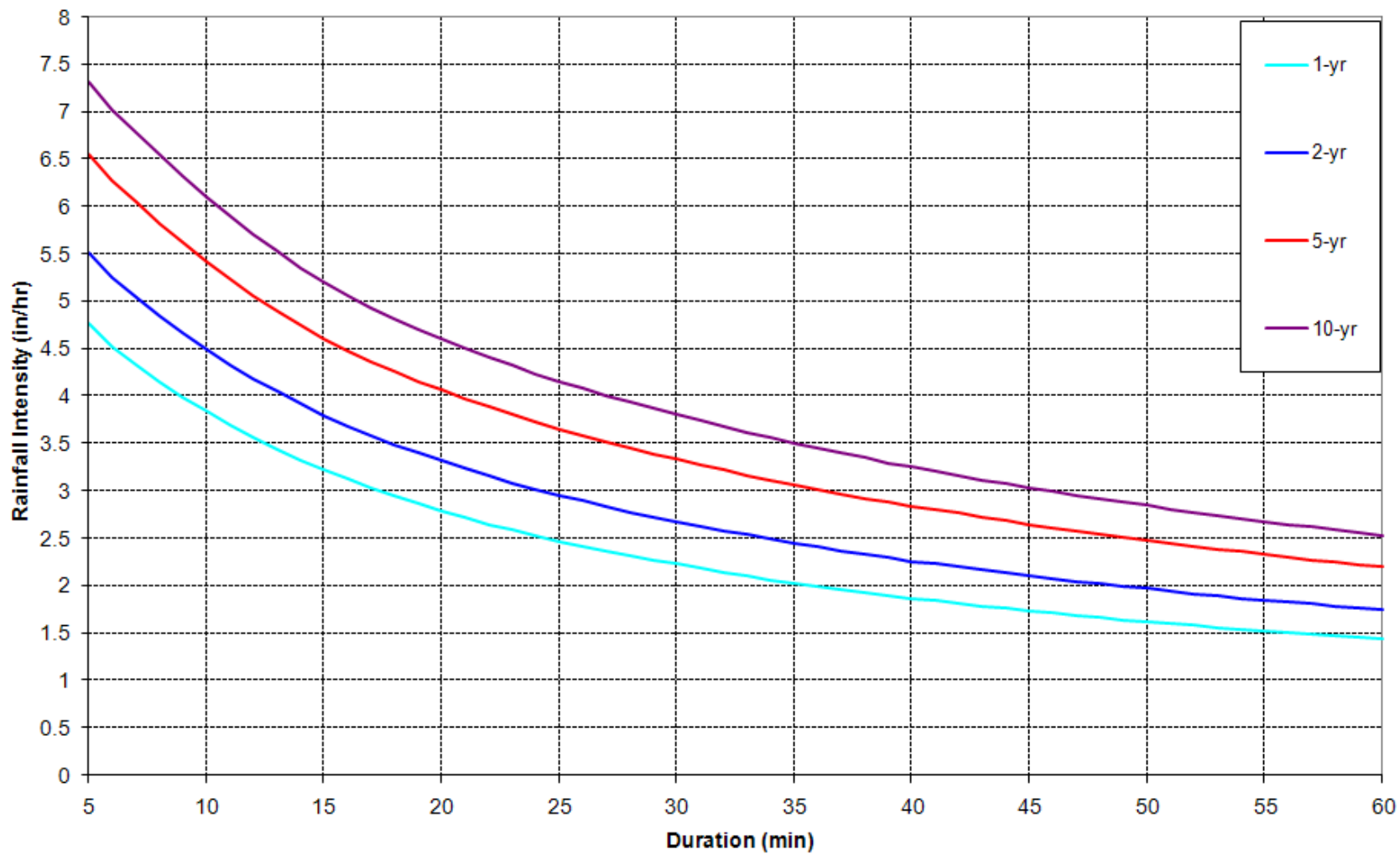


Emporia, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.25	1.66	4.77	5.52	6.56	7.32	8.44	9.32	10.2
6	1.25	1.66	4.53	5.26	6.28	7.03	8.13	8.99	9.84
7	1.22	1.63	4.33	5.05	6.05	6.78	7.85	8.69	9.52
8	1.18	1.58	4.15	4.85	5.83	6.55	7.59	8.41	9.22
9	1.15	1.53	3.99	4.67	5.63	6.33	7.34	8.14	8.93
10	1.11	1.47	3.84	4.5	5.43	6.11	7.1	7.87	8.64
11	1.07	1.42	3.7	4.34	5.25	5.9	6.86	7.61	8.36
12	1.03	1.38	3.57	4.19	5.07	5.71	6.64	7.37	8.09
13	1.00	1.33	3.44	4.05	4.91	5.53	6.43	7.14	7.84
14	0.96	1.29	3.33	3.92	4.76	5.36	6.24	6.93	7.61
15	0.93	1.25	3.22	3.8	4.62	5.21	6.06	6.73	7.4
16	0.91	1.21	3.13	3.69	4.49	5.07	5.91	6.56	7.21
17	0.88	1.17	3.03	3.59	4.37	4.94	5.76	6.4	7.04
18	0.85	1.14	2.95	3.49	4.27	4.82	5.63	6.25	6.88
19	0.83	1.11	2.87	3.4	4.16	4.71	5.5	6.12	6.73
20	0.81	1.08	2.79	3.32	4.07	4.61	5.38	5.99	6.59
21	0.79	1.05	2.72	3.24	3.98	4.51	5.27	5.87	6.46
22	0.77	1.02	2.65	3.16	3.89	4.41	5.17	5.76	6.34
23	0.75	1.00	2.59	3.09	3.81	4.33	5.07	5.65	6.22
24	0.73	0.98	2.53	3.02	3.74	4.24	4.97	5.54	6.11
25	0.72	0.95	2.47	2.96	3.66	4.16	4.88	5.44	6
26	0.70	0.93	2.42	2.9	3.59	4.09	4.8	5.35	5.9
27	0.68	0.91	2.37	2.84	3.53	4.01	4.71	5.26	5.8
28	0.67	0.89	2.32	2.78	3.46	3.94	4.63	5.17	5.7
29	0.66	0.88	2.27	2.73	3.4	3.87	4.55	5.08	5.61
30	0.64	0.86	2.23	2.68	3.34	3.81	4.48	5	5.52
31	0.63	0.84	2.18	2.63	3.28	3.74	4.41	4.92	5.43
32	0.62	0.83	2.14	2.58	3.23	3.68	4.33	4.84	5.35
33	0.61	0.81	2.1	2.54	3.17	3.62	4.27	4.77	5.26
34	0.60	0.80	2.06	2.49	3.12	3.57	4.2	4.69	5.18
35	0.59	0.78	2.03	2.45	3.07	3.51	4.14	4.62	5.11
36	0.58	0.77	1.99	2.41	3.02	3.46	4.07	4.55	5.03
37	0.57	0.75	1.96	2.37	2.98	3.4	4.01	4.49	4.96
38	0.56	0.74	1.93	2.34	2.93	3.35	3.95	4.42	4.89
39	0.55	0.73	1.9	2.3	2.89	3.3	3.9	4.36	4.82
40	0.54	0.72	1.87	2.26	2.85	3.26	3.84	4.3	4.75
41	0.53	0.71	1.84	2.23	2.81	3.21	3.79	4.24	4.68
42	0.52	0.70	1.81	2.2	2.77	3.16	3.73	4.18	4.62
43	0.52	0.69	1.78	2.17	2.73	3.12	3.68	4.12	4.56
44	0.51	0.68	1.76	2.14	2.69	3.08	3.63	4.06	4.49
45	0.50	0.67	1.73	2.11	2.65	3.04	3.58	4.01	4.44
46	0.49	0.66	1.71	2.08	2.62	3	3.54	3.96	4.38
47	0.49	0.65	1.69	2.05	2.58	2.96	3.49	3.91	4.32
48	0.48	0.64	1.66	2.02	2.55	2.92	3.45	3.86	4.27
49	0.47	0.63	1.64	2	2.52	2.88	3.4	3.81	4.21
50	0.47	0.62	1.62	1.97	2.48	2.85	3.36	3.76	4.16
51	0.46	0.62	1.6	1.95	2.45	2.81	3.32	3.72	4.11
52	0.46	0.61	1.58	1.92	2.42	2.78	3.28	3.67	4.06
53	0.45	0.60	1.56	1.9	2.39	2.74	3.24	3.63	4.01
54	0.44	0.59	1.54	1.87	2.37	2.71	3.2	3.58	3.96
55	0.44	0.59	1.52	1.85	2.34	2.68	3.16	3.54	3.92
56	0.43	0.58	1.5	1.83	2.31	2.65	3.13	3.5	3.87
57	0.43	0.57	1.49	1.81	2.28	2.62	3.09	3.46	3.83
58	0.42	0.57	1.47	1.79	2.26	2.59	3.06	3.42	3.78
59	0.42	0.56	1.45	1.77	2.23	2.56	3.02	3.38	3.74
60	0.41	0.55	1.44	1.75	2.21	2.53	2.99	3.34	3.7

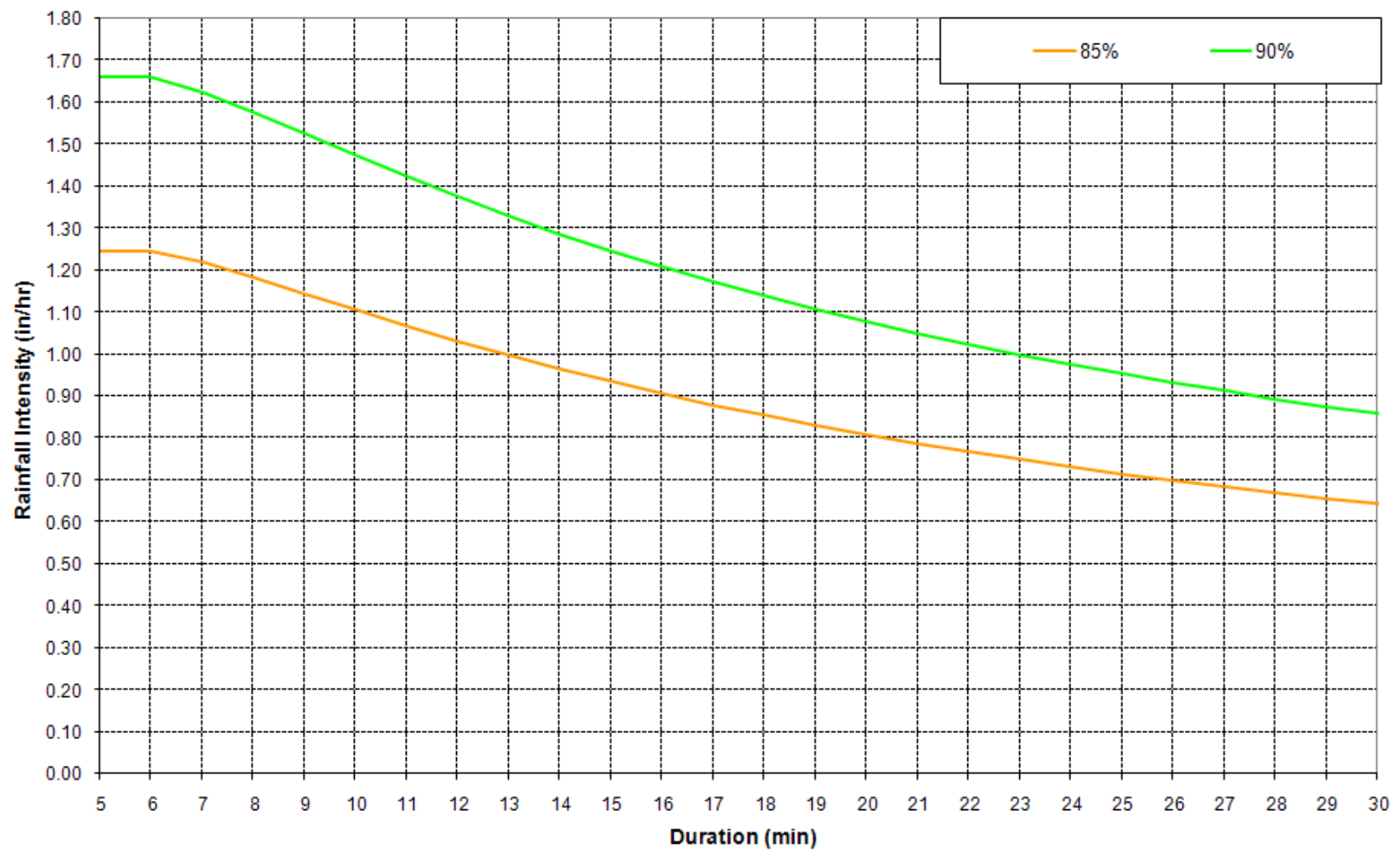
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Emporia, Kansas



Emporia, Kansas

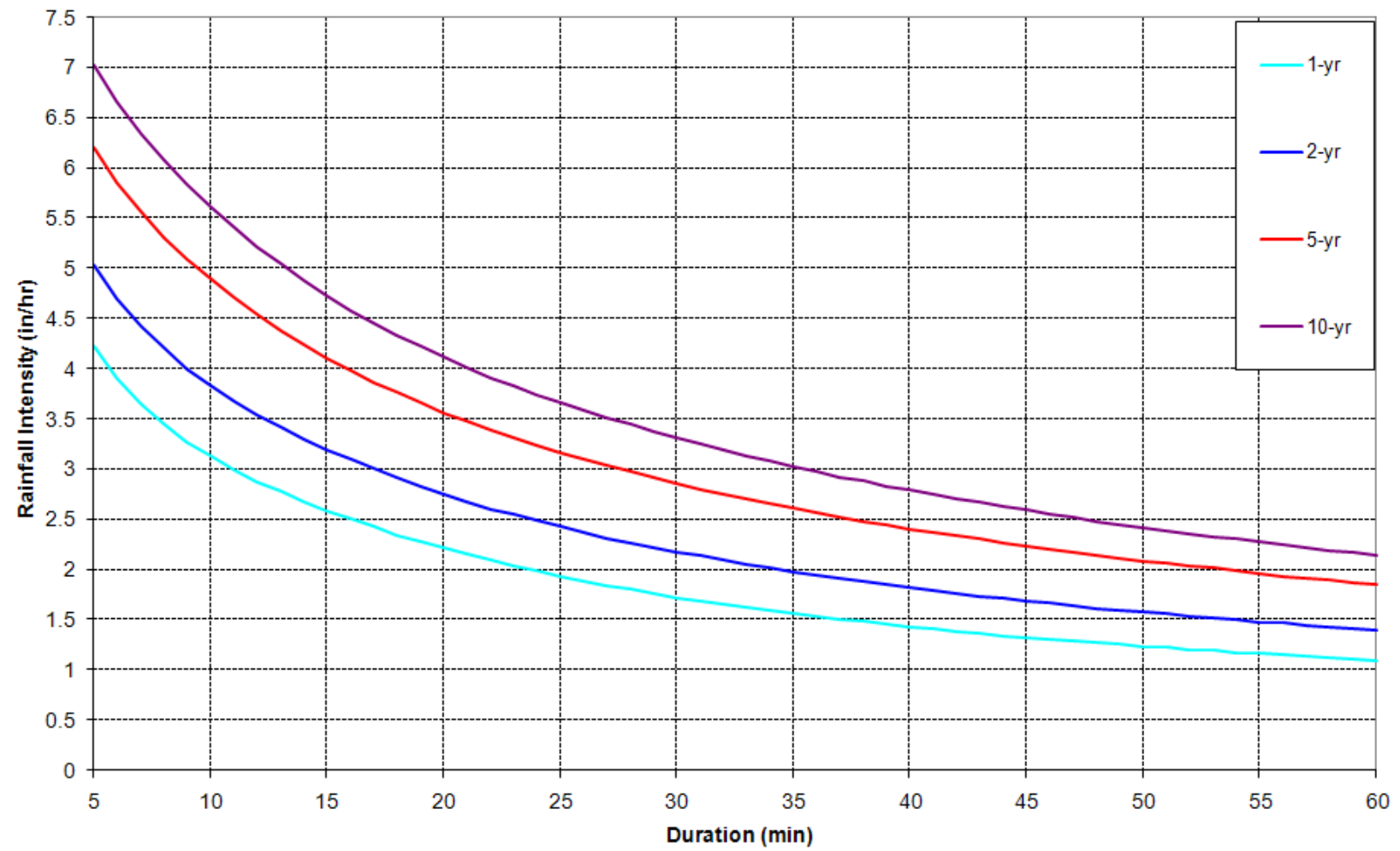


Garden City, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	0.83	1.23	4.23	5.04	6.2	7.03	8.22	9.15	10.08
6	0.83	1.23	3.91	4.7	5.85	6.66	7.82	8.73	9.64
7	0.81	1.21	3.66	4.43	5.56	6.35	7.49	8.38	9.26
8	0.79	1.17	3.45	4.21	5.31	6.09	7.19	8.05	8.91
9	0.76	1.13	3.28	4.01	5.09	5.84	6.92	7.76	8.59
10	0.74	1.09	3.13	3.84	4.89	5.62	6.66	7.47	8.28
11	0.71	1.06	3	3.69	4.71	5.42	6.42	7.21	7.99
12	0.69	1.02	2.88	3.55	4.54	5.22	6.2	6.96	7.71
13	0.66	0.99	2.78	3.42	4.38	5.05	5.99	6.73	7.46
14	0.64	0.95	2.68	3.31	4.24	4.88	5.8	6.51	7.22
15	0.62	0.92	2.59	3.2	4.1	4.73	5.62	6.31	7
16	0.60	0.90	2.51	3.1	3.98	4.59	5.46	6.13	6.8
17	0.59	0.87	2.43	3.01	3.86	4.46	5.3	5.96	6.61
18	0.57	0.84	2.35	2.92	3.76	4.34	5.16	5.8	6.44
19	0.55	0.82	2.28	2.83	3.66	4.23	5.03	5.66	6.28
20	0.54	0.80	2.22	2.76	3.56	4.12	4.91	5.52	6.13
21	0.53	0.78	2.16	2.68	3.47	4.02	4.79	5.39	5.98
22	0.51	0.76	2.1	2.61	3.39	3.92	4.68	5.27	5.85
23	0.50	0.74	2.04	2.55	3.31	3.83	4.58	5.15	5.72
24	0.49	0.72	1.99	2.49	3.23	3.75	4.48	5.04	5.6
25	0.48	0.71	1.94	2.43	3.16	3.67	4.38	4.94	5.49
26	0.47	0.69	1.89	2.37	3.09	3.59	4.29	4.84	5.38
27	0.46	0.68	1.85	2.32	3.03	3.52	4.21	4.74	5.27
28	0.45	0.66	1.81	2.27	2.97	3.45	4.12	4.65	5.17
29	0.44	0.65	1.77	2.23	2.91	3.38	4.05	4.56	5.07
30	0.43	0.64	1.73	2.18	2.85	3.32	3.97	4.48	4.98
31	0.42	0.62	1.7	2.14	2.8	3.26	3.9	4.4	4.89
32	0.41	0.61	1.66	2.1	2.75	3.2	3.83	4.32	4.8
33	0.40	0.60	1.63	2.06	2.7	3.14	3.76	4.24	4.72
34	0.40	0.59	1.6	2.02	2.65	3.09	3.7	4.17	4.64
35	0.39	0.58	1.57	1.98	2.61	3.03	3.64	4.1	4.57
36	0.38	0.57	1.54	1.95	2.56	2.98	3.58	4.03	4.49
37	0.38	0.56	1.51	1.92	2.52	2.93	3.52	3.97	4.42
38	0.37	0.55	1.49	1.88	2.48	2.89	3.46	3.91	4.35
39	0.37	0.54	1.46	1.85	2.44	2.84	3.41	3.85	4.28
40	0.36	0.53	1.44	1.82	2.4	2.8	3.36	3.79	4.22
41	0.35	0.53	1.42	1.79	2.36	2.76	3.31	3.73	4.16
42	0.35	0.52	1.39	1.77	2.33	2.71	3.26	3.68	4.09
43	0.34	0.51	1.37	1.74	2.3	2.68	3.21	3.62	4.04
44	0.34	0.50	1.35	1.72	2.26	2.64	3.16	3.57	3.98
45	0.33	0.49	1.33	1.69	2.23	2.6	3.12	3.52	3.92
46	0.33	0.49	1.31	1.67	2.2	2.56	3.08	3.47	3.87
47	0.32	0.48	1.3	1.64	2.17	2.53	3.03	3.43	3.82
48	0.32	0.47	1.28	1.62	2.14	2.49	2.99	3.38	3.77
49	0.32	0.47	1.26	1.6	2.11	2.46	2.95	3.34	3.72
50	0.31	0.46	1.24	1.58	2.08	2.43	2.92	3.29	3.67
51	0.31	0.46	1.23	1.56	2.06	2.4	2.88	3.25	3.62
52	0.30	0.45	1.21	1.54	2.03	2.37	2.84	3.21	3.58
53	0.30	0.44	1.2	1.52	2.01	2.34	2.81	3.17	3.53
54	0.30	0.44	1.18	1.5	1.98	2.31	2.77	3.13	3.49
55	0.29	0.43	1.17	1.48	1.96	2.28	2.74	3.09	3.45
56	0.29	0.43	1.16	1.47	1.93	2.26	2.71	3.06	3.4
57	0.29	0.42	1.14	1.45	1.91	2.23	2.68	3.02	3.36
58	0.28	0.42	1.13	1.43	1.89	2.2	2.64	2.99	3.33
59	0.28	0.41	1.12	1.42	1.87	2.18	2.61	2.95	3.29
60	0.28	0.41	1.1	1.4	1.85	2.15	2.58	2.92	3.25

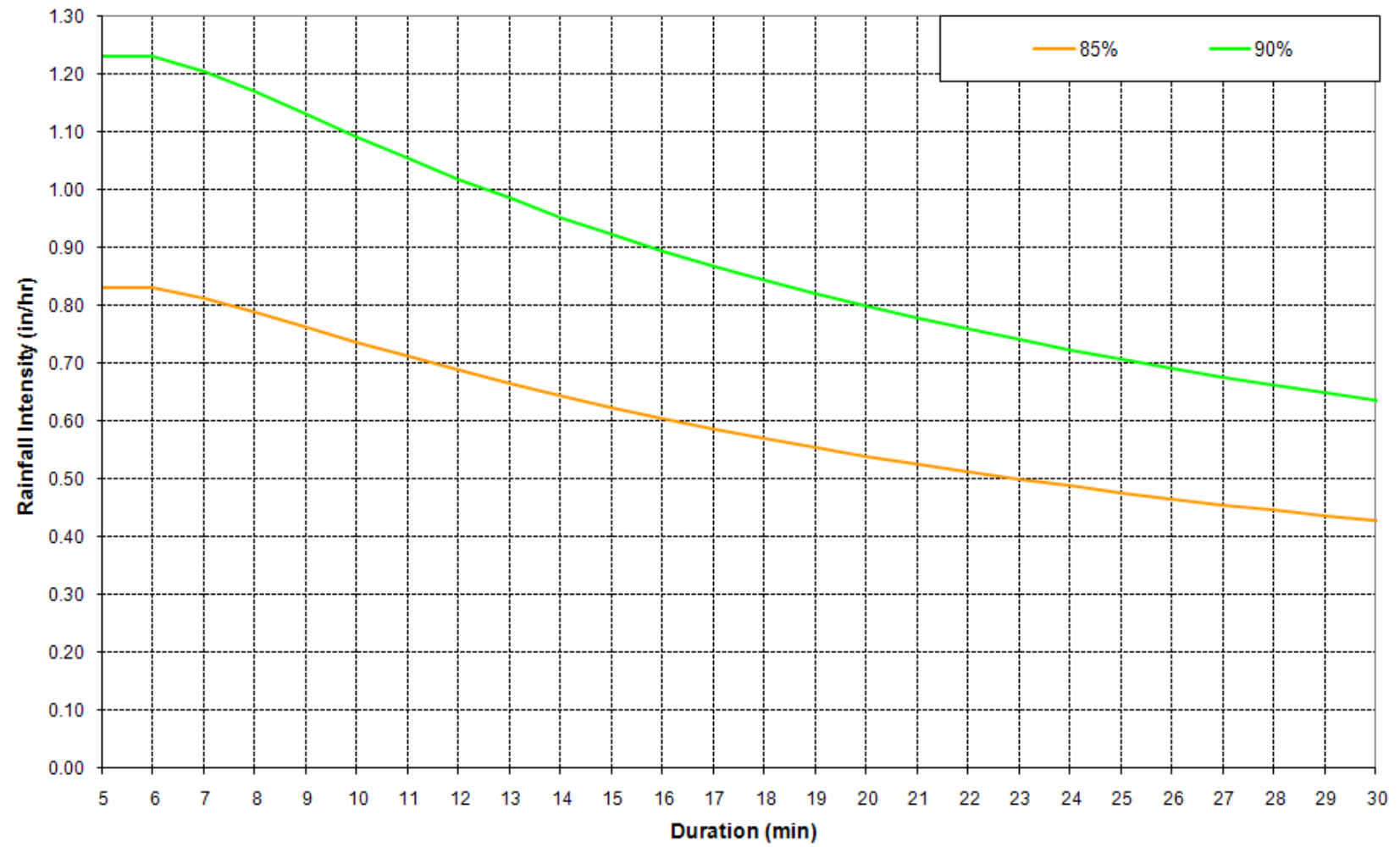
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Garden City, Kansas



Garden City, Kansas

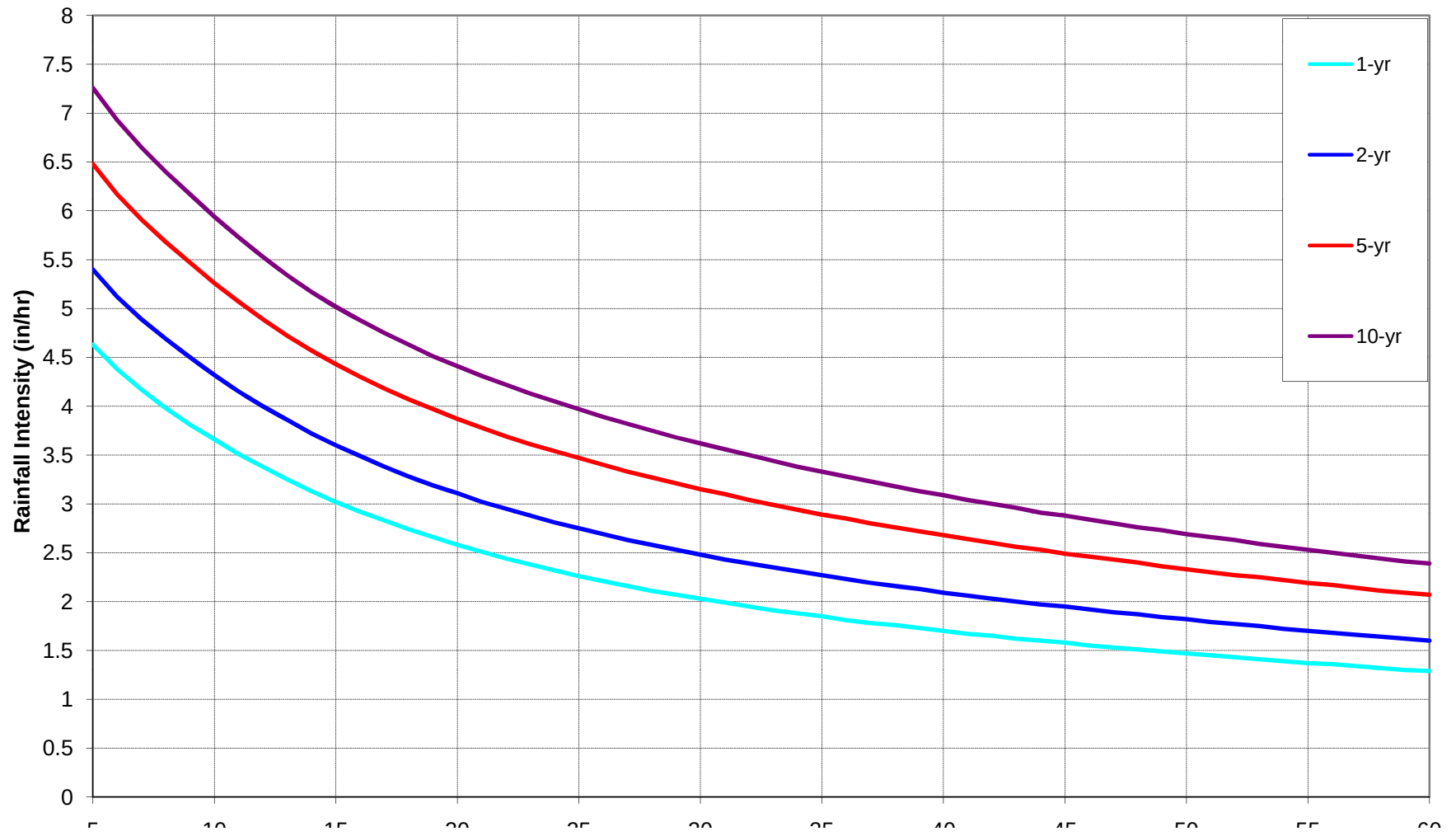


Great Bend, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.11	1.38	4.63	5.4	6.48	7.26	8.41	9.31	10.2
6	1.11	1.38	4.38	5.12	6.17	6.93	8.04	8.91	9.78
7	1.08	1.36	4.17	4.89	5.91	6.65	7.73	8.58	9.41
8	1.05	1.32	3.98	4.69	5.68	6.4	7.45	8.27	9.08
9	1.02	1.27	3.81	4.5	5.47	6.17	7.18	7.97	8.76
10	0.98	1.23	3.66	4.32	5.26	5.94	6.93	7.69	8.46
11	0.95	1.19	3.51	4.15	5.07	5.73	6.68	7.43	8.17
12	0.92	1.15	3.38	4	4.89	5.53	6.45	7.18	7.89
13	0.89	1.11	3.25	3.86	4.72	5.34	6.24	6.94	7.64
14	0.86	1.07	3.13	3.72	4.57	5.17	6.05	6.73	7.41
15	0.83	1.04	3.02	3.6	4.43	5.02	5.87	6.54	7.2
16	0.81	1.01	2.92	3.49	4.3	4.88	5.71	6.36	7.01
17	0.78	0.98	2.83	3.38	4.18	4.75	5.56	6.2	6.84
18	0.76	0.95	2.74	3.28	4.07	4.63	5.43	6.06	6.68
19	0.74	0.92	2.66	3.19	3.97	4.51	5.3	5.92	6.53
20	0.72	0.90	2.58	3.11	3.87	4.41	5.19	5.79	6.39
21	0.70	0.88	2.51	3.02	3.78	4.31	5.07	5.67	6.26
22	0.68	0.85	2.44	2.95	3.69	4.22	4.97	5.56	6.14
23	0.67	0.83	2.38	2.88	3.61	4.13	4.87	5.45	6.02
24	0.65	0.81	2.32	2.81	3.54	4.05	4.78	5.34	5.91
25	0.64	0.79	2.26	2.75	3.47	3.97	4.69	5.24	5.8
26	0.62	0.78	2.21	2.69	3.4	3.89	4.6	5.15	5.7
27	0.61	0.76	2.16	2.63	3.33	3.82	4.52	5.06	5.6
28	0.60	0.74	2.11	2.58	3.27	3.75	4.44	4.97	5.5
29	0.58	0.73	2.07	2.53	3.21	3.68	4.36	4.89	5.41
30	0.57	0.71	2.03	2.48	3.15	3.62	4.29	4.8	5.32
31	0.56	0.70	1.99	2.43	3.1	3.56	4.21	4.72	5.23
32	0.55	0.69	1.95	2.39	3.04	3.5	4.14	4.65	5.15
33	0.54	0.67	1.91	2.35	2.99	3.44	4.08	4.57	5.07
34	0.53	0.66	1.88	2.31	2.94	3.38	4.01	4.5	4.99
35	0.52	0.65	1.85	2.27	2.89	3.33	3.95	4.43	4.91
36	0.51	0.64	1.81	2.23	2.85	3.28	3.89	4.36	4.84
37	0.50	0.63	1.78	2.19	2.8	3.23	3.83	4.3	4.76
38	0.50	0.62	1.76	2.16	2.76	3.18	3.77	4.23	4.69
39	0.49	0.61	1.73	2.13	2.72	3.13	3.72	4.17	4.62
40	0.48	0.60	1.7	2.09	2.68	3.09	3.66	4.11	4.56
41	0.47	0.59	1.67	2.06	2.64	3.04	3.61	4.05	4.49
42	0.46	0.58	1.65	2.03	2.6	3	3.56	4	4.43
43	0.46	0.57	1.62	2	2.56	2.96	3.51	3.94	4.37
44	0.45	0.56	1.6	1.97	2.53	2.91	3.46	3.89	4.31
45	0.44	0.56	1.58	1.95	2.49	2.88	3.42	3.84	4.25
46	0.44	0.55	1.55	1.92	2.46	2.84	3.37	3.79	4.2
47	0.43	0.54	1.53	1.89	2.43	2.8	3.33	3.74	4.14
48	0.43	0.53	1.51	1.87	2.4	2.76	3.28	3.69	4.09
49	0.42	0.53	1.49	1.84	2.36	2.73	3.24	3.64	4.04
50	0.42	0.52	1.47	1.82	2.33	2.69	3.2	3.6	3.99
51	0.41	0.51	1.45	1.79	2.3	2.66	3.16	3.55	3.94
52	0.40	0.51	1.43	1.77	2.27	2.63	3.12	3.51	3.89
53	0.40	0.50	1.41	1.75	2.25	2.59	3.08	3.47	3.85
54	0.40	0.49	1.39	1.72	2.22	2.56	3.05	3.42	3.8
55	0.39	0.49	1.37	1.7	2.19	2.53	3.01	3.38	3.76
56	0.39	0.48	1.36	1.68	2.17	2.5	2.98	3.35	3.71
57	0.38	0.48	1.34	1.66	2.14	2.47	2.94	3.31	3.67
58	0.38	0.47	1.32	1.64	2.11	2.44	2.91	3.27	3.63
59	0.37	0.47	1.3	1.62	2.09	2.41	2.88	3.23	3.59
60	0.37	0.46	1.29	1.6	2.07	2.39	2.84	3.2	3.55

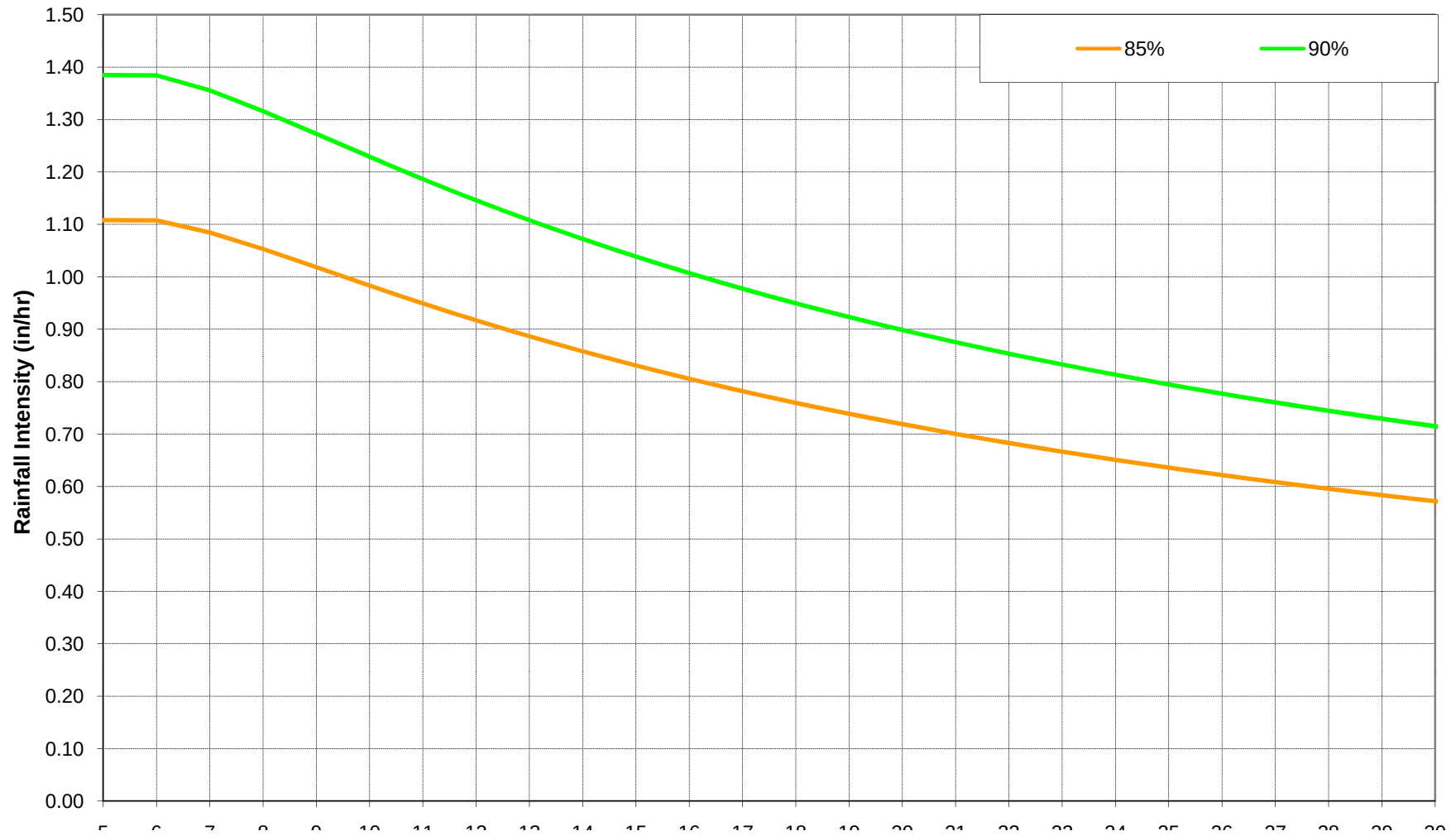
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Great Bend, Kansas



Great Bend, Kansas

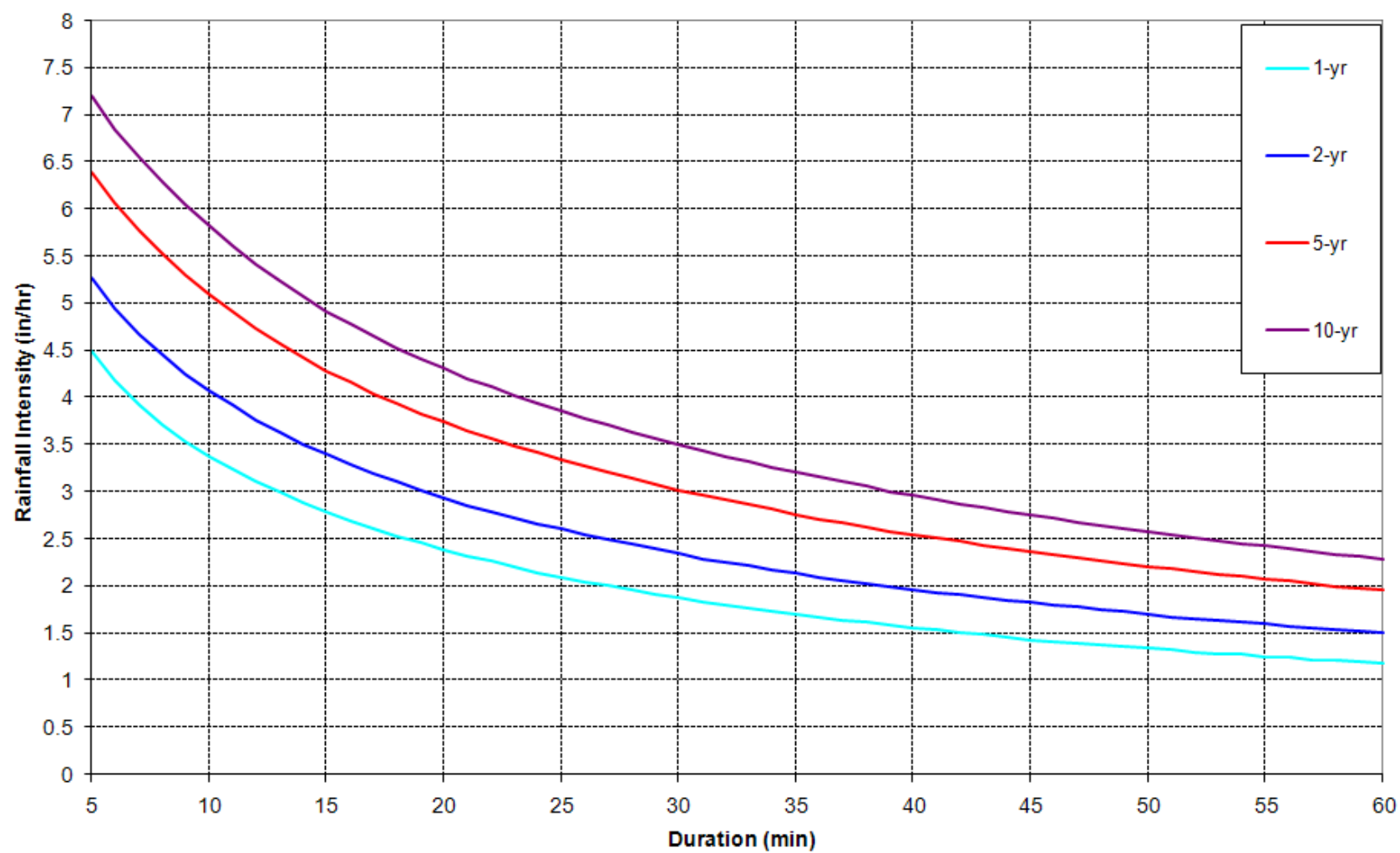


Hays, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	0.97	1.25	4.49	5.28	6.39	7.2	8.37	9.29	10.2
6	0.97	1.25	4.18	4.95	6.06	6.85	7.99	8.89	9.78
7	0.95	1.22	3.93	4.68	5.77	6.55	7.67	8.54	9.41
8	0.92	1.18	3.72	4.46	5.53	6.29	7.38	8.23	9.08
9	0.89	1.15	3.54	4.26	5.31	6.05	7.11	7.94	8.76
10	0.86	1.11	3.38	4.08	5.1	5.82	6.86	7.66	8.46
11	0.83	1.07	3.24	3.92	4.91	5.61	6.61	7.4	8.17
12	0.80	1.03	3.11	3.77	4.74	5.42	6.39	7.15	7.9
13	0.78	1.00	3	3.64	4.58	5.24	6.18	6.92	7.65
14	0.75	0.96	2.89	3.51	4.43	5.07	5.99	6.7	7.41
15	0.73	0.93	2.79	3.4	4.29	4.92	5.81	6.51	7.2
16	0.70	0.91	2.7	3.29	4.17	4.78	5.65	6.33	7
17	0.68	0.88	2.62	3.2	4.05	4.65	5.5	6.16	6.82
18	0.66	0.85	2.54	3.11	3.94	4.53	5.36	6.01	6.66
19	0.65	0.83	2.46	3.02	3.84	4.42	5.23	5.87	6.5
20	0.63	0.81	2.39	2.94	3.75	4.31	5.11	5.73	6.35
21	0.61	0.79	2.33	2.86	3.66	4.21	5	5.61	6.21
22	0.60	0.77	2.27	2.79	3.57	4.12	4.89	5.49	6.08
23	0.58	0.75	2.21	2.73	3.49	4.03	4.78	5.37	5.96
24	0.57	0.73	2.15	2.66	3.42	3.94	4.69	5.26	5.84
25	0.56	0.72	2.1	2.6	3.34	3.86	4.59	5.16	5.73
26	0.54	0.70	2.05	2.54	3.28	3.78	4.5	5.06	5.62
27	0.53	0.68	2.01	2.49	3.21	3.71	4.42	4.97	5.51
28	0.52	0.67	1.96	2.44	3.15	3.64	4.33	4.87	5.41
29	0.51	0.66	1.92	2.39	3.09	3.57	4.25	4.79	5.31
30	0.50	0.64	1.88	2.34	3.03	3.5	4.18	4.7	5.22
31	0.49	0.63	1.84	2.29	2.97	3.44	4.1	4.62	5.13
32	0.48	0.62	1.8	2.25	2.92	3.38	4.03	4.54	5.04
33	0.47	0.61	1.77	2.21	2.87	3.32	3.96	4.46	4.96
34	0.46	0.60	1.74	2.17	2.82	3.27	3.9	4.39	4.88
35	0.46	0.59	1.7	2.13	2.77	3.21	3.83	4.32	4.8
36	0.45	0.58	1.67	2.09	2.72	3.16	3.77	4.25	4.72
37	0.44	0.57	1.64	2.06	2.68	3.11	3.71	4.18	4.65
38	0.43	0.56	1.62	2.02	2.64	3.06	3.65	4.12	4.58
39	0.43	0.55	1.59	1.99	2.59	3.01	3.6	4.05	4.51
40	0.42	0.54	1.56	1.96	2.55	2.97	3.54	3.99	4.44
41	0.41	0.53	1.54	1.93	2.52	2.92	3.49	3.93	4.38
42	0.41	0.52	1.51	1.9	2.48	2.88	3.44	3.88	4.31
43	0.40	0.52	1.49	1.87	2.44	2.84	3.39	3.82	4.25
44	0.39	0.51	1.47	1.84	2.41	2.8	3.34	3.77	4.19
45	0.39	0.50	1.44	1.82	2.37	2.76	3.3	3.72	4.14
46	0.38	0.49	1.42	1.79	2.34	2.72	3.25	3.67	4.08
47	0.38	0.49	1.4	1.77	2.31	2.68	3.21	3.62	4.03
48	0.37	0.48	1.38	1.74	2.28	2.65	3.17	3.57	3.97
49	0.37	0.47	1.36	1.72	2.25	2.61	3.13	3.53	3.92
50	0.36	0.47	1.35	1.69	2.22	2.58	3.09	3.48	3.87
51	0.36	0.46	1.33	1.67	2.19	2.55	3.05	3.44	3.83
52	0.35	0.46	1.31	1.65	2.16	2.52	3.01	3.4	3.78
53	0.35	0.45	1.29	1.63	2.14	2.49	2.98	3.36	3.73
54	0.35	0.44	1.28	1.61	2.11	2.46	2.94	3.32	3.69
55	0.34	0.44	1.26	1.59	2.09	2.43	2.91	3.28	3.65
56	0.34	0.43	1.25	1.57	2.06	2.4	2.87	3.24	3.61
57	0.33	0.43	1.23	1.55	2.04	2.37	2.84	3.2	3.57
58	0.33	0.42	1.22	1.53	2.01	2.34	2.81	3.17	3.53
59	0.33	0.42	1.2	1.52	1.99	2.32	2.78	3.13	3.49
60	0.32	0.41	1.19	1.5	1.97	2.29	2.75	3.1	3.45

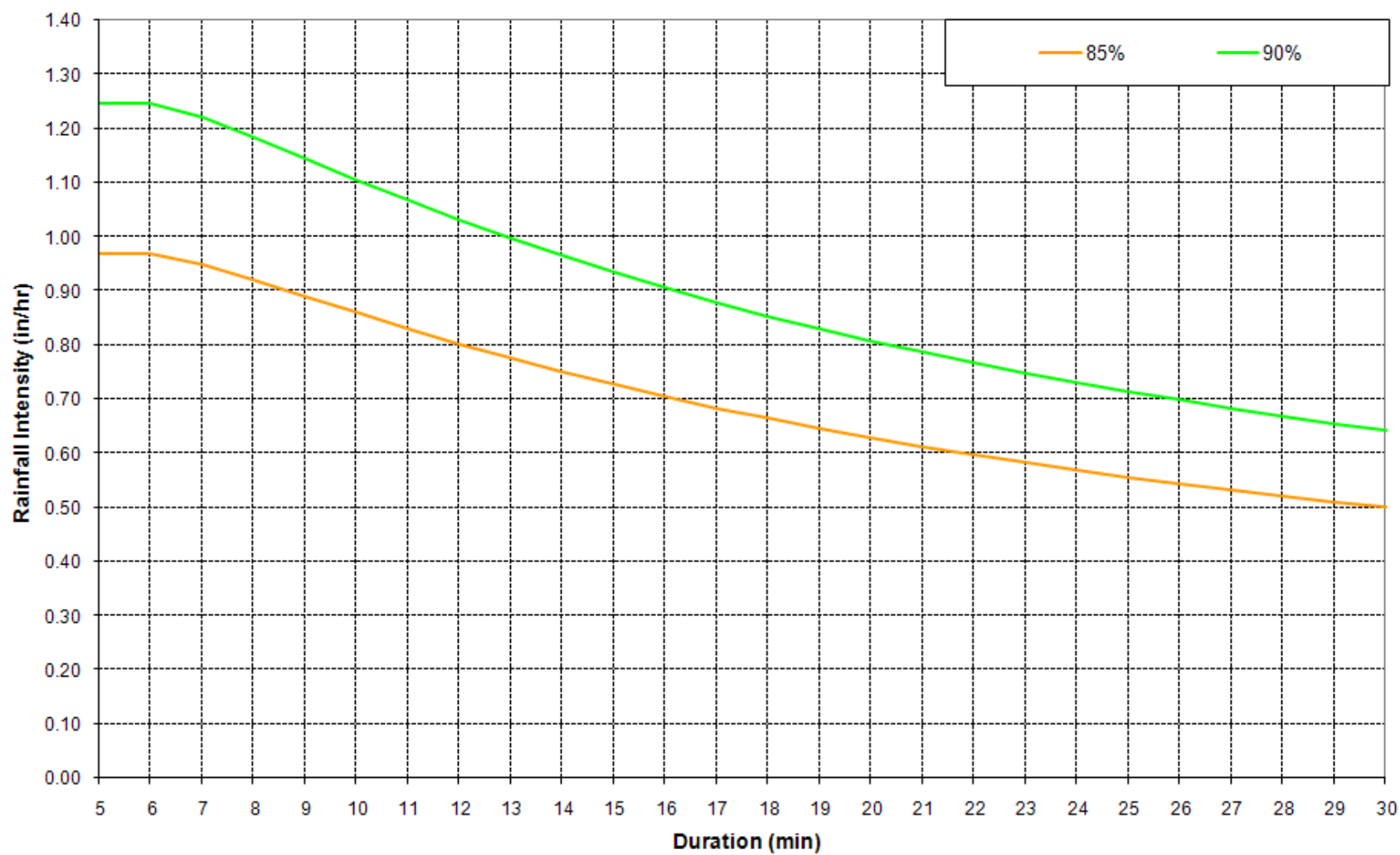
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Hays, Kansas



Hays, Kansas

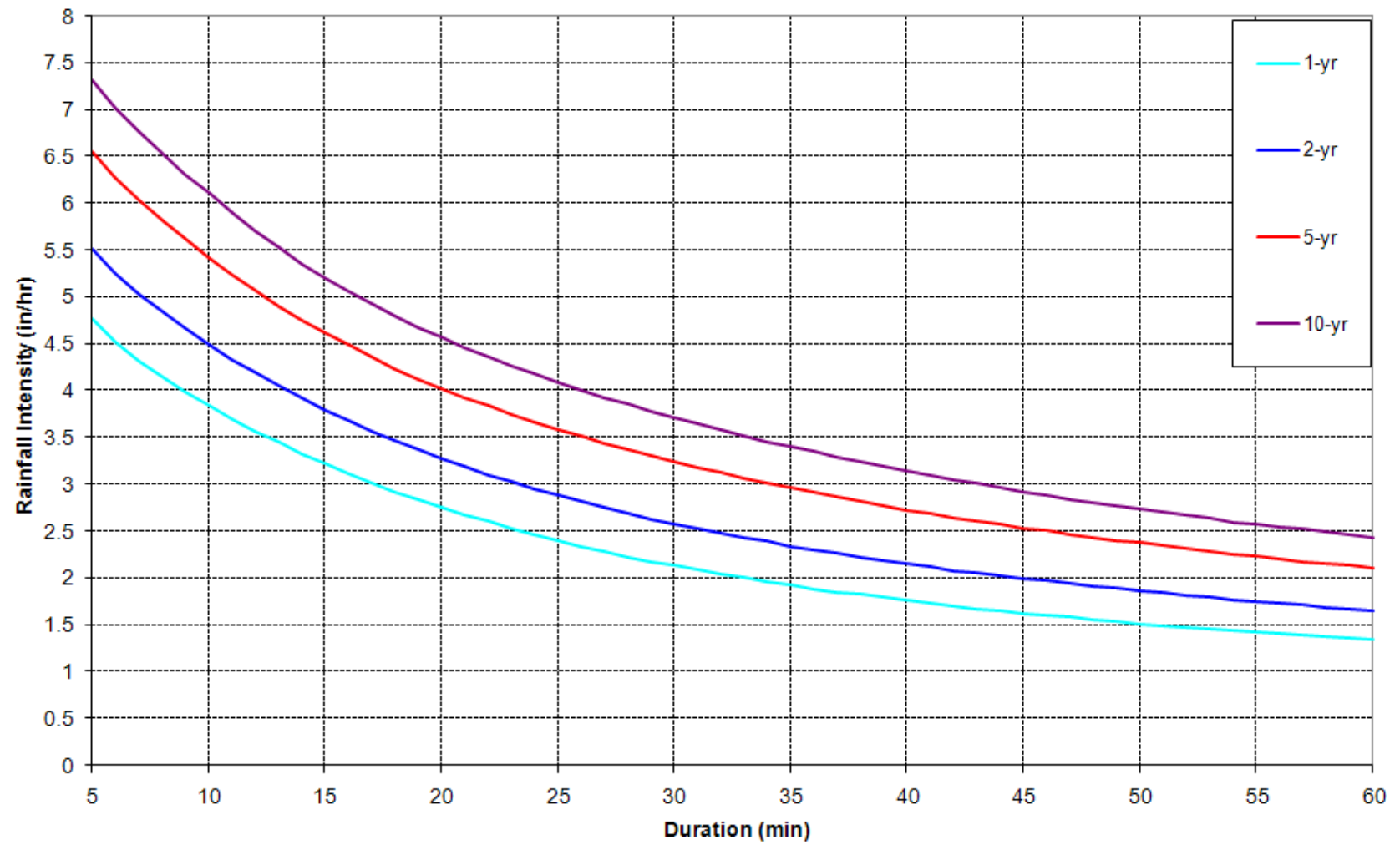


Hutchinson, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.25	1.66	4.77	5.52	6.56	7.32	8.44	9.32	10.2
6	1.25	1.66	4.53	5.26	6.28	7.03	8.12	8.98	9.84
7	1.22	1.63	4.32	5.04	6.04	6.77	7.84	8.68	9.52
8	1.18	1.58	4.15	4.85	5.83	6.54	7.59	8.4	9.22
9	1.15	1.53	3.99	4.67	5.63	6.32	7.34	8.13	8.93
10	1.11	1.47	3.84	4.5	5.43	6.11	7.1	7.87	8.64
11	1.07	1.42	3.7	4.34	5.25	5.91	6.87	7.61	8.36
12	1.03	1.38	3.57	4.2	5.08	5.71	6.64	7.37	8.09
13	1.00	1.33	3.45	4.06	4.91	5.53	6.44	7.14	7.84
14	0.96	1.29	3.33	3.92	4.76	5.36	6.24	6.93	7.61
15	0.93	1.25	3.22	3.8	4.62	5.21	6.06	6.73	7.4
16	0.91	1.21	3.12	3.68	4.49	5.06	5.9	6.55	7.21
17	0.88	1.17	3.02	3.57	4.36	4.93	5.75	6.39	7.03
18	0.85	1.14	2.92	3.47	4.24	4.8	5.61	6.23	6.86
19	0.83	1.11	2.83	3.37	4.13	4.68	5.47	6.09	6.71
20	0.81	1.08	2.75	3.28	4.03	4.57	5.35	5.95	6.56
21	0.79	1.05	2.67	3.19	3.93	4.46	5.23	5.83	6.42
22	0.77	1.02	2.6	3.1	3.84	4.36	5.12	5.71	6.29
23	0.75	1.00	2.52	3.03	3.75	4.27	5.01	5.59	6.16
24	0.73	0.98	2.46	2.95	3.67	4.18	4.91	5.48	6.05
25	0.72	0.95	2.39	2.88	3.59	4.09	4.81	5.37	5.93
26	0.70	0.93	2.33	2.82	3.52	4.01	4.72	5.27	5.82
27	0.68	0.91	2.28	2.75	3.44	3.93	4.63	5.17	5.72
28	0.67	0.89	2.22	2.69	3.37	3.86	4.54	5.08	5.61
29	0.66	0.88	2.17	2.63	3.31	3.78	4.46	4.99	5.52
30	0.64	0.86	2.13	2.58	3.25	3.71	4.38	4.9	5.42
31	0.63	0.84	2.08	2.53	3.19	3.65	4.31	4.82	5.33
32	0.62	0.83	2.04	2.48	3.13	3.58	4.23	4.74	5.24
33	0.61	0.81	2	2.43	3.07	3.52	4.16	4.66	5.15
34	0.60	0.80	1.96	2.39	3.02	3.46	4.09	4.58	5.07
35	0.59	0.78	1.92	2.34	2.97	3.4	4.02	4.51	4.99
36	0.58	0.77	1.88	2.3	2.92	3.35	3.96	4.44	4.91
37	0.57	0.75	1.85	2.26	2.87	3.29	3.9	4.37	4.83
38	0.56	0.74	1.82	2.22	2.82	3.24	3.84	4.3	4.76
39	0.55	0.73	1.79	2.19	2.78	3.19	3.78	4.23	4.69
40	0.54	0.72	1.76	2.15	2.73	3.14	3.72	4.17	4.62
41	0.53	0.71	1.73	2.12	2.69	3.09	3.67	4.11	4.55
42	0.52	0.70	1.7	2.08	2.65	3.05	3.61	4.05	4.49
43	0.52	0.69	1.67	2.05	2.61	3.01	3.56	4	4.43
44	0.51	0.68	1.65	2.02	2.58	2.96	3.51	3.94	4.37
45	0.50	0.67	1.62	1.99	2.54	2.92	3.47	3.89	4.31
46	0.49	0.66	1.6	1.97	2.51	2.88	3.42	3.84	4.25
47	0.49	0.65	1.58	1.94	2.47	2.84	3.37	3.78	4.19
48	0.48	0.64	1.55	1.91	2.44	2.81	3.33	3.74	4.14
49	0.47	0.63	1.53	1.89	2.41	2.77	3.29	3.69	4.09
50	0.47	0.62	1.51	1.86	2.38	2.74	3.25	3.64	4.04
51	0.46	0.62	1.49	1.84	2.35	2.7	3.21	3.6	3.99
52	0.46	0.61	1.47	1.81	2.32	2.67	3.17	3.55	3.94
53	0.45	0.60	1.45	1.79	2.29	2.64	3.13	3.51	3.89
54	0.44	0.59	1.44	1.77	2.26	2.6	3.09	3.47	3.85
55	0.44	0.59	1.42	1.75	2.24	2.57	3.06	3.43	3.8
56	0.43	0.58	1.4	1.73	2.21	2.55	3.02	3.39	3.76
57	0.43	0.57	1.39	1.71	2.18	2.52	2.99	3.35	3.72
58	0.42	0.57	1.37	1.69	2.16	2.49	2.96	3.32	3.68
59	0.42	0.56	1.35	1.67	2.14	2.46	2.92	3.28	3.64
60	0.41	0.55	1.34	1.65	2.11	2.43	2.89	3.25	3.6

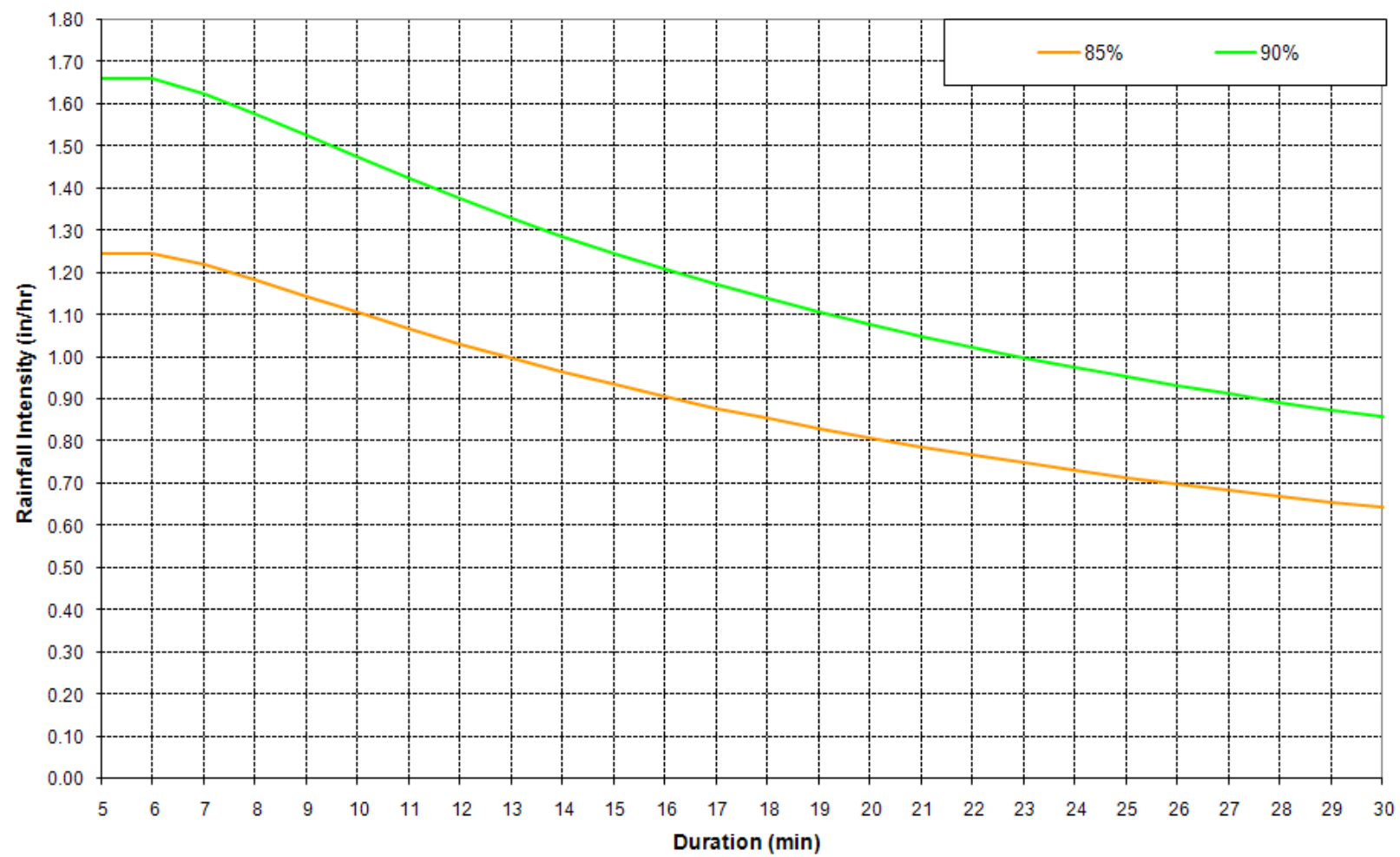
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Hutchinson, Kansas



Hutchinson, Kansas

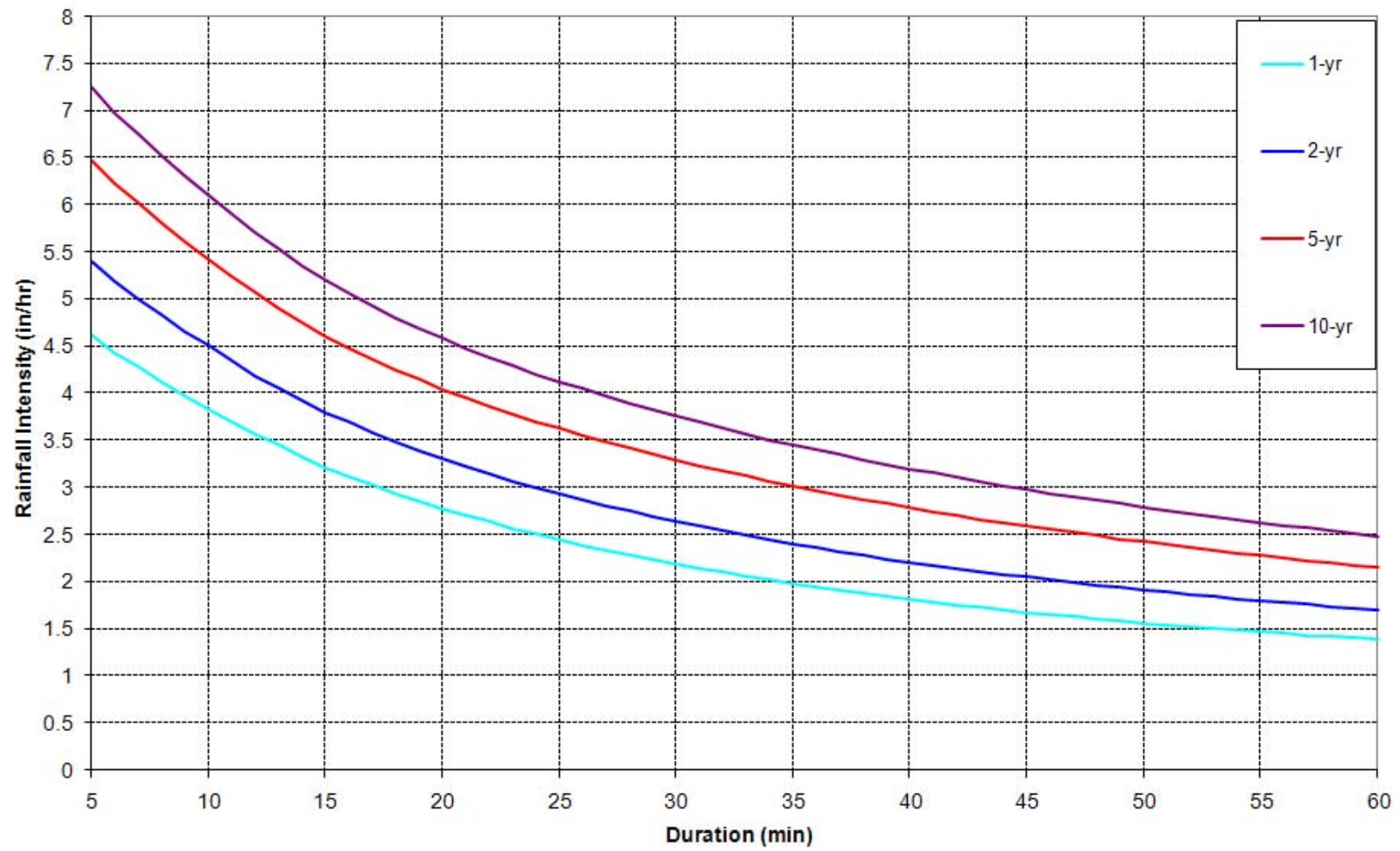


Lawrence, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.25	1.63	4.63	5.4	6.48	7.26	8.41	9.31	10.2
6	1.25	1.63	4.44	5.19	6.23	6.99	8.1	8.97	9.84
7	1.22	1.60	4.28	5	6.02	6.75	7.83	8.68	9.52
8	1.18	1.55	4.12	4.83	5.82	6.53	7.58	8.4	9.22
9	1.15	1.50	3.98	4.66	5.62	6.32	7.34	8.13	8.93
10	1.11	1.45	3.84	4.5	5.43	6.11	7.1	7.87	8.64
11	1.07	1.40	3.7	4.34	5.25	5.91	6.87	7.61	8.36
12	1.03	1.35	3.57	4.19	5.08	5.71	6.64	7.37	8.09
13	1.00	1.31	3.45	4.05	4.91	5.53	6.43	7.14	7.84
14	0.96	1.27	3.33	3.92	4.76	5.36	6.24	6.93	7.61
15	0.93	1.23	3.22	3.8	4.62	5.21	6.06	6.73	7.4
16	0.91	1.19	3.12	3.69	4.49	5.06	5.9	6.56	7.21
17	0.88	1.15	3.03	3.58	4.37	4.93	5.75	6.39	7.03
18	0.85	1.12	2.94	3.48	4.26	4.81	5.61	6.24	6.86
19	0.83	1.09	2.86	3.39	4.15	4.69	5.48	6.1	6.71
20	0.81	1.06	2.78	3.3	4.05	4.59	5.36	5.97	6.57
21	0.79	1.03	2.71	3.22	3.96	4.48	5.25	5.84	6.43
22	0.77	1.01	2.64	3.14	3.87	4.39	5.14	5.72	6.3
23	0.75	0.98	2.57	3.07	3.79	4.3	5.03	5.61	6.18
24	0.73	0.96	2.51	3	3.71	4.21	4.94	5.5	6.06
25	0.72	0.94	2.45	2.93	3.63	4.13	4.84	5.4	5.95
26	0.70	0.92	2.39	2.87	3.56	4.05	4.75	5.3	5.85
27	0.68	0.90	2.34	2.81	3.49	3.97	4.67	5.21	5.74
28	0.67	0.88	2.29	2.75	3.42	3.9	4.58	5.12	5.65
29	0.66	0.86	2.24	2.69	3.36	3.83	4.5	5.03	5.55
30	0.64	0.84	2.19	2.64	3.3	3.76	4.43	4.94	5.46
31	0.63	0.83	2.14	2.59	3.24	3.7	4.35	4.86	5.37
32	0.62	0.81	2.1	2.54	3.18	3.63	4.28	4.78	5.29
33	0.61	0.80	2.06	2.49	3.13	3.57	4.21	4.71	5.2
34	0.60	0.78	2.02	2.45	3.07	3.51	4.14	4.64	5.12
35	0.59	0.77	1.98	2.4	3.02	3.46	4.08	4.56	5.05
36	0.58	0.76	1.94	2.36	2.97	3.4	4.02	4.5	4.97
37	0.57	0.74	1.91	2.32	2.93	3.35	3.96	4.43	4.9
38	0.56	0.73	1.88	2.28	2.88	3.3	3.9	4.36	4.83
39	0.55	0.72	1.84	2.24	2.84	3.25	3.84	4.3	4.76
40	0.54	0.71	1.81	2.21	2.79	3.2	3.78	4.24	4.69
41	0.53	0.70	1.78	2.17	2.75	3.16	3.73	4.18	4.62
42	0.52	0.69	1.75	2.14	2.71	3.11	3.68	4.12	4.56
43	0.52	0.68	1.73	2.11	2.67	3.07	3.63	4.07	4.5
44	0.51	0.67	1.7	2.08	2.63	3.02	3.58	4.01	4.44
45	0.50	0.66	1.67	2.05	2.6	2.98	3.53	3.96	4.38
46	0.49	0.65	1.65	2.02	2.56	2.94	3.48	3.9	4.32
47	0.49	0.64	1.63	1.99	2.53	2.9	3.44	3.85	4.27
48	0.48	0.63	1.6	1.96	2.5	2.87	3.39	3.8	4.21
49	0.47	0.62	1.58	1.94	2.46	2.83	3.35	3.76	4.16
50	0.47	0.61	1.56	1.91	2.43	2.79	3.31	3.71	4.11
51	0.46	0.60	1.54	1.89	2.4	2.76	3.27	3.66	4.06
52	0.46	0.60	1.52	1.86	2.37	2.72	3.23	3.62	4.01
53	0.45	0.59	1.5	1.84	2.34	2.69	3.19	3.58	3.96
54	0.44	0.58	1.48	1.82	2.31	2.66	3.15	3.53	3.91
55	0.44	0.58	1.47	1.8	2.29	2.63	3.11	3.49	3.87
56	0.43	0.57	1.45	1.78	2.26	2.6	3.08	3.45	3.82
57	0.43	0.56	1.43	1.76	2.23	2.57	3.04	3.41	3.78
58	0.42	0.56	1.42	1.74	2.21	2.54	3.01	3.37	3.73
59	0.42	0.55	1.4	1.72	2.18	2.51	2.97	3.33	3.69
60	0.41	0.54	1.39	1.7	2.16	2.48	2.94	3.3	3.65

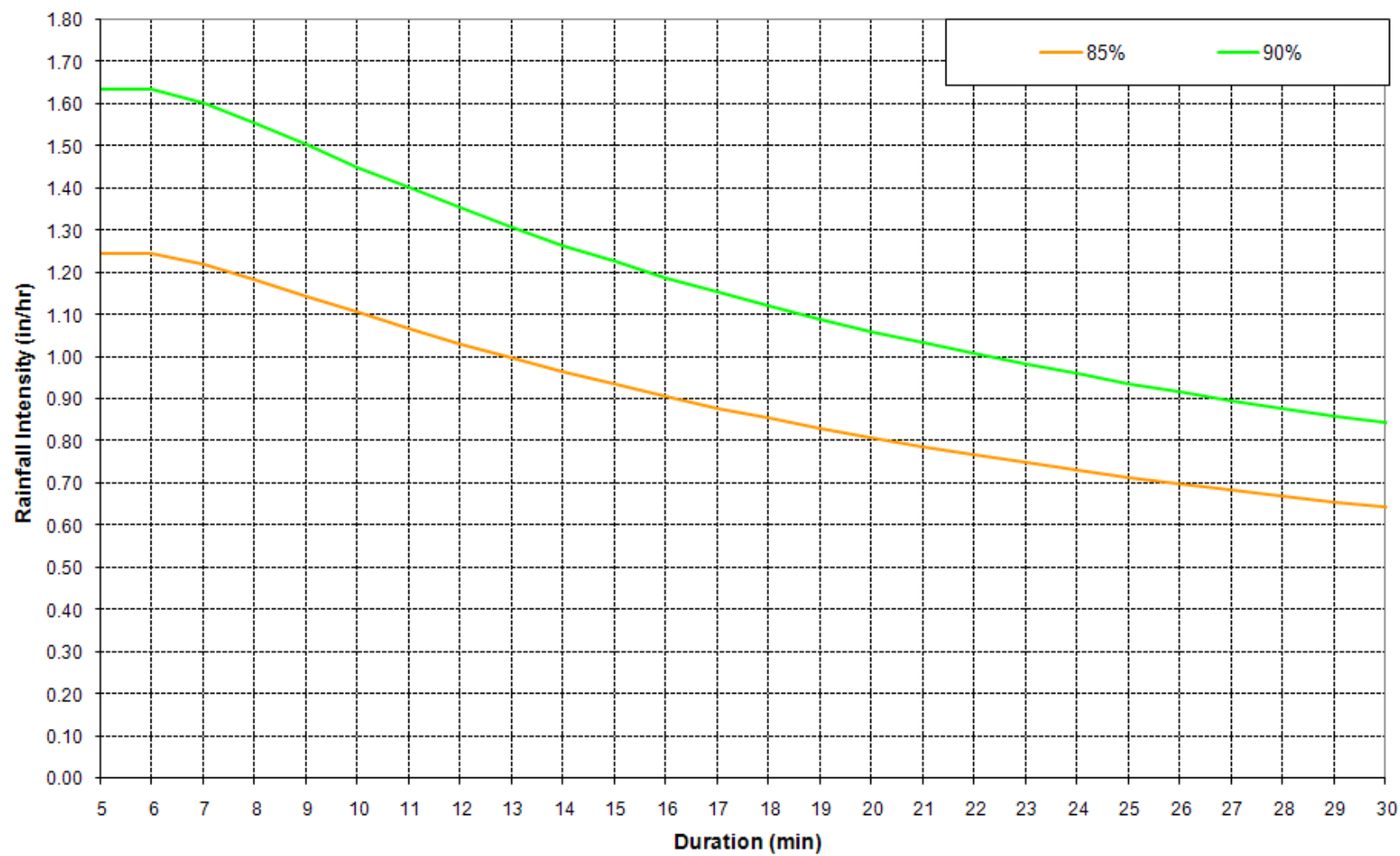
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Lawrence, Kansas



Lawrence, Kansas

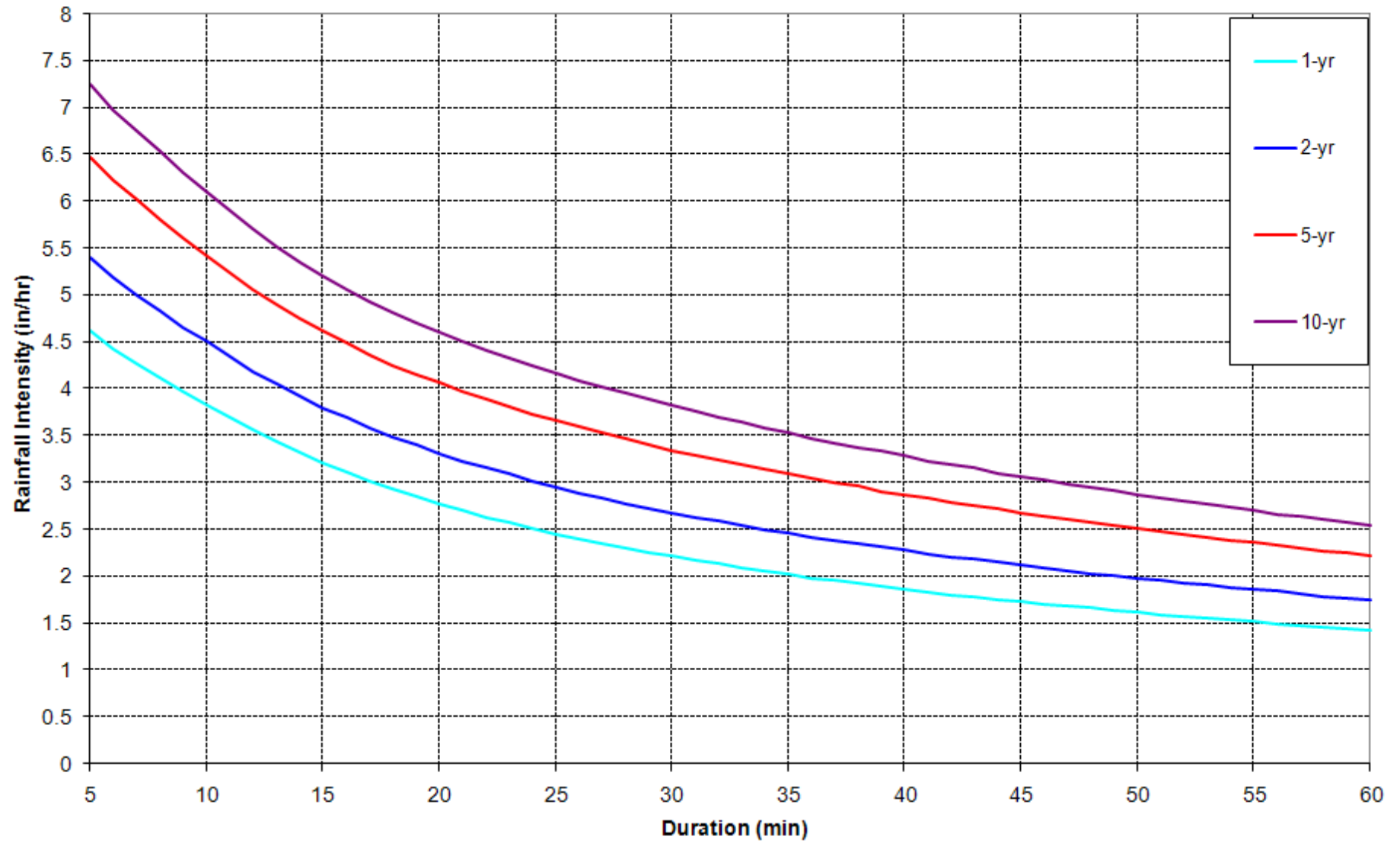


Manhattan, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.14	1.52	4.63	5.4	6.48	7.26	8.41	9.31	10.2
6	1.14	1.52	4.44	5.19	6.23	6.99	8.1	8.98	9.84
7	1.11	1.49	4.28	5	6.02	6.76	7.84	8.68	9.52
8	1.08	1.45	4.12	4.83	5.82	6.54	7.58	8.41	9.22
9	1.04	1.40	3.98	4.66	5.62	6.32	7.34	8.14	8.93
10	1.01	1.35	3.84	4.5	5.43	6.11	7.1	7.87	8.64
11	0.97	1.31	3.7	4.34	5.25	5.91	6.86	7.61	8.36
12	0.94	1.26	3.57	4.19	5.07	5.71	6.64	7.36	8.09
13	0.91	1.22	3.45	4.05	4.91	5.53	6.43	7.14	7.84
14	0.88	1.18	3.33	3.92	4.76	5.36	6.24	6.92	7.61
15	0.85	1.14	3.22	3.8	4.62	5.21	6.06	6.73	7.4
16	0.83	1.11	3.12	3.69	4.49	5.07	5.91	6.56	7.21
17	0.80	1.07	3.03	3.58	4.37	4.94	5.76	6.4	7.04
18	0.78	1.04	2.94	3.49	4.26	4.82	5.63	6.26	6.89
19	0.76	1.02	2.86	3.4	4.16	4.71	5.5	6.12	6.74
20	0.74	0.99	2.78	3.31	4.07	4.61	5.39	6	6.6
21	0.72	0.96	2.71	3.23	3.98	4.51	5.28	5.88	6.48
22	0.70	0.94	2.64	3.16	3.89	4.42	5.18	5.77	6.36
23	0.68	0.92	2.58	3.09	3.81	4.33	5.08	5.66	6.24
24	0.67	0.89	2.52	3.02	3.74	4.25	4.99	5.56	6.13
25	0.65	0.87	2.46	2.95	3.67	4.17	4.9	5.46	6.03
26	0.64	0.85	2.41	2.89	3.6	4.1	4.81	5.37	5.93
27	0.62	0.84	2.36	2.84	3.53	4.03	4.73	5.28	5.83
28	0.61	0.82	2.31	2.78	3.47	3.96	4.65	5.2	5.74
29	0.60	0.80	2.26	2.73	3.41	3.89	4.58	5.11	5.65
30	0.59	0.79	2.22	2.68	3.35	3.83	4.5	5.03	5.56
31	0.57	0.77	2.18	2.63	3.3	3.76	4.43	4.96	5.48
32	0.56	0.76	2.14	2.59	3.24	3.7	4.37	4.88	5.39
33	0.55	0.74	2.1	2.54	3.19	3.65	4.3	4.81	5.31
34	0.54	0.73	2.06	2.5	3.14	3.59	4.24	4.74	5.24
35	0.53	0.72	2.03	2.46	3.09	3.54	4.17	4.67	5.16
36	0.52	0.70	1.99	2.42	3.05	3.48	4.11	4.6	5.09
37	0.52	0.69	1.96	2.38	3	3.43	4.05	4.54	5.01
38	0.51	0.68	1.93	2.35	2.96	3.38	4	4.47	4.95
39	0.50	0.67	1.9	2.31	2.91	3.34	3.94	4.41	4.88
40	0.49	0.66	1.87	2.28	2.87	3.29	3.88	4.35	4.81
41	0.48	0.65	1.84	2.24	2.83	3.24	3.83	4.29	4.75
42	0.48	0.64	1.81	2.21	2.79	3.2	3.78	4.23	4.68
43	0.47	0.63	1.79	2.18	2.75	3.16	3.73	4.18	4.62
44	0.46	0.62	1.76	2.15	2.72	3.11	3.68	4.12	4.56
45	0.46	0.61	1.74	2.12	2.68	3.07	3.63	4.07	4.5
46	0.45	0.60	1.71	2.09	2.64	3.03	3.58	4.02	4.44
47	0.44	0.59	1.69	2.06	2.61	2.99	3.54	3.96	4.39
48	0.44	0.59	1.67	2.03	2.57	2.95	3.49	3.91	4.33
49	0.43	0.58	1.64	2.01	2.54	2.92	3.45	3.86	4.28
50	0.43	0.57	1.62	1.98	2.51	2.88	3.41	3.82	4.22
51	0.42	0.56	1.6	1.96	2.48	2.84	3.36	3.77	4.17
52	0.42	0.56	1.58	1.93	2.45	2.81	3.32	3.72	4.12
53	0.41	0.55	1.56	1.91	2.42	2.77	3.28	3.68	4.07
54	0.40	0.54	1.54	1.88	2.39	2.74	3.24	3.63	4.02
55	0.40	0.54	1.52	1.86	2.36	2.71	3.2	3.59	3.98
56	0.40	0.53	1.5	1.84	2.33	2.67	3.17	3.55	3.93
57	0.39	0.52	1.48	1.81	2.3	2.64	3.13	3.51	3.88
58	0.39	0.52	1.46	1.79	2.27	2.61	3.09	3.47	3.84
59	0.38	0.51	1.45	1.77	2.25	2.58	3.06	3.43	3.79
60	0.38	0.51	1.43	1.75	2.22	2.55	3.02	3.39	3.75

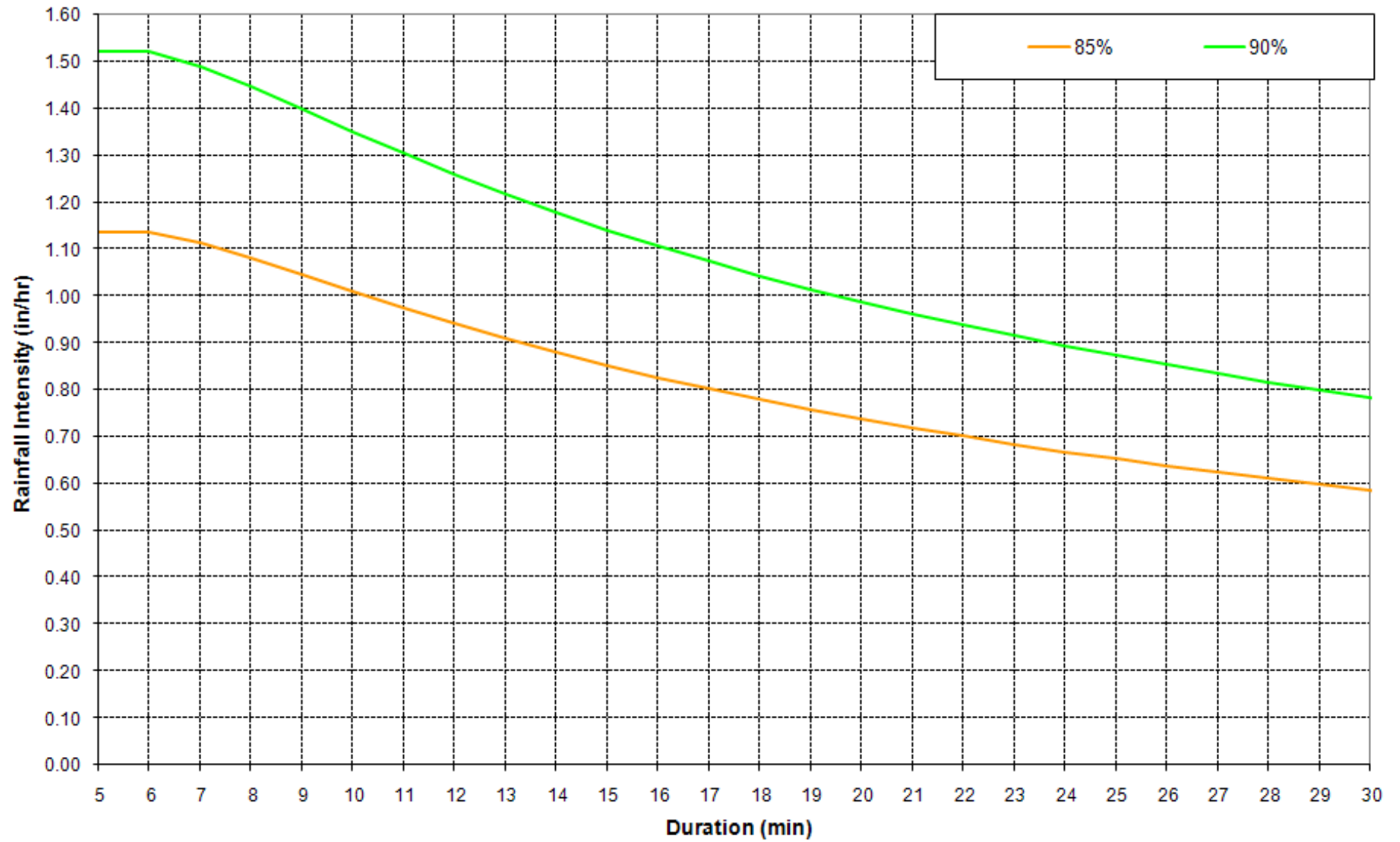
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Manhattan, Kansas



Manhattan, Kansas

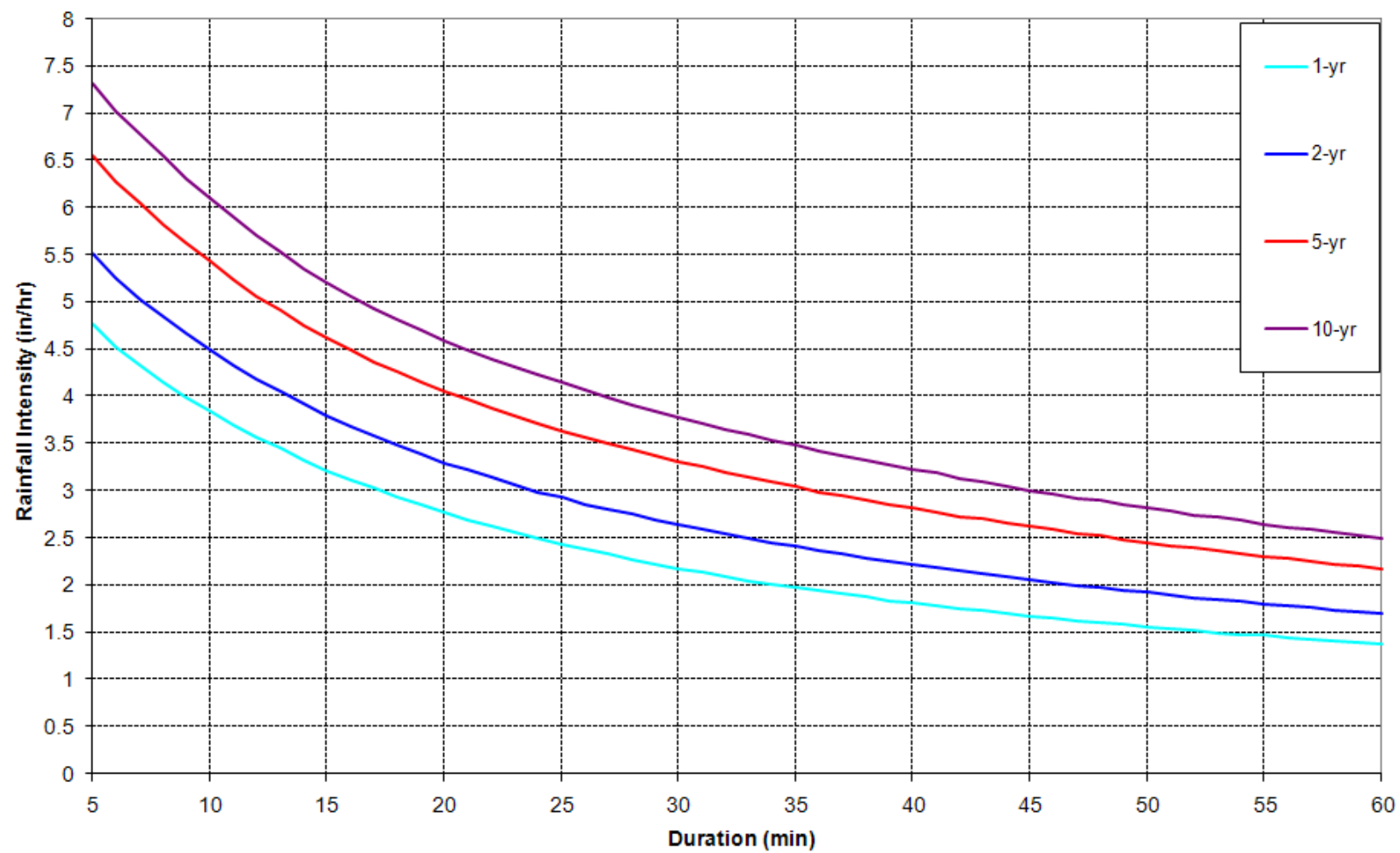


Newton, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.25	1.66	4.77	5.52	6.56	7.32	8.44	9.32	10.2
6	1.25	1.66	4.53	5.26	6.28	7.03	8.13	8.99	9.84
7	1.22	1.63	4.33	5.04	6.05	6.78	7.85	8.69	9.52
8	1.18	1.58	4.15	4.85	5.83	6.55	7.59	8.41	9.22
9	1.15	1.53	3.99	4.67	5.63	6.32	7.34	8.14	8.93
10	1.11	1.47	3.84	4.5	5.43	6.11	7.1	7.87	8.64
11	1.07	1.42	3.7	4.34	5.25	5.91	6.86	7.61	8.36
12	1.03	1.38	3.57	4.19	5.07	5.71	6.64	7.37	8.09
13	1.00	1.33	3.45	4.05	4.91	5.53	6.43	7.14	7.84
14	0.96	1.29	3.33	3.92	4.76	5.36	6.24	6.93	7.61
15	0.93	1.25	3.22	3.8	4.62	5.21	6.06	6.73	7.4
16	0.91	1.21	3.12	3.69	4.49	5.07	5.9	6.56	7.21
17	0.88	1.17	3.03	3.58	4.37	4.94	5.76	6.4	7.04
18	0.85	1.14	2.94	3.48	4.26	4.82	5.62	6.25	6.88
19	0.83	1.11	2.85	3.39	4.15	4.7	5.5	6.12	6.73
20	0.81	1.08	2.77	3.3	4.06	4.6	5.38	5.99	6.59
21	0.79	1.05	2.7	3.22	3.97	4.5	5.27	5.87	6.46
22	0.77	1.02	2.63	3.14	3.88	4.4	5.16	5.75	6.34
23	0.75	1.00	2.56	3.06	3.8	4.31	5.06	5.64	6.22
24	0.73	0.98	2.5	2.99	3.72	4.23	4.97	5.54	6.11
25	0.72	0.95	2.44	2.93	3.64	4.15	4.87	5.44	6
26	0.70	0.93	2.38	2.86	3.57	4.07	4.79	5.34	5.9
27	0.68	0.91	2.33	2.8	3.5	4	4.7	5.25	5.8
28	0.67	0.89	2.27	2.75	3.44	3.92	4.62	5.16	5.7
29	0.66	0.88	2.23	2.69	3.37	3.85	4.54	5.08	5.61
30	0.64	0.86	2.18	2.64	3.31	3.79	4.47	4.99	5.52
31	0.63	0.84	2.14	2.59	3.26	3.72	4.39	4.91	5.43
32	0.62	0.83	2.09	2.54	3.2	3.66	4.32	4.84	5.35
33	0.61	0.81	2.05	2.5	3.15	3.6	4.25	4.76	5.26
34	0.60	0.80	2.01	2.45	3.09	3.54	4.19	4.69	5.18
35	0.59	0.78	1.98	2.41	3.04	3.49	4.12	4.62	5.11
36	0.58	0.77	1.94	2.37	2.99	3.43	4.06	4.55	5.03
37	0.57	0.75	1.91	2.33	2.95	3.38	4	4.48	4.96
38	0.56	0.74	1.88	2.29	2.9	3.33	3.94	4.41	4.89
39	0.55	0.73	1.84	2.25	2.86	3.28	3.88	4.35	4.82
40	0.54	0.72	1.81	2.22	2.82	3.23	3.83	4.29	4.75
41	0.53	0.71	1.79	2.18	2.77	3.19	3.77	4.23	4.68
42	0.52	0.70	1.76	2.15	2.73	3.14	3.72	4.17	4.62
43	0.52	0.69	1.73	2.12	2.7	3.1	3.67	4.11	4.56
44	0.51	0.68	1.7	2.09	2.66	3.05	3.62	4.06	4.5
45	0.50	0.67	1.68	2.06	2.62	3.01	3.57	4	4.44
46	0.49	0.66	1.65	2.03	2.59	2.97	3.52	3.95	4.38
47	0.49	0.65	1.63	2	2.55	2.93	3.48	3.9	4.32
48	0.48	0.64	1.61	1.97	2.52	2.9	3.43	3.85	4.27
49	0.47	0.63	1.59	1.95	2.48	2.86	3.39	3.8	4.21
50	0.47	0.62	1.56	1.92	2.45	2.82	3.35	3.75	4.16
51	0.46	0.62	1.54	1.9	2.42	2.79	3.31	3.71	4.11
52	0.46	0.61	1.52	1.87	2.39	2.75	3.26	3.66	4.06
53	0.45	0.60	1.5	1.85	2.36	2.72	3.23	3.62	4.01
54	0.44	0.59	1.48	1.83	2.33	2.69	3.19	3.58	3.96
55	0.44	0.59	1.47	1.8	2.3	2.65	3.15	3.53	3.92
56	0.43	0.58	1.45	1.78	2.28	2.62	3.11	3.49	3.87
57	0.43	0.57	1.43	1.76	2.25	2.59	3.08	3.45	3.83
58	0.42	0.57	1.41	1.74	2.22	2.56	3.04	3.41	3.78
59	0.42	0.56	1.4	1.72	2.2	2.53	3.01	3.38	3.74
60	0.41	0.55	1.38	1.7	2.17	2.5	2.97	3.34	3.7

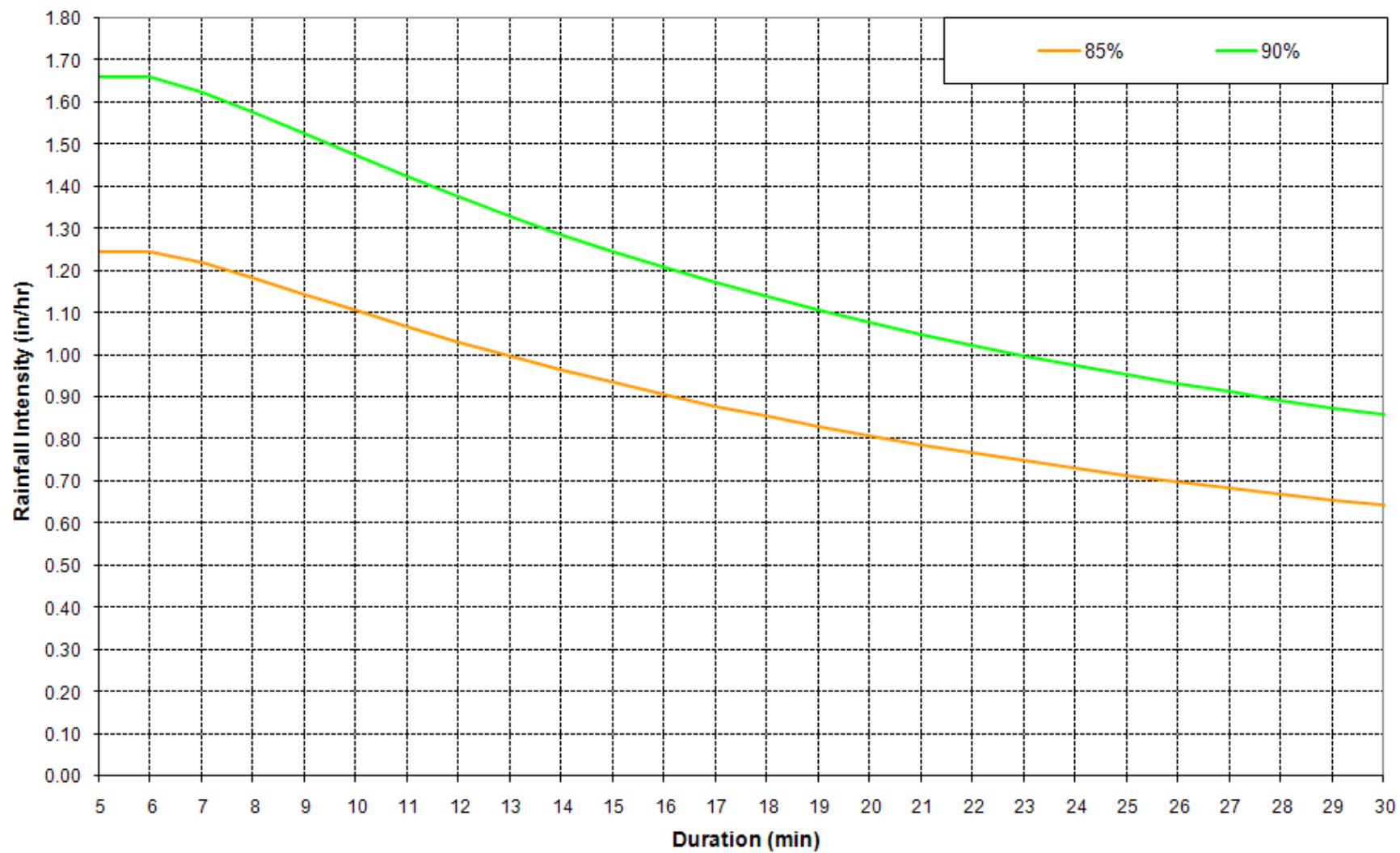
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Newton, Kansas



Newton, Kansas

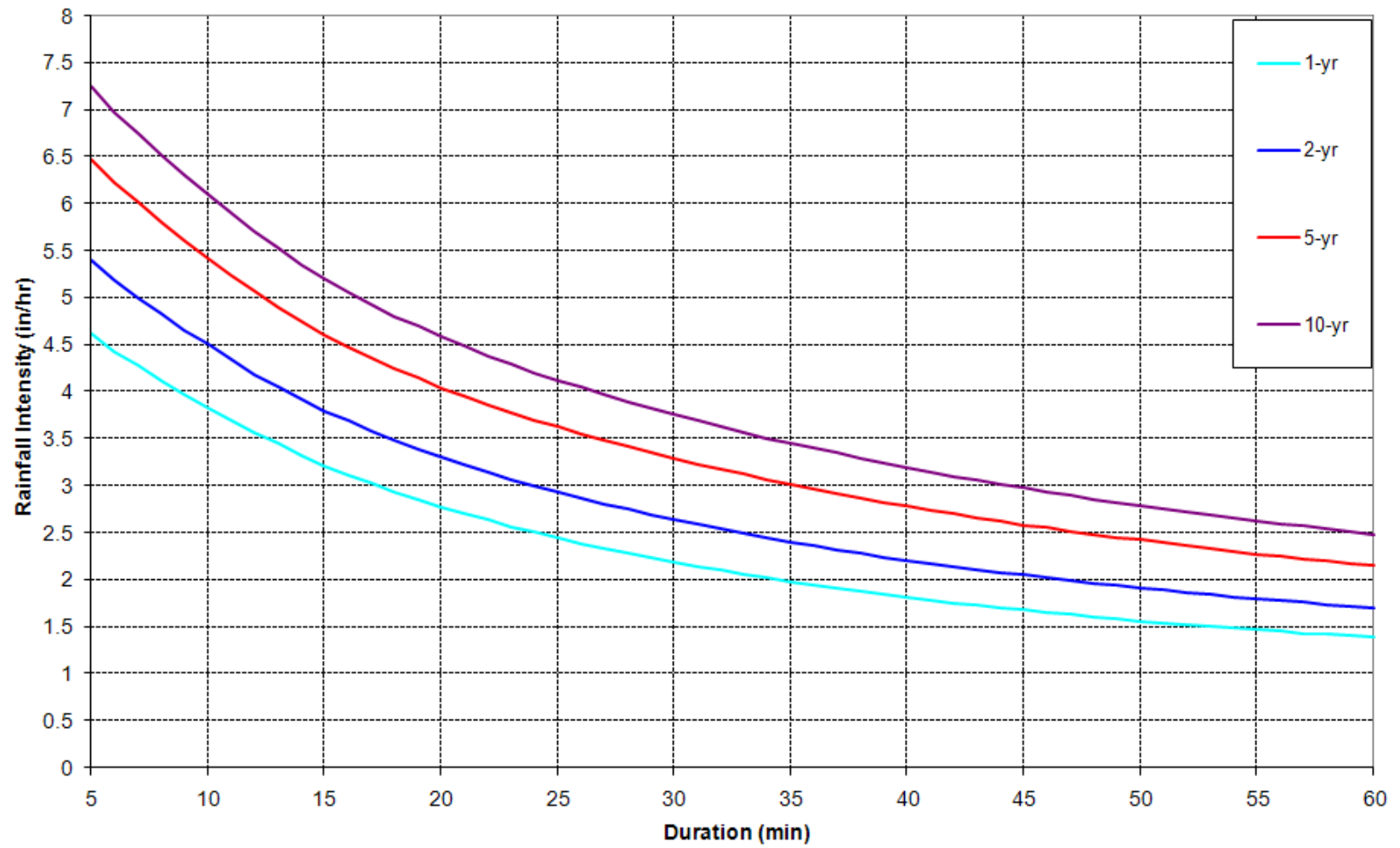


Ottawa, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.25	1.66	4.63	5.4	6.48	7.26	8.41	9.31	10.2
6	1.25	1.66	4.44	5.19	6.23	6.99	8.1	8.97	9.84
7	1.22	1.63	4.28	5	6.02	6.75	7.83	8.68	9.52
8	1.18	1.58	4.12	4.83	5.82	6.53	7.58	8.4	9.22
9	1.15	1.53	3.98	4.66	5.62	6.32	7.34	8.13	8.93
10	1.11	1.47	3.84	4.5	5.43	6.11	7.1	7.87	8.64
11	1.07	1.42	3.7	4.34	5.25	5.91	6.86	7.61	8.36
12	1.03	1.38	3.57	4.19	5.08	5.71	6.64	7.37	8.09
13	1.00	1.33	3.45	4.05	4.91	5.53	6.43	7.14	7.84
14	0.96	1.29	3.33	3.92	4.76	5.36	6.24	6.93	7.61
15	0.93	1.25	3.22	3.8	4.62	5.21	6.06	6.73	7.4
16	0.91	1.21	3.12	3.69	4.49	5.06	5.9	6.56	7.21
17	0.88	1.17	3.03	3.58	4.37	4.93	5.75	6.39	7.03
18	0.85	1.14	2.94	3.48	4.26	4.81	5.61	6.24	6.87
19	0.83	1.11	2.86	3.39	4.15	4.7	5.48	6.1	6.71
20	0.81	1.08	2.78	3.3	4.05	4.59	5.36	5.97	6.57
21	0.79	1.05	2.71	3.22	3.96	4.49	5.25	5.84	6.43
22	0.77	1.02	2.64	3.14	3.87	4.39	5.14	5.72	6.31
23	0.75	1.00	2.57	3.07	3.79	4.3	5.04	5.61	6.18
24	0.73	0.98	2.51	3	3.71	4.21	4.94	5.5	6.07
25	0.72	0.95	2.45	2.93	3.63	4.13	4.84	5.4	5.96
26	0.70	0.93	2.39	2.87	3.56	4.05	4.75	5.3	5.85
27	0.68	0.91	2.34	2.81	3.49	3.97	4.67	5.21	5.75
28	0.67	0.89	2.29	2.75	3.42	3.9	4.58	5.12	5.65
29	0.66	0.88	2.24	2.69	3.36	3.83	4.5	5.03	5.55
30	0.64	0.86	2.19	2.64	3.3	3.76	4.43	4.94	5.46
31	0.63	0.84	2.14	2.59	3.24	3.7	4.35	4.86	5.37
32	0.62	0.83	2.1	2.54	3.18	3.63	4.28	4.78	5.28
33	0.61	0.81	2.06	2.49	3.13	3.57	4.21	4.71	5.2
34	0.60	0.80	2.02	2.45	3.07	3.51	4.14	4.63	5.12
35	0.59	0.78	1.98	2.4	3.02	3.45	4.08	4.56	5.04
36	0.58	0.77	1.94	2.36	2.97	3.4	4.01	4.49	4.96
37	0.57	0.75	1.91	2.32	2.92	3.35	3.95	4.42	4.89
38	0.56	0.74	1.88	2.28	2.88	3.29	3.89	4.36	4.82
39	0.55	0.73	1.84	2.24	2.83	3.24	3.83	4.29	4.75
40	0.54	0.72	1.81	2.21	2.79	3.2	3.78	4.23	4.68
41	0.53	0.71	1.78	2.17	2.75	3.15	3.72	4.17	4.61
42	0.52	0.70	1.75	2.14	2.71	3.1	3.67	4.11	4.55
43	0.52	0.69	1.73	2.11	2.67	3.06	3.62	4.06	4.49
44	0.51	0.68	1.7	2.08	2.63	3.02	3.57	4	4.43
45	0.50	0.67	1.68	2.05	2.59	2.98	3.52	3.95	4.37
46	0.49	0.66	1.65	2.02	2.56	2.94	3.48	3.9	4.31
47	0.49	0.65	1.63	1.99	2.52	2.9	3.43	3.84	4.26
48	0.48	0.64	1.6	1.96	2.49	2.86	3.39	3.8	4.2
49	0.47	0.63	1.58	1.94	2.46	2.82	3.34	3.75	4.15
50	0.47	0.62	1.56	1.91	2.43	2.79	3.3	3.7	4.1
51	0.46	0.62	1.54	1.89	2.4	2.75	3.26	3.66	4.05
52	0.46	0.61	1.52	1.86	2.37	2.72	3.22	3.61	4
53	0.45	0.60	1.5	1.84	2.34	2.69	3.18	3.57	3.95
54	0.44	0.59	1.49	1.82	2.31	2.66	3.15	3.53	3.91
55	0.44	0.59	1.47	1.8	2.28	2.62	3.11	3.49	3.86
56	0.43	0.58	1.45	1.78	2.26	2.59	3.07	3.45	3.82
57	0.43	0.57	1.43	1.76	2.23	2.57	3.04	3.41	3.77
58	0.42	0.57	1.42	1.74	2.21	2.54	3.01	3.37	3.73
59	0.42	0.56	1.4	1.72	2.18	2.51	2.97	3.33	3.69
60	0.41	0.55	1.39	1.7	2.16	2.48	2.94	3.3	3.65

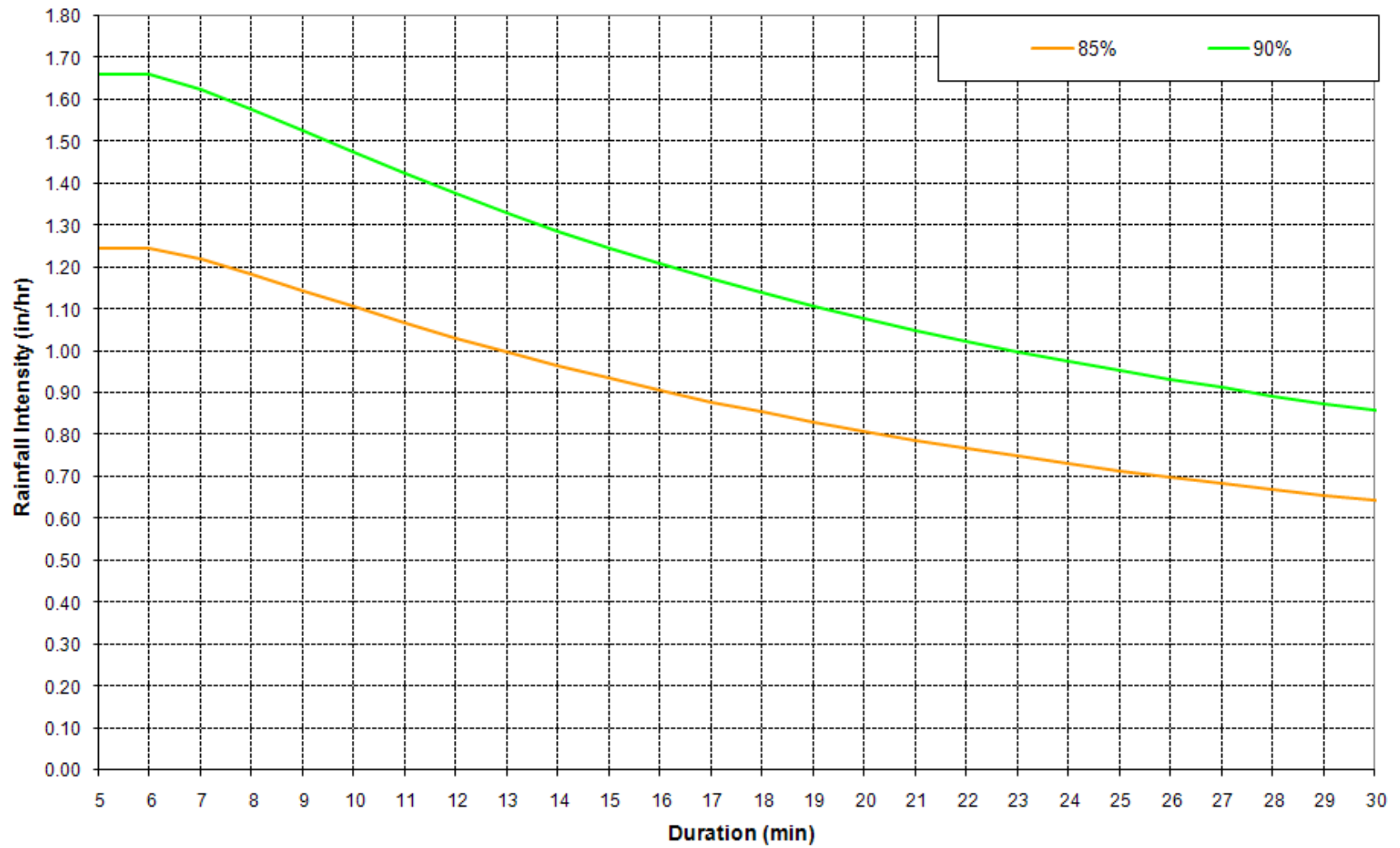
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Ottawa, Kansas



Ottawa, Kansas

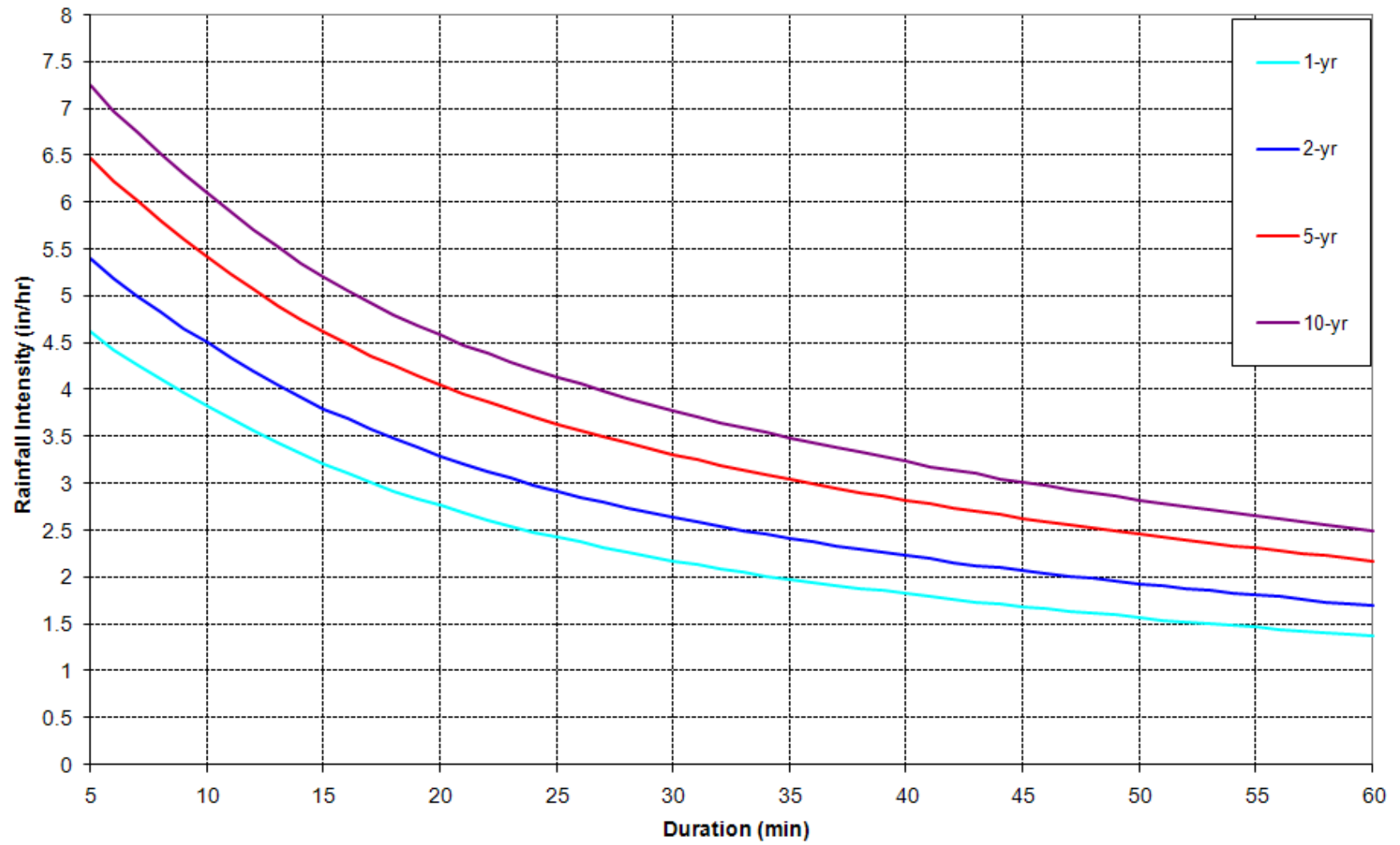


Salina, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.11	1.48	4.63	5.4	6.48	7.26	8.41	9.31	10.2
6	1.11	1.48	4.44	5.19	6.23	6.99	8.1	8.97	9.84
7	1.08	1.45	4.28	5	6.02	6.76	7.84	8.68	9.52
8	1.05	1.41	4.12	4.83	5.82	6.53	7.58	8.4	9.22
9	1.02	1.36	3.98	4.66	5.62	6.32	7.34	8.14	8.93
10	0.98	1.32	3.84	4.5	5.43	6.11	7.1	7.87	8.64
11	0.95	1.27	3.7	4.34	5.25	5.91	6.86	7.61	8.36
12	0.92	1.23	3.57	4.2	5.08	5.71	6.64	7.37	8.09
13	0.89	1.19	3.45	4.06	4.91	5.53	6.43	7.14	7.84
14	0.86	1.15	3.33	3.92	4.76	5.36	6.24	6.93	7.61
15	0.83	1.11	3.22	3.8	4.62	5.21	6.06	6.73	7.4
16	0.81	1.08	3.12	3.69	4.49	5.07	5.9	6.56	7.21
17	0.78	1.05	3.02	3.58	4.37	4.93	5.76	6.4	7.04
18	0.76	1.02	2.93	3.48	4.26	4.81	5.62	6.25	6.88
19	0.74	0.99	2.85	3.38	4.15	4.7	5.49	6.11	6.73
20	0.72	0.96	2.77	3.29	4.05	4.59	5.37	5.98	6.59
21	0.70	0.94	2.69	3.21	3.96	4.49	5.26	5.86	6.46
22	0.68	0.91	2.62	3.13	3.87	4.4	5.16	5.75	6.34
23	0.67	0.89	2.55	3.06	3.79	4.31	5.06	5.64	6.22
24	0.65	0.87	2.49	2.99	3.71	4.23	4.96	5.54	6.11
25	0.64	0.85	2.43	2.92	3.64	4.14	4.87	5.44	6
26	0.62	0.83	2.38	2.86	3.57	4.07	4.78	5.34	5.9
27	0.61	0.81	2.32	2.8	3.5	3.99	4.7	5.25	5.8
28	0.60	0.80	2.27	2.74	3.44	3.92	4.62	5.16	5.7
29	0.58	0.78	2.22	2.69	3.37	3.85	4.54	5.08	5.61
30	0.57	0.76	2.18	2.64	3.31	3.79	4.47	4.99	5.52
31	0.56	0.75	2.14	2.59	3.26	3.72	4.39	4.91	5.43
32	0.55	0.74	2.1	2.54	3.2	3.66	4.32	4.84	5.35
33	0.54	0.72	2.06	2.5	3.15	3.6	4.26	4.76	5.27
34	0.53	0.71	2.02	2.46	3.1	3.55	4.19	4.69	5.19
35	0.52	0.70	1.98	2.42	3.05	3.49	4.13	4.62	5.11
36	0.51	0.68	1.95	2.38	3	3.44	4.06	4.55	5.04
37	0.50	0.67	1.92	2.34	2.95	3.39	4	4.48	4.96
38	0.50	0.66	1.89	2.3	2.91	3.34	3.95	4.42	4.89
39	0.49	0.65	1.86	2.26	2.87	3.29	3.89	4.36	4.82
40	0.48	0.64	1.83	2.23	2.82	3.24	3.83	4.3	4.75
41	0.47	0.63	1.8	2.2	2.78	3.19	3.78	4.24	4.69
42	0.46	0.62	1.77	2.16	2.74	3.15	3.73	4.18	4.63
43	0.46	0.61	1.74	2.13	2.71	3.11	3.68	4.12	4.56
44	0.45	0.60	1.72	2.1	2.67	3.06	3.63	4.07	4.5
45	0.44	0.59	1.69	2.07	2.63	3.02	3.58	4.01	4.44
46	0.44	0.59	1.67	2.04	2.6	2.98	3.53	3.96	4.39
47	0.43	0.58	1.64	2.01	2.56	2.94	3.49	3.91	4.33
48	0.43	0.57	1.62	1.99	2.53	2.9	3.44	3.86	4.27
49	0.42	0.56	1.6	1.96	2.49	2.87	3.4	3.81	4.22
50	0.42	0.56	1.58	1.93	2.46	2.83	3.35	3.76	4.17
51	0.41	0.55	1.55	1.91	2.43	2.79	3.31	3.71	4.12
52	0.40	0.54	1.53	1.88	2.4	2.76	3.27	3.67	4.07
53	0.40	0.53	1.51	1.86	2.37	2.72	3.23	3.62	4.02
54	0.40	0.53	1.49	1.83	2.34	2.69	3.19	3.58	3.97
55	0.39	0.52	1.47	1.81	2.31	2.66	3.15	3.54	3.92
56	0.39	0.52	1.45	1.79	2.28	2.63	3.12	3.5	3.87
57	0.38	0.51	1.43	1.76	2.25	2.59	3.08	3.46	3.83
58	0.38	0.50	1.42	1.74	2.23	2.56	3.04	3.42	3.79
59	0.37	0.50	1.4	1.72	2.2	2.53	3.01	3.38	3.74
60	0.37	0.49	1.38	1.7	2.17	2.5	2.97	3.34	3.7

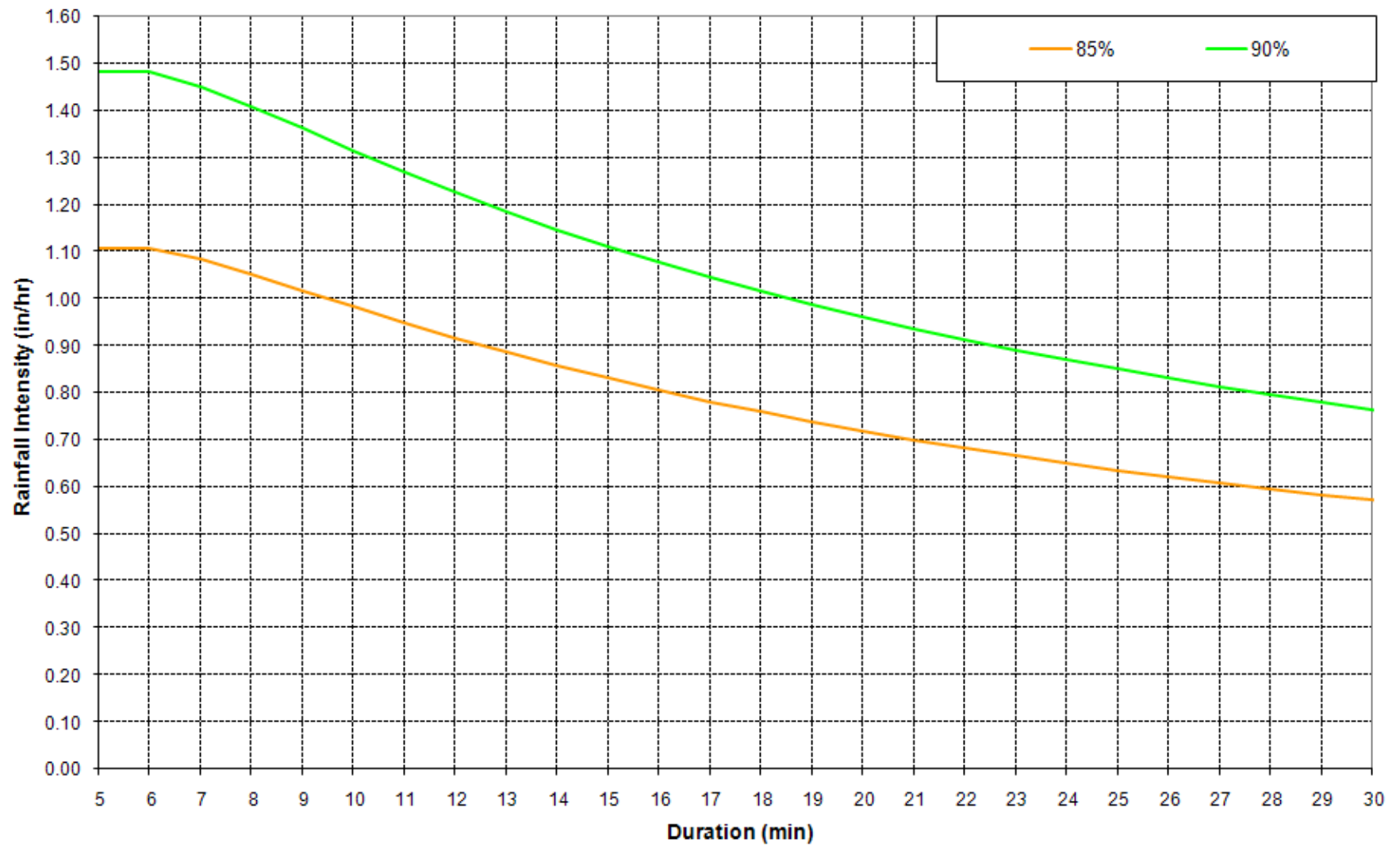
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

Salina, Kansas



Salina, Kansas

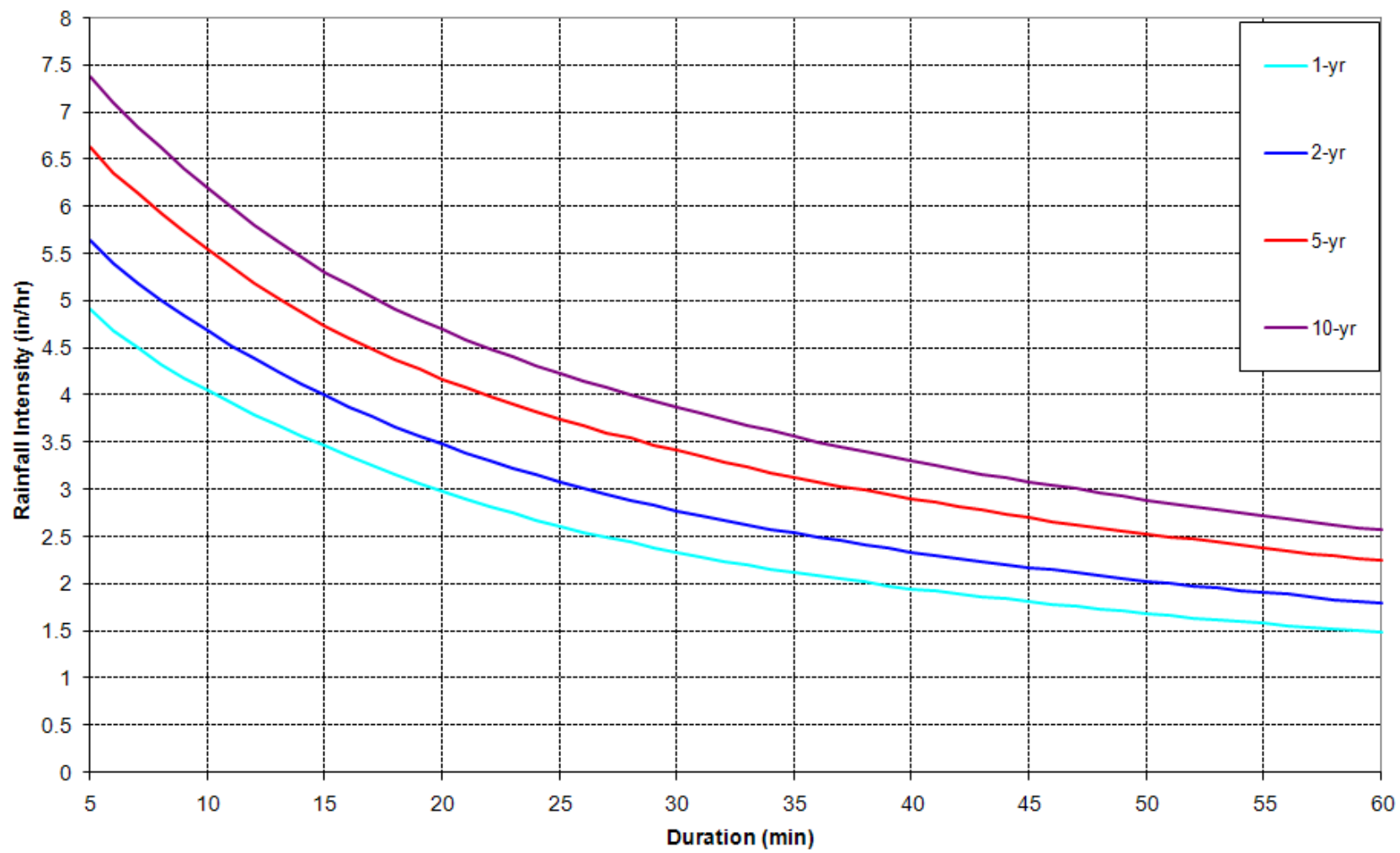


Winfield, Kansas Rainfall Intensity									
Duration (minute)	85% ¹	90% ¹	1-yr ²	2-yr ²	5-yr ²	10-yr ²	25-yr ²	50-yr ²	100-yr ²
	(inch/hour)								
5	1.27	1.66	4.91	5.64	6.64	7.38	8.48	9.34	10.2
6	1.27	1.66	4.69	5.4	6.37	7.1	8.17	9.01	9.84
7	1.25	1.63	4.5	5.19	6.15	6.85	7.89	8.71	9.53
8	1.21	1.58	4.33	5.01	5.94	6.63	7.64	8.43	9.22
9	1.17	1.53	4.18	4.84	5.74	6.41	7.39	8.16	8.93
10	1.13	1.47	4.05	4.68	5.56	6.2	7.15	7.9	8.64
11	1.09	1.42	3.92	4.53	5.38	6	6.92	7.64	8.36
12	1.05	1.38	3.79	4.39	5.2	5.81	6.69	7.39	8.09
13	1.02	1.33	3.68	4.25	5.04	5.63	6.49	7.16	7.83
14	0.99	1.29	3.56	4.12	4.89	5.46	6.3	6.95	7.61
15	0.96	1.25	3.46	4	4.75	5.31	6.12	6.76	7.4
16	0.93	1.21	3.35	3.88	4.62	5.17	5.96	6.59	7.21
17	0.90	1.17	3.25	3.77	4.5	5.04	5.82	6.43	7.05
18	0.87	1.14	3.16	3.67	4.39	4.91	5.69	6.29	6.89
19	0.85	1.11	3.06	3.57	4.28	4.8	5.56	6.16	6.75
20	0.83	1.08	2.98	3.48	4.18	4.7	5.44	6.03	6.61
21	0.81	1.05	2.9	3.39	4.09	4.59	5.33	5.91	6.49
22	0.79	1.02	2.82	3.31	4	4.5	5.23	5.8	6.37
23	0.77	1.00	2.75	3.23	3.92	4.41	5.13	5.69	6.25
24	0.75	0.98	2.68	3.16	3.83	4.32	5.03	5.59	6.14
25	0.73	0.95	2.61	3.08	3.76	4.24	4.94	5.49	6.04
26	0.71	0.93	2.55	3.02	3.68	4.16	4.86	5.4	5.94
27	0.70	0.91	2.49	2.95	3.61	4.09	4.77	5.31	5.84
28	0.68	0.89	2.44	2.89	3.55	4.01	4.69	5.22	5.74
29	0.67	0.88	2.38	2.84	3.48	3.94	4.61	5.13	5.65
30	0.66	0.86	2.34	2.78	3.42	3.88	4.53	5.05	5.56
31	0.64	0.84	2.29	2.73	3.36	3.81	4.46	4.97	5.47
32	0.63	0.83	2.24	2.68	3.3	3.75	4.39	4.89	5.39
33	0.62	0.81	2.2	2.63	3.25	3.69	4.32	4.81	5.3
34	0.61	0.80	2.16	2.58	3.19	3.63	4.25	4.74	5.22
35	0.60	0.78	2.12	2.54	3.14	3.57	4.19	4.67	5.14
36	0.59	0.77	2.09	2.5	3.09	3.51	4.12	4.6	5.07
37	0.58	0.75	2.05	2.46	3.04	3.46	4.06	4.53	4.99
38	0.57	0.74	2.02	2.42	3	3.41	4	4.46	4.92
39	0.56	0.73	1.98	2.38	2.95	3.36	3.94	4.4	4.85
40	0.55	0.72	1.95	2.34	2.91	3.31	3.89	4.34	4.78
41	0.54	0.71	1.92	2.31	2.87	3.26	3.83	4.28	4.72
42	0.53	0.70	1.89	2.27	2.83	3.22	3.78	4.22	4.65
43	0.53	0.69	1.86	2.24	2.79	3.17	3.73	4.16	4.59
44	0.52	0.68	1.84	2.21	2.75	3.13	3.68	4.1	4.53
45	0.51	0.67	1.81	2.18	2.71	3.09	3.63	4.05	4.47
46	0.50	0.66	1.78	2.15	2.67	3.05	3.58	4	4.41
47	0.50	0.65	1.76	2.12	2.64	3.01	3.54	3.95	4.36
48	0.49	0.64	1.73	2.09	2.6	2.97	3.49	3.9	4.3
49	0.48	0.63	1.71	2.06	2.57	2.93	3.45	3.85	4.25
50	0.48	0.62	1.69	2.03	2.54	2.89	3.4	3.8	4.2
51	0.47	0.62	1.67	2.01	2.51	2.86	3.36	3.76	4.15
52	0.47	0.61	1.64	1.98	2.48	2.82	3.32	3.71	4.1
53	0.46	0.60	1.62	1.96	2.45	2.79	3.28	3.67	4.05
54	0.45	0.59	1.6	1.93	2.42	2.76	3.25	3.63	4.01
55	0.45	0.59	1.58	1.91	2.39	2.73	3.21	3.59	3.96
56	0.44	0.58	1.56	1.89	2.36	2.69	3.17	3.55	3.92
57	0.44	0.57	1.54	1.86	2.33	2.66	3.14	3.51	3.87
58	0.43	0.57	1.52	1.84	2.31	2.63	3.1	3.47	3.83
59	0.43	0.56	1.51	1.82	2.28	2.6	3.07	3.43	3.79
60	0.42	0.55	1.49	1.8	2.26	2.58	3.04	3.39	3.75

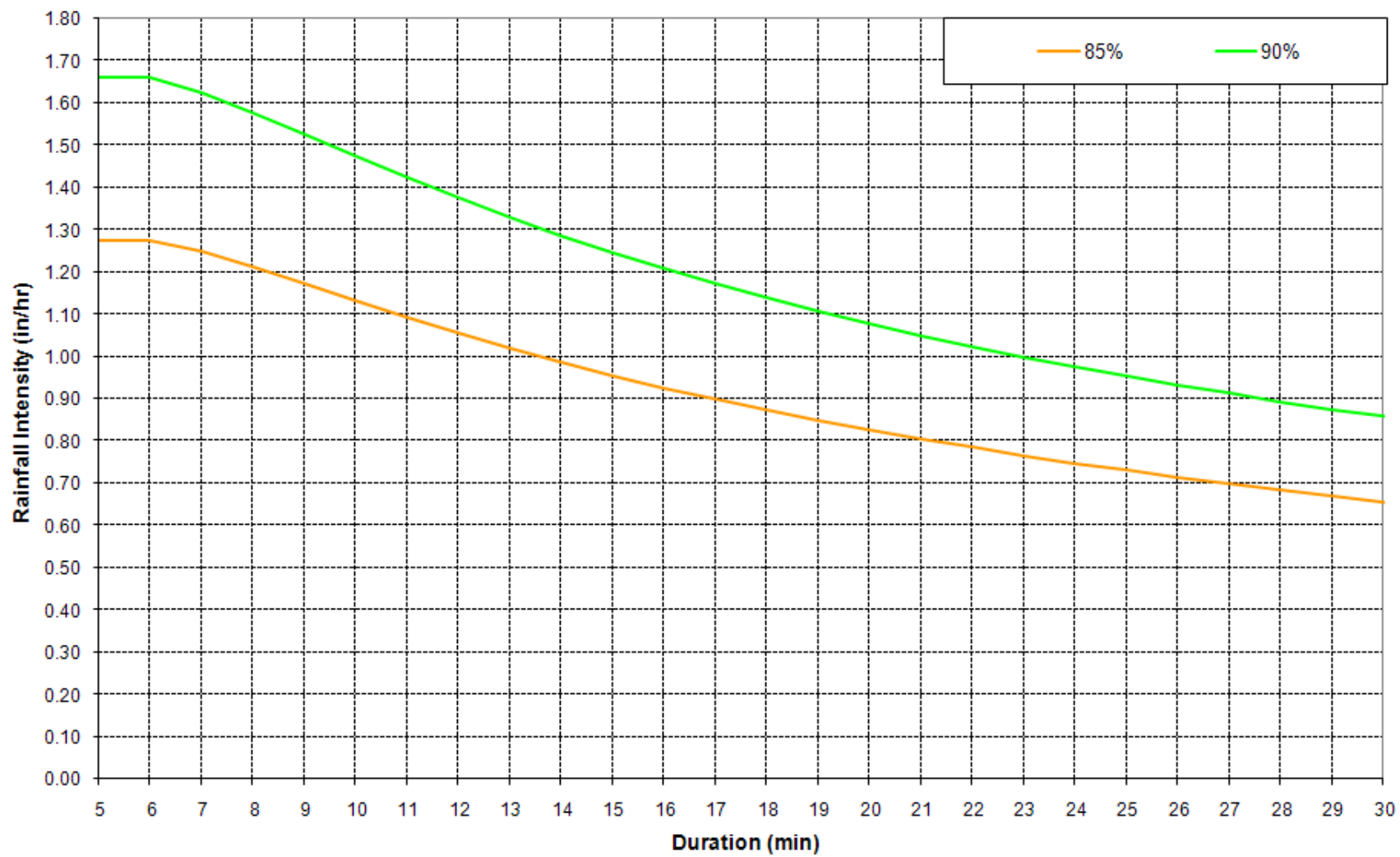
¹ Rainfall intensity for the 85% and 90% events were derived using equations from Young, C. Bryan and McEnroe, B.M., 2002. *Precipitation Frequency Estimates for the Kansas City Metropolitan Area*.

² Rainfall intensity for the 1-yr through 100-yr events are from KDOT, 1997. *Rainfall Intensity*

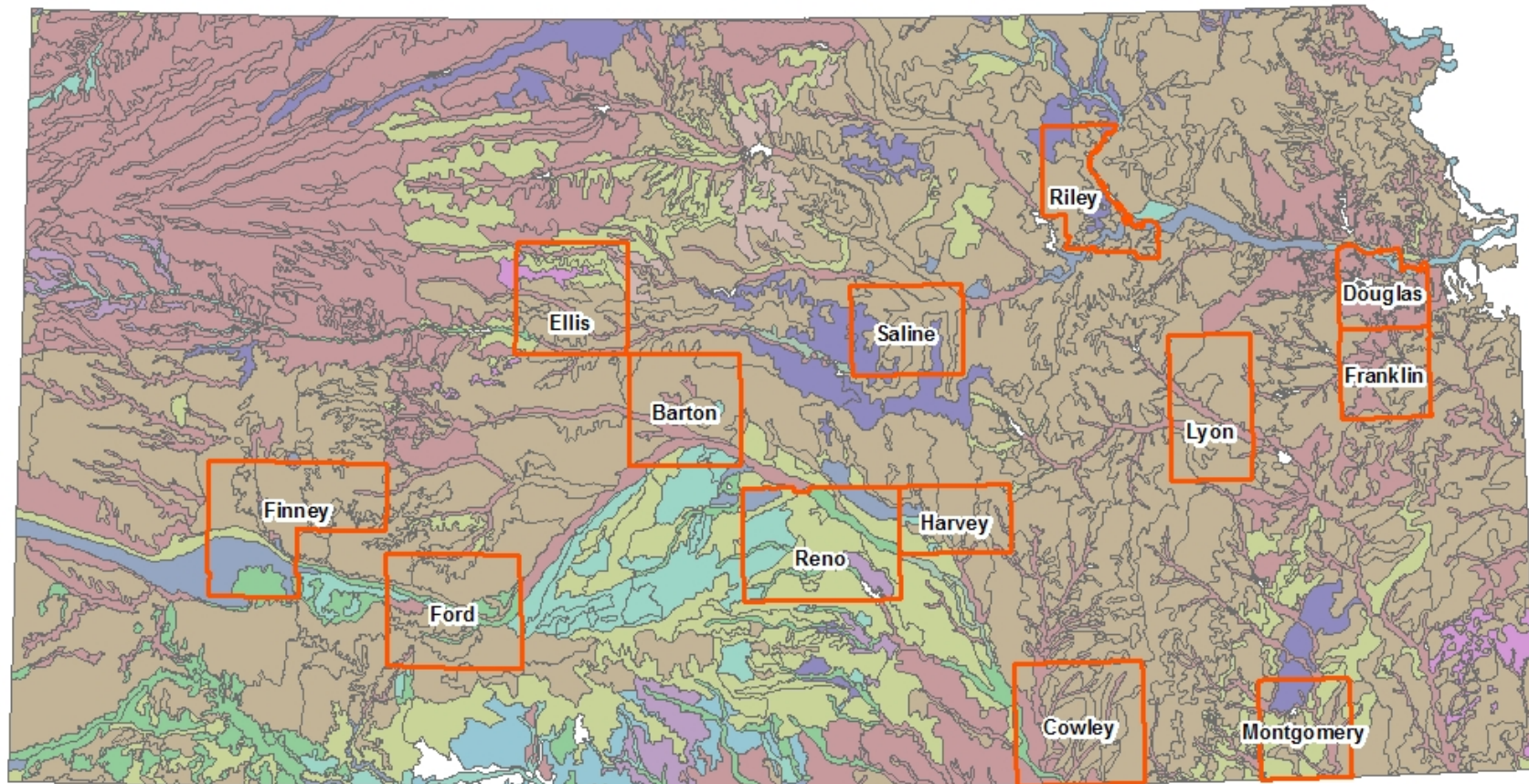
Winfield, Kansas



Winfield, Kansas







Soil Texture



0 40 80 Miles

1" = 40 Miles

Study County

clayey

coarse-loamy

coarse-silty

fine

fine-loamy

fine-loamy over sandy or sandy-skeletal

fine-silty

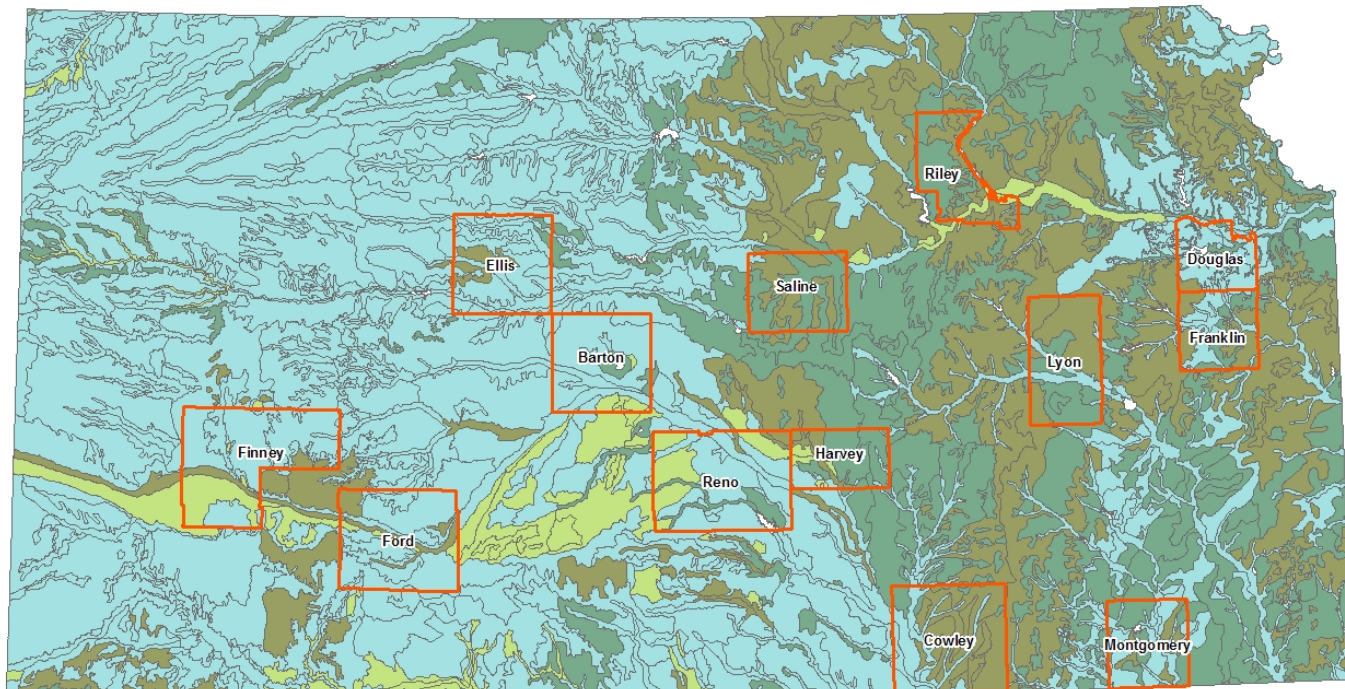
loamy

loamy-skeletal

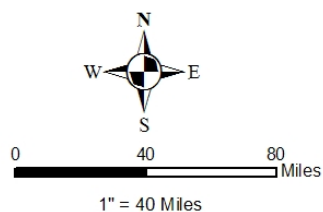
not used

sandy

very-fine



Soil Types



Hydrologic Group

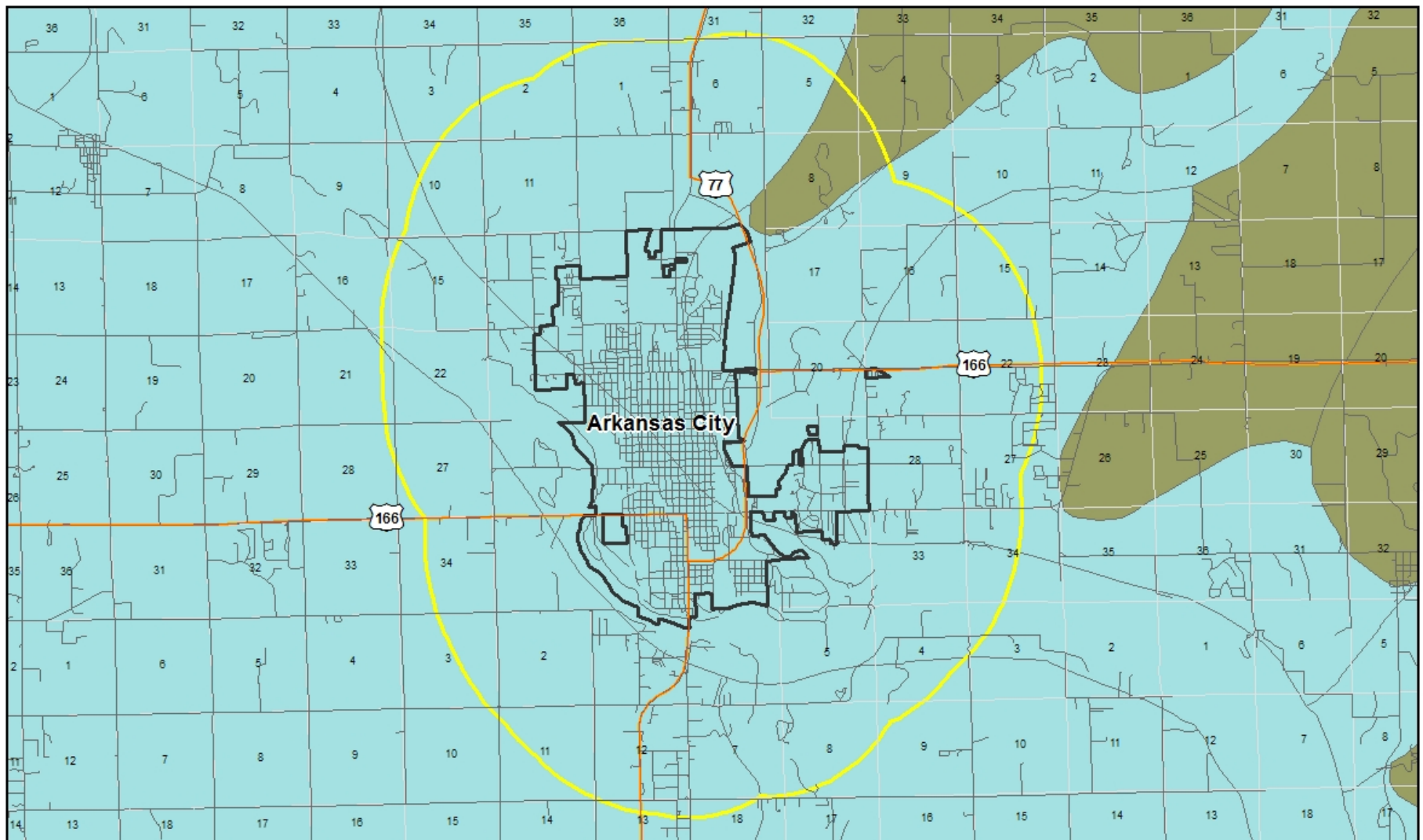


Study County

CDM

Soil Group	Description	Infiltration Rate (in hr^{-1})
A	Deep sands with very little silt and clay, also deep rapidly permeable loess	0.3-0.5
B	Mostly sand soils less deep than A, and loess less deep or less aggregated than A, but the group as a whole has high infiltration rate after wetting	0.16-0.3
C	Shallow soils and soils containing considerable clay and colloids, though less than those of group D. The group has a below-average infiltration after presaturation	0.04-0.16
D	Mostly clays of high swelling potential, but the group also includes some shallow soils with nearly impermeable subhorizons near the surface	0-0.04

Source: SCS (1972)



Soil Types Arkansas City

CDM

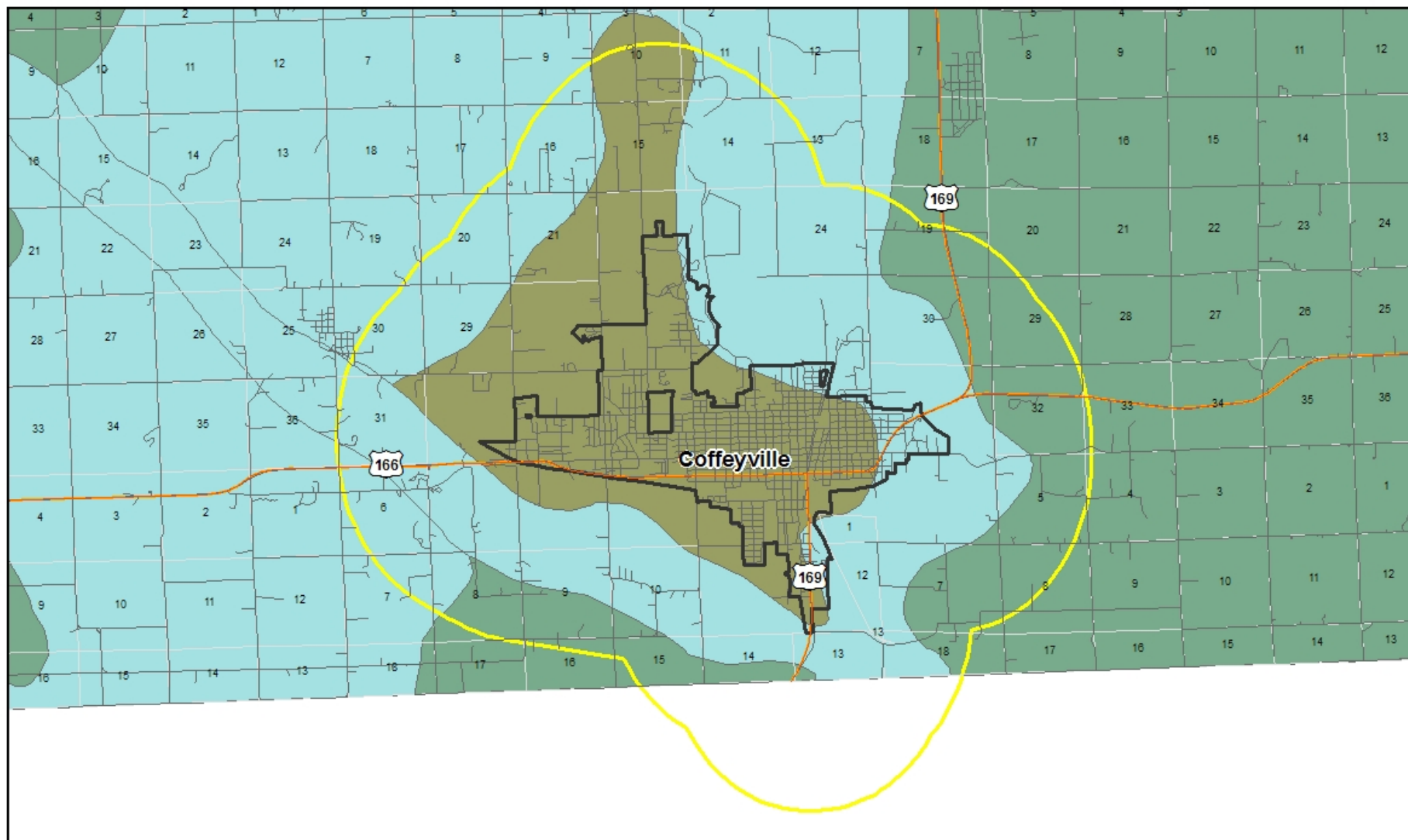


0 1 2 Miles

Hydrologic Group

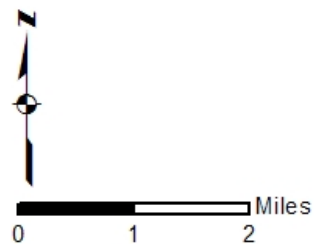


- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types Coffeyville

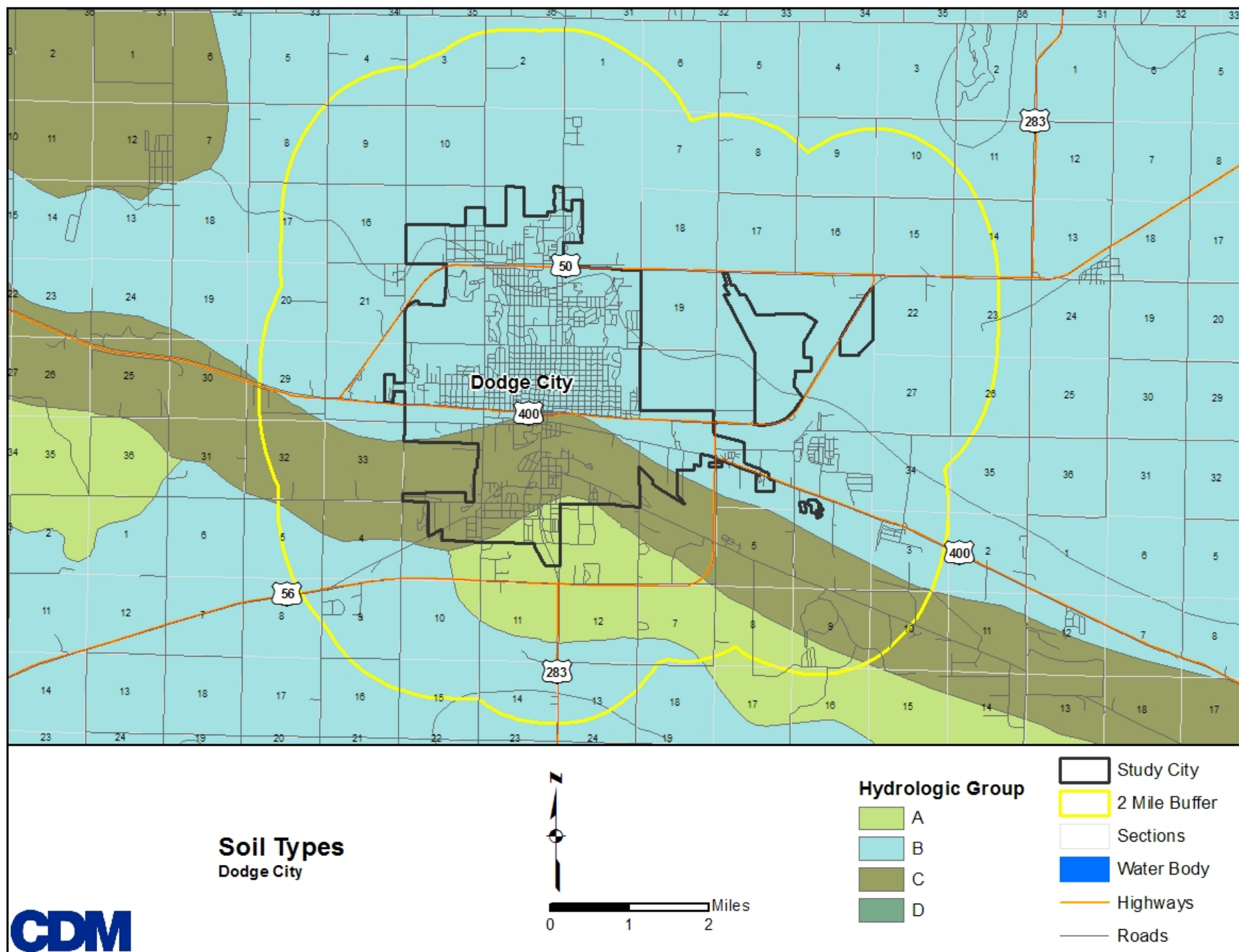
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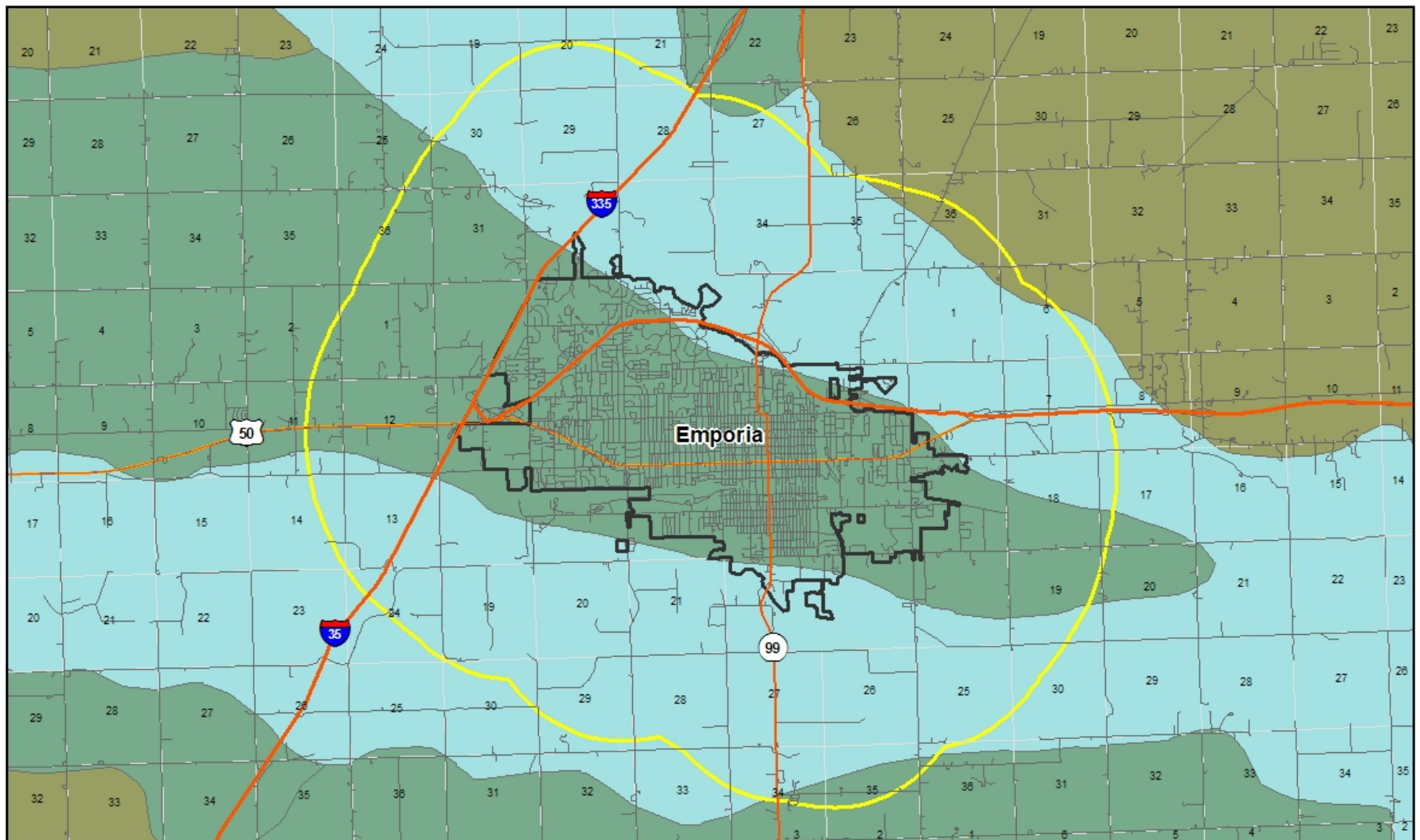


Hydrologic Group



- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads





Soil Types Emporia

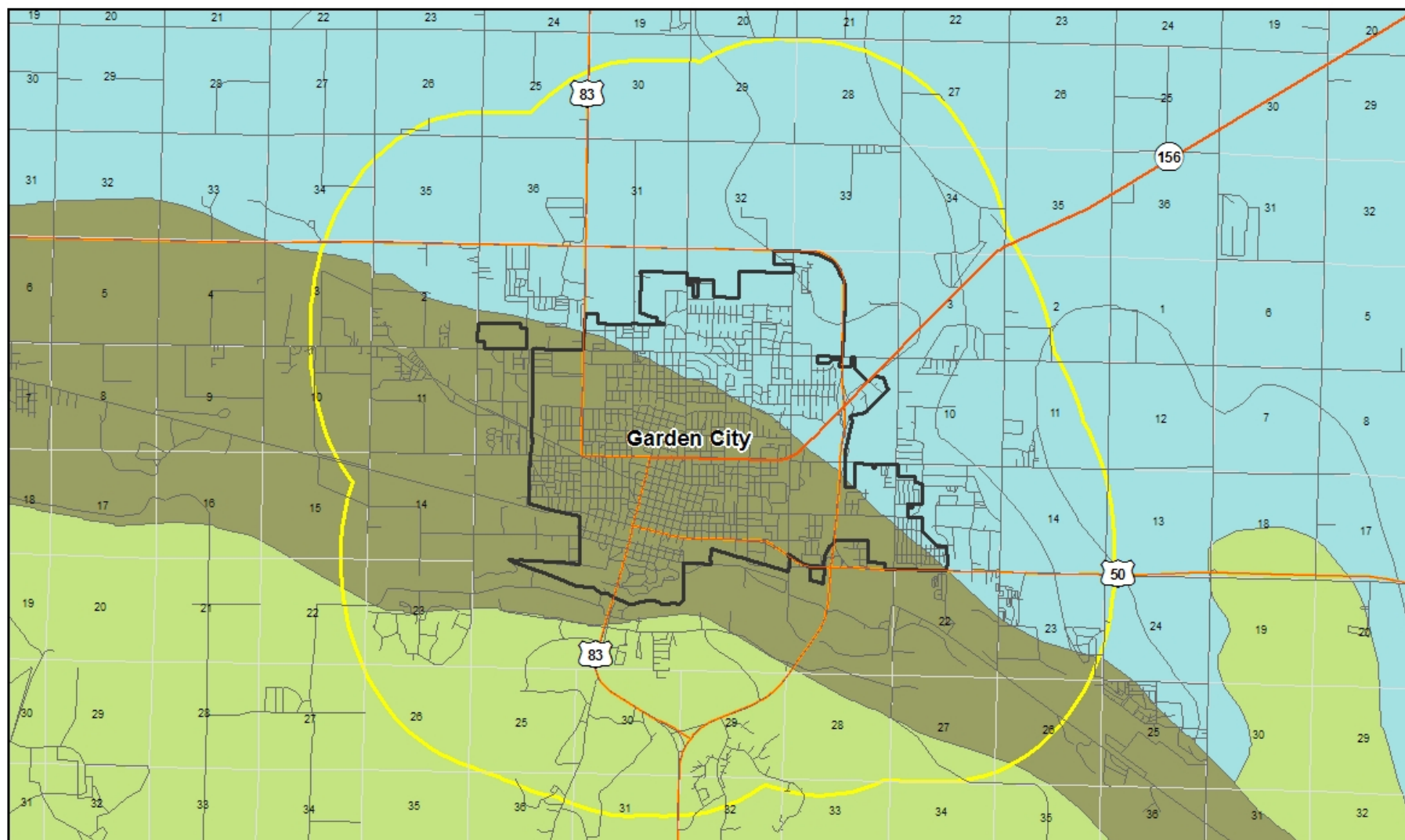


0 1 2 Miles

Hydrologic Group



- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types Garden City

CDM

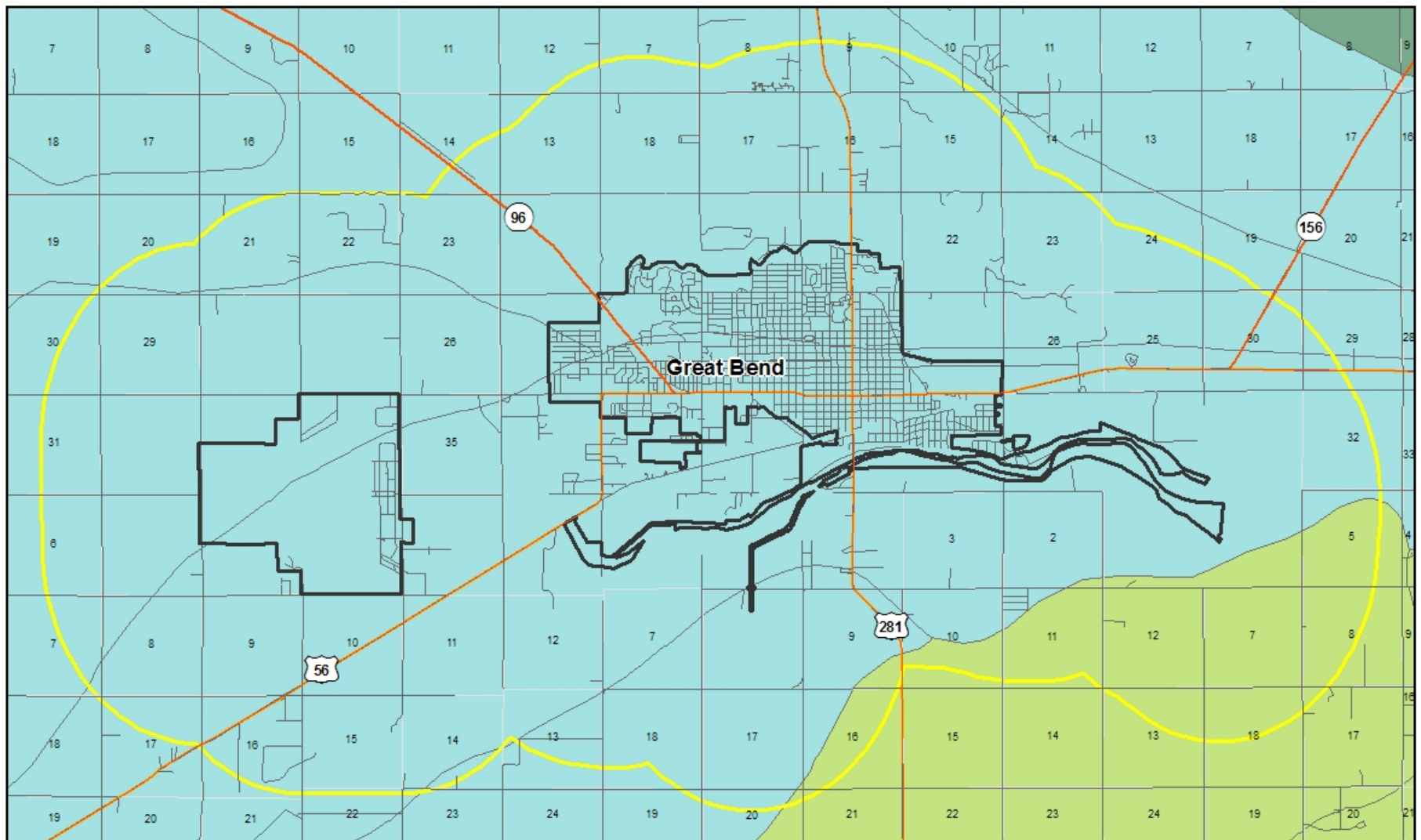


0 1 2 Miles

Hydrologic Group



- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types Great Bend

CDM

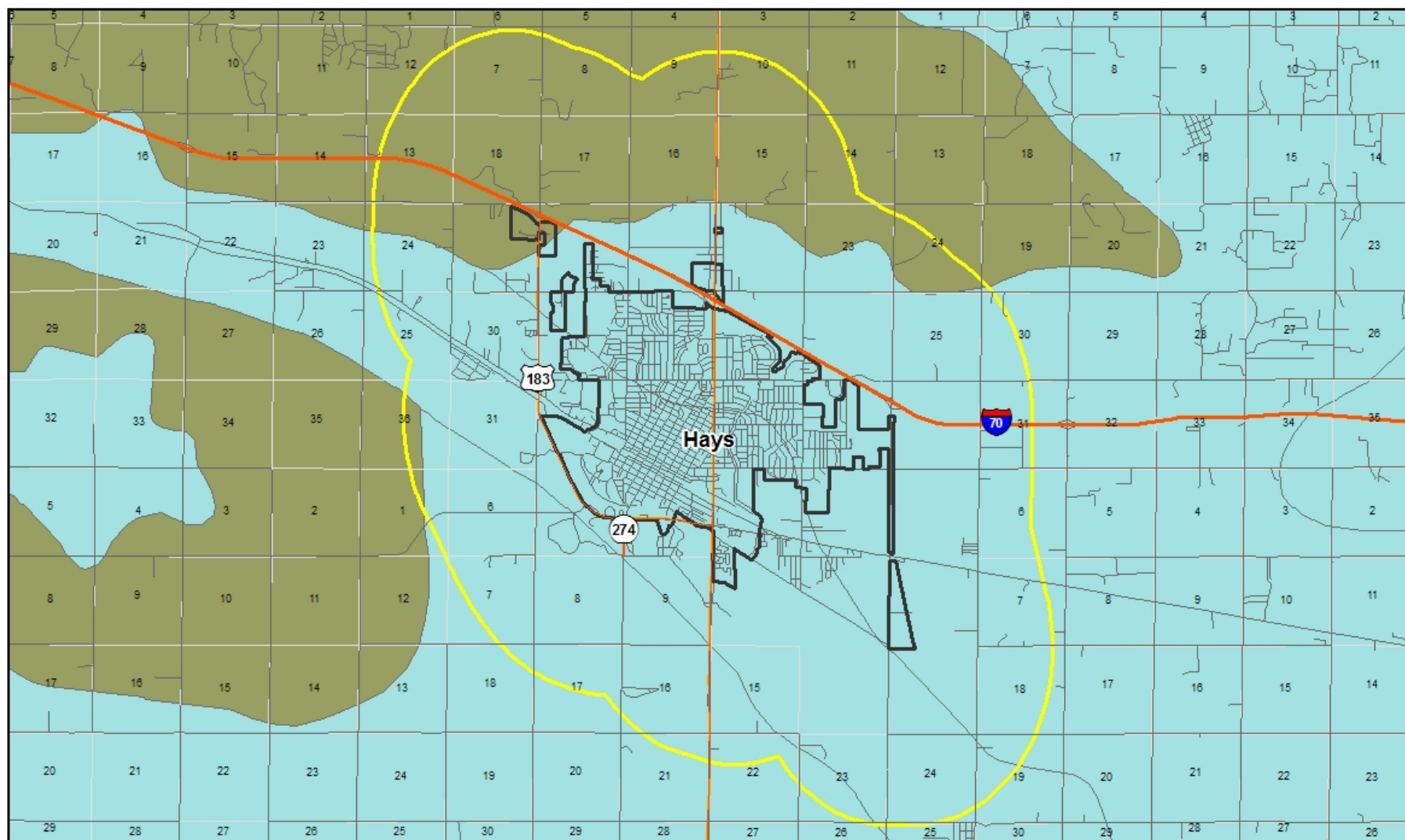


0 1 2 Miles

Hydrologic Group



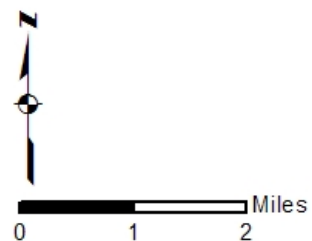
- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types

Hays

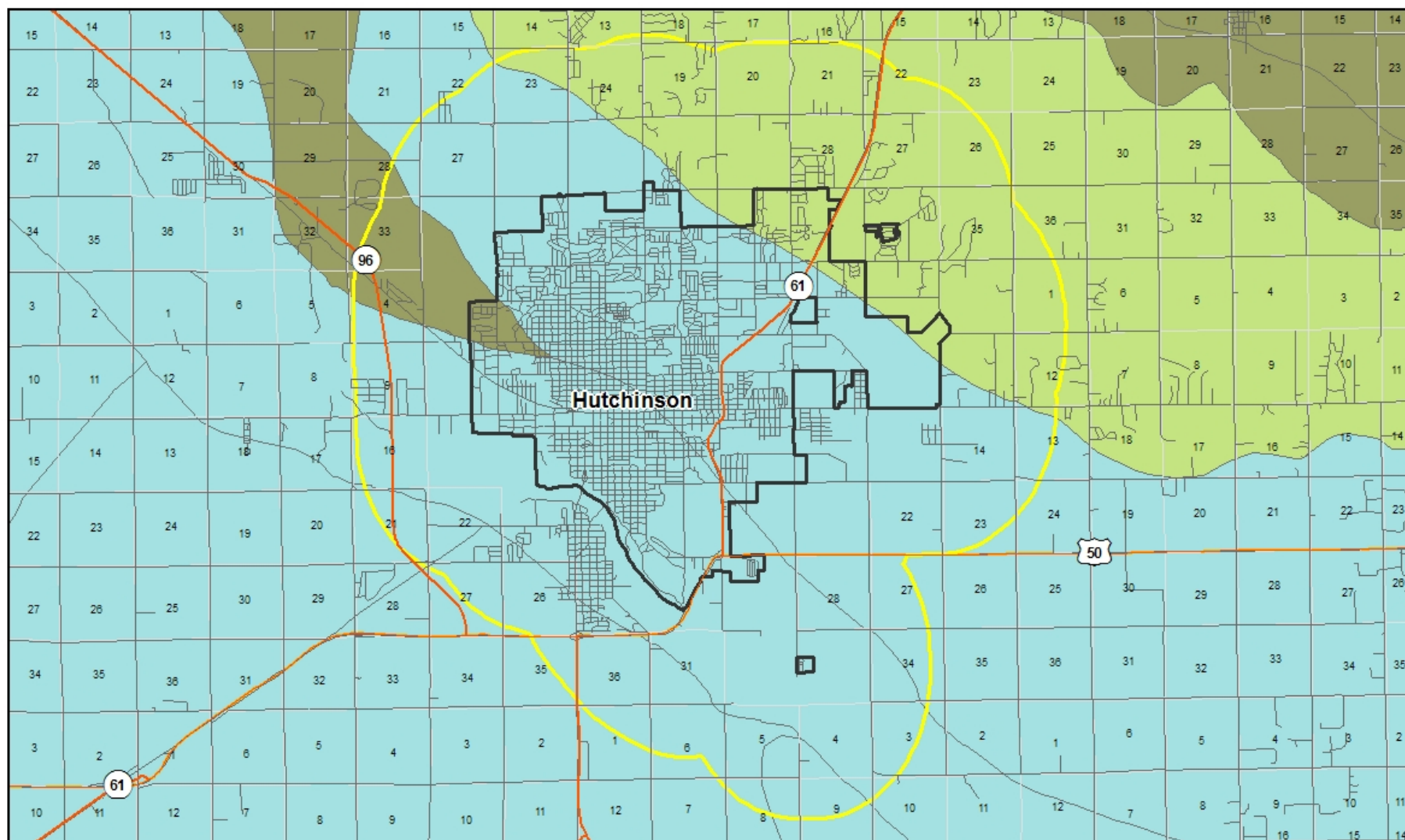
CDM



Hydrologic Group

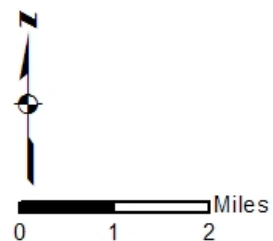


- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types Hutchinson

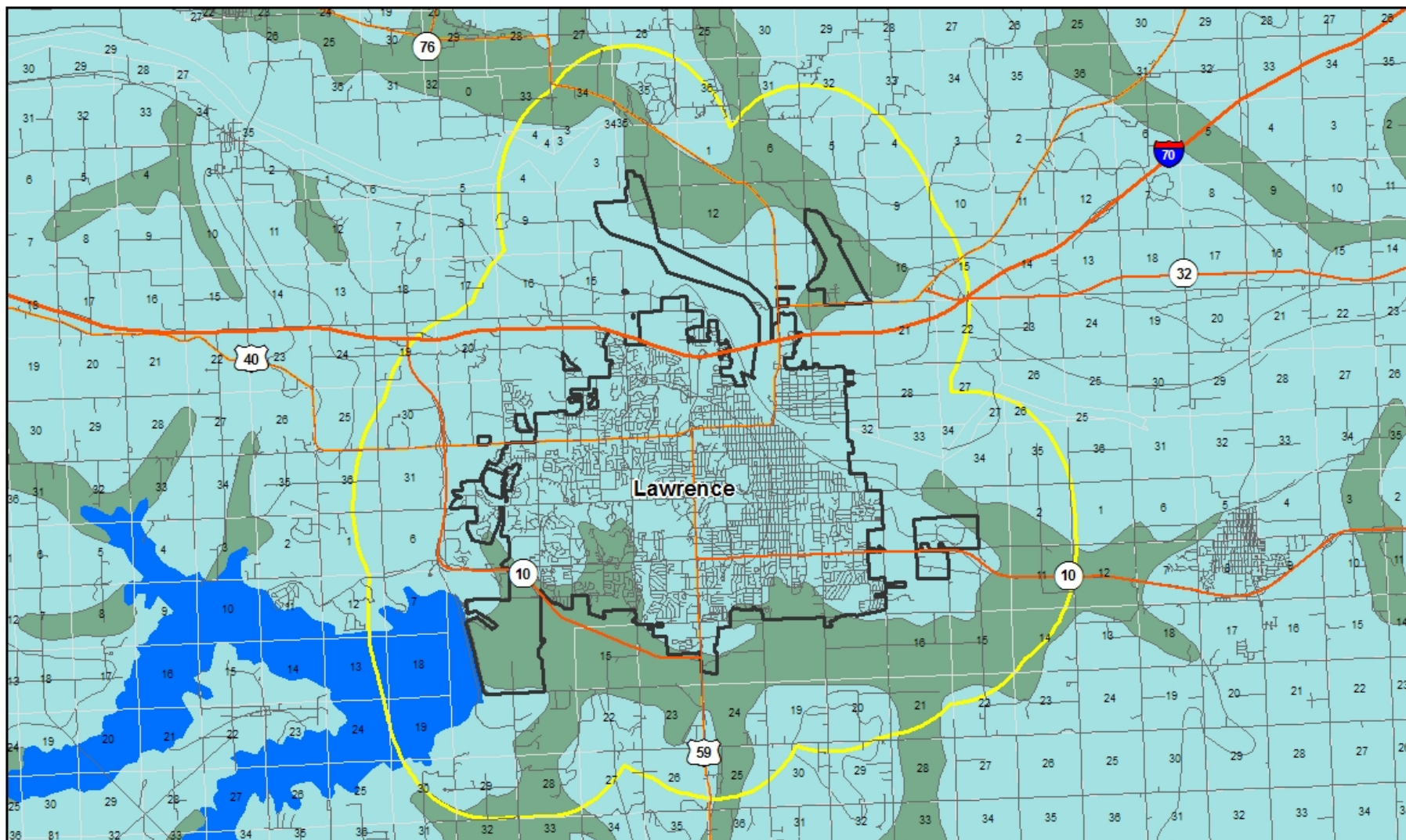
CDM



Hydrologic Group



-  Study City
-  2 Mile Buffer
-  Sections
-  Water Body
-  Highways
-  Roads



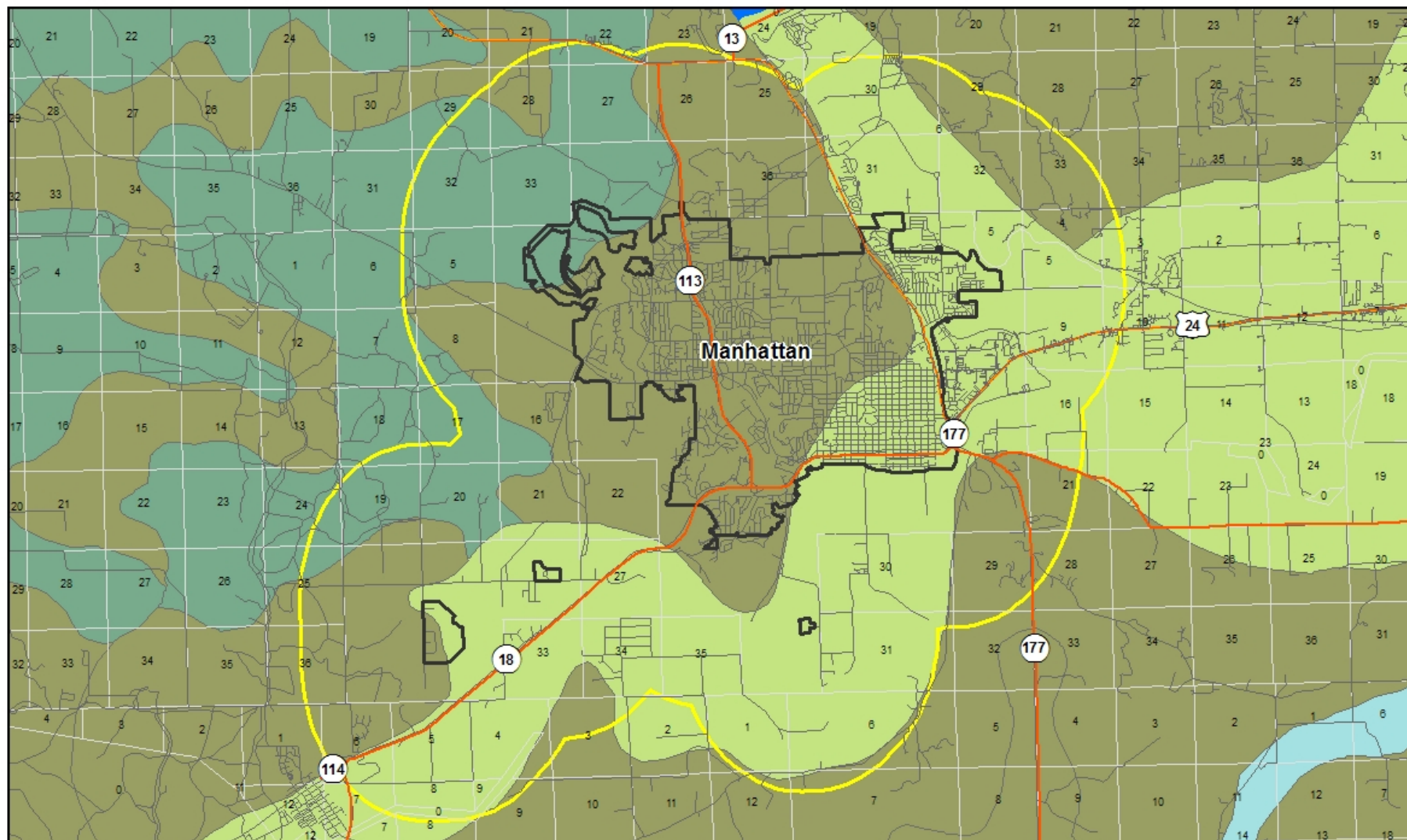
Soil Types Lawrence

CDM

Hydrologic Group

- A
- B
- C
- D

- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types Manhattan

CDM

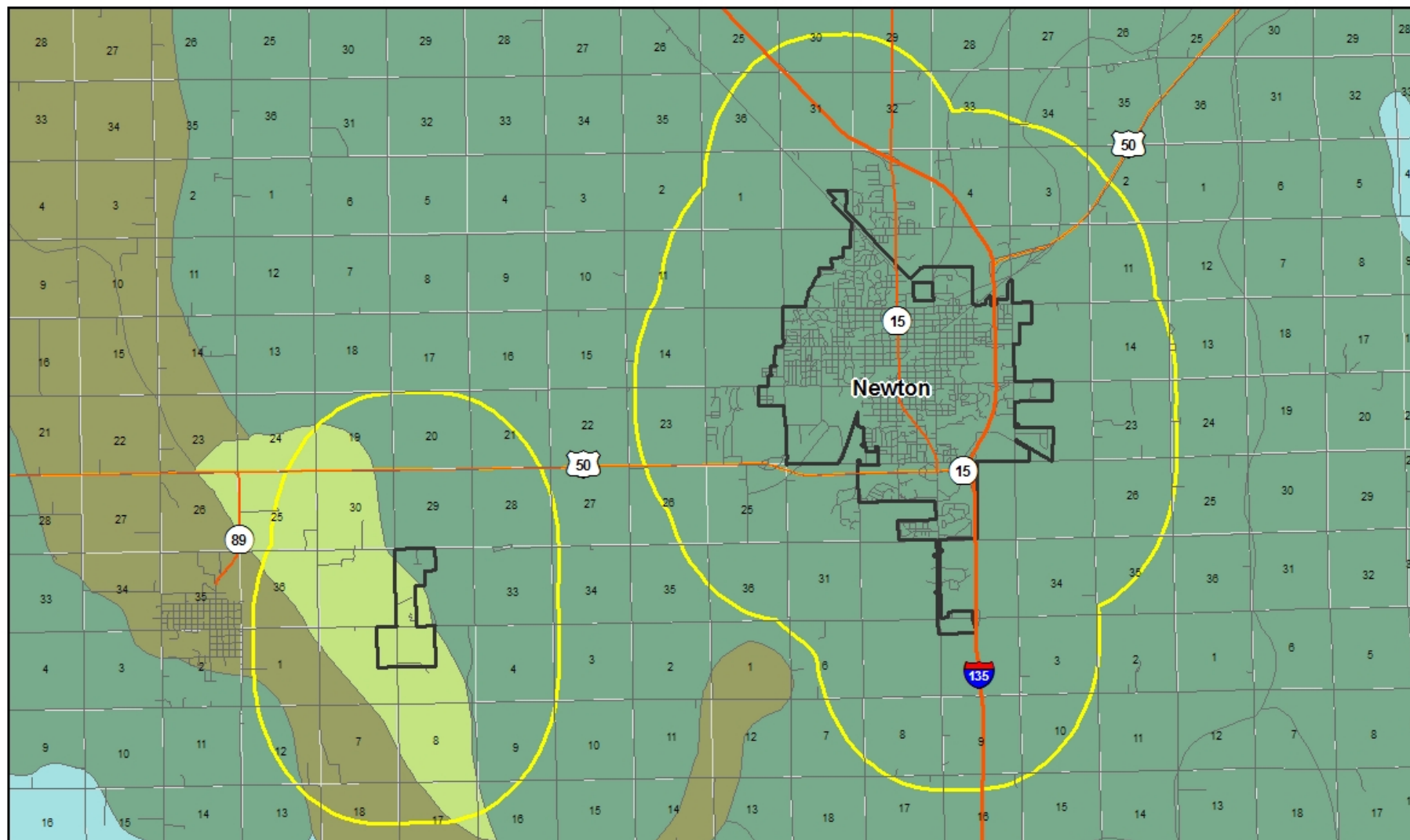


0 1 2 Miles

Hydrologic Group

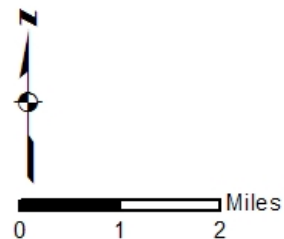


-  Study City
-  2 Mile Buffer
-  Sections
-  Water Body
-  Highways
-  Roads



Soil Types Newton

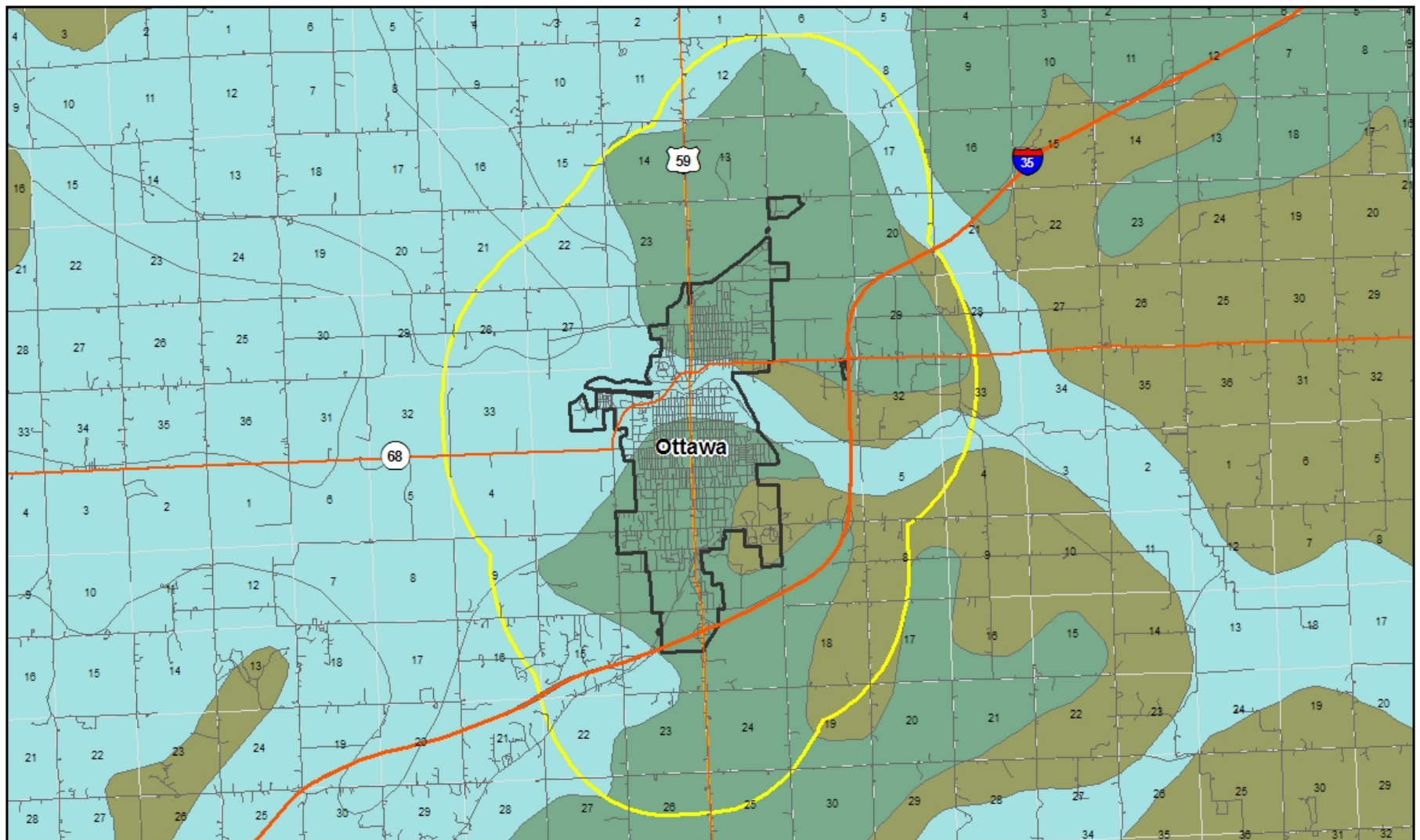
CDM



Hydrologic Group



- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types Ottawa

CDM

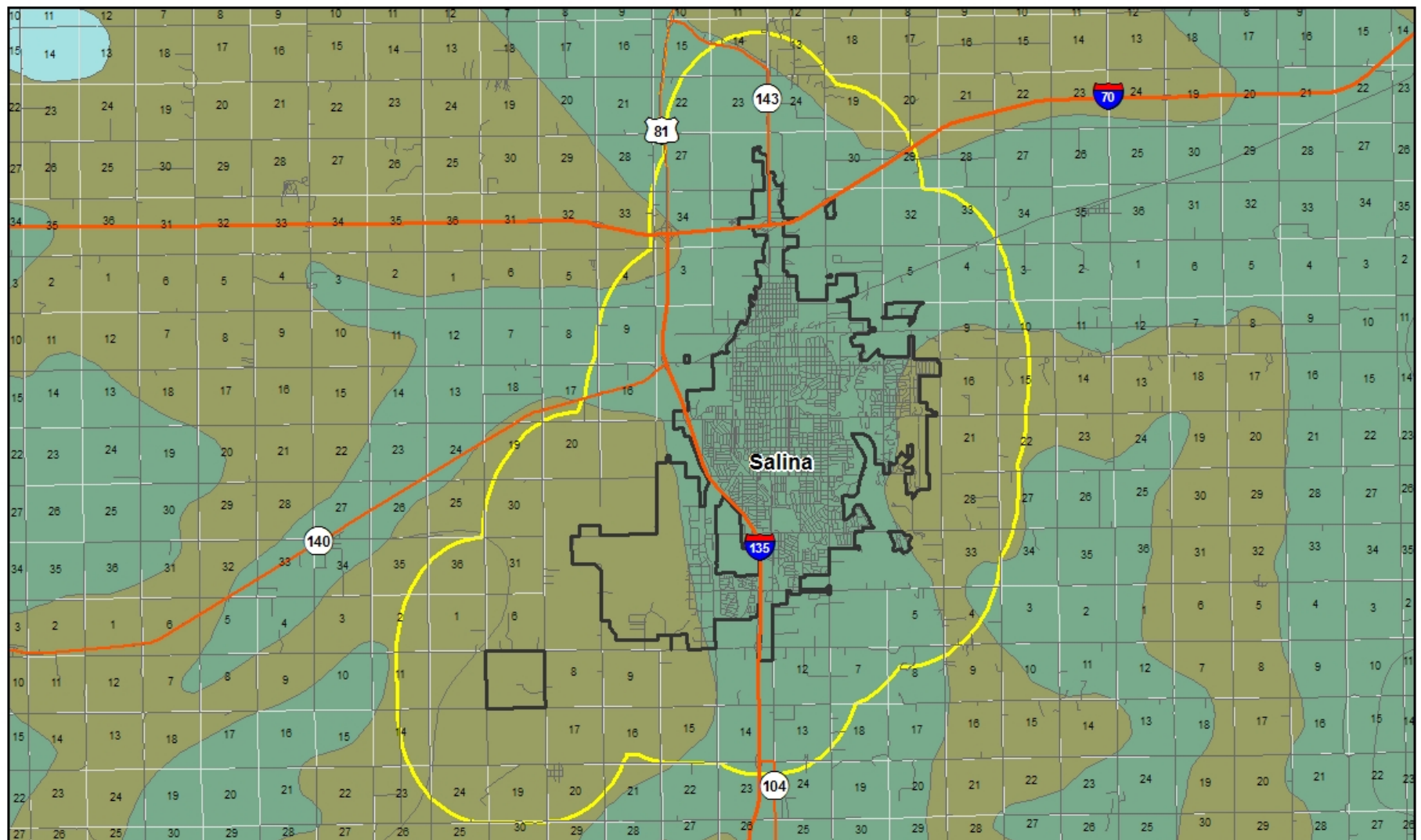


0 1 2 Miles

Hydrologic Group

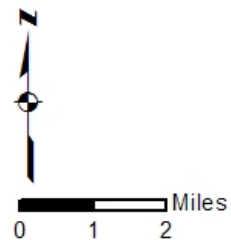
- A
- B
- C
- D

- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types Salina

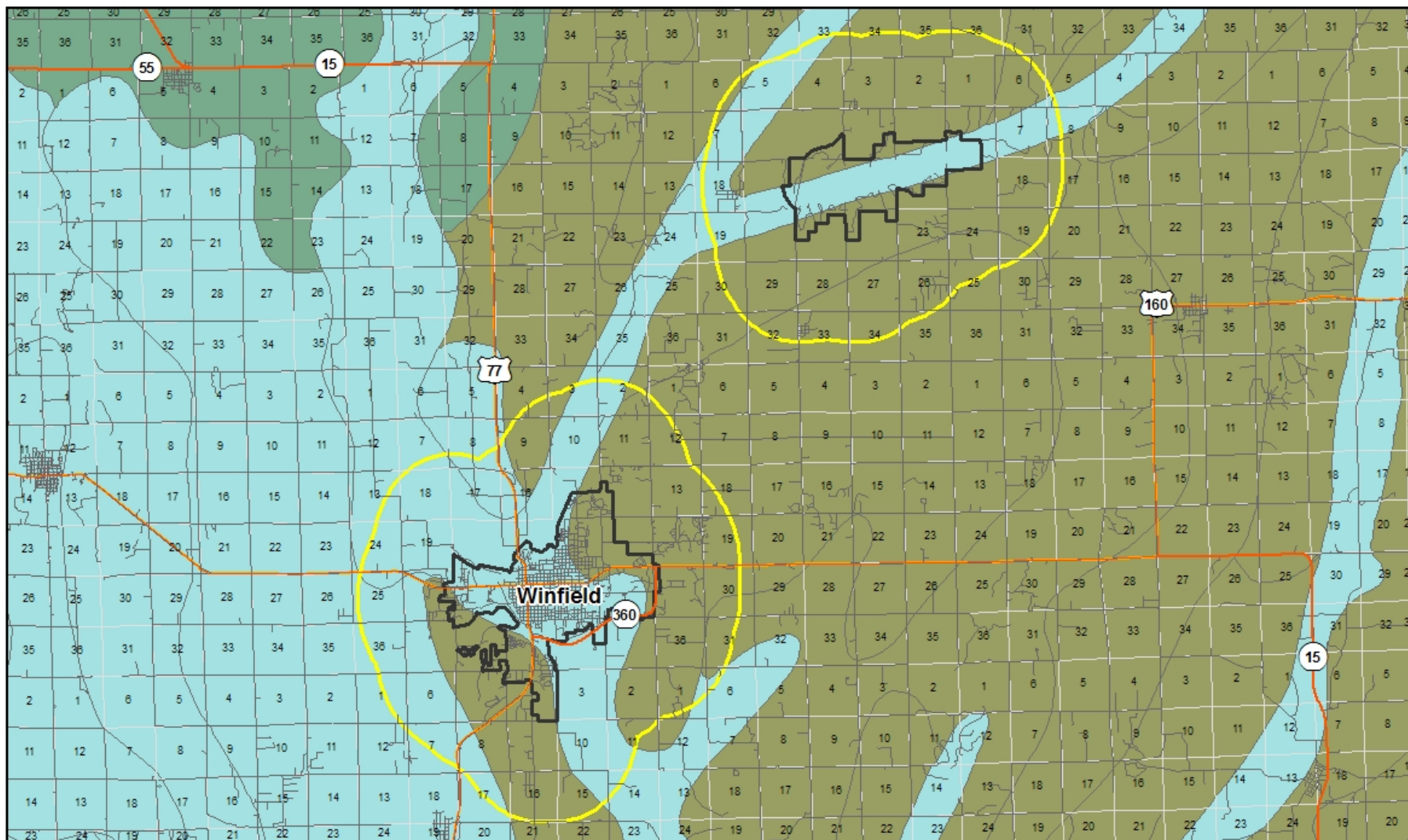
CDM



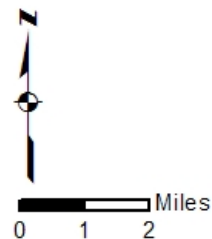
Hydrologic Group



- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads



Soil Types Winfield



Hydrologic Group



- Study City
- 2 Mile Buffer
- Sections
- Water Body
- Highways
- Roads

2. Before redistribution of the material removed under paragraph C and D of this section the regraded land shall be scarified to reduce potential slippage of the redistributed material and to promote root penetration. Such treatment may be conducted after the material is replaced if no harm will be caused to the redistributed material and reestablished vegetation.
 3. The Engineer may choose not to require the redistribution of topsoil or topsoil substitutes on the final embankments if it determines that--
 - a. Placement of topsoil or topsoil substitutes on such embankments will result in greater sedimentation than would otherwise occur, or
 - b. Such embankments will be stabilized by other approved means.
- G. Vegetation: Vegetation shall be established on all exposed surfaces. Plantings shall be as shown in the plans and as specified in Section 2314 – Best Management Practice Planting.

A1-3. BIORETENTION FACILITY:

- 1.1 Description: Bioretention facilities are small landscaped basins intended to provide water quality management by filtering stormwater runoff before release into stormdrain systems. This work shall consist of installing bioretention facilities as specified in the Contract Documents, including all materials, equipment, labor and services required to perform the work.
- 1.2 Materials:

Bioretention Soil Mixture. The Bioretention Soil Mixture (BSM) is a mixture of planting soil, mulch, and sand consisting of the following:

ITEM	COMPOSITION BY VOLUME	REFERENCE
Planting Soil	30%	See below.
Organic Compost	20%	See below.
Sand	50%	ASTM C33 Fine Aggregate

Planting Soil: The USDA textural classification of the Planting Soil for the BSM shall be LOAMY SAND OR SANDY LOAM. The Planting Soil shall be the best available on site material or furnished. Additionally, the Planting Soil shall be tested and meet the following criteria or as approved by the engineer:

ITEM	PERCENT BY WEIGHT	TEST METHOD
Sand (2.0 – 0.050 mm)	50 – 85%	AASHTO T88
Silt (0.050 – 0.002 mm)	0 – 50%	AASHTO T88
Clay (less than 0.002 mm)	2 – 5%	AASHTO T88
Organic Matter	3 – 10%	AASHTO T194

The textural analysis for the Planting Soil shall be as follows:

ASTM E11 SIEVE SIZE	MINIMUM PERCENT PASSING BY WEIGHT
2 in.	100
No. 4	90
No. 10	80

At least 45 days prior to the start of construction of bioretention facilities, the Contractor shall submit the source and testing results of the Planting Soil for the BSM to the Engineer for approval. No time extensions will be granted should the proposed Planting Soil fail to meet the minimum requirements stated above. Once a stockpile of the Planting Soil has been sampled, no material shall be added to the stockpile.

Organic Compost: Compost is a homogeneous and friable mixture of partially decomposed organic matter, with or without soil, resulting from composting, which is a managed process of bio-oxidation of a solid heterogeneous organic substrate including a thermophilic phase.

Compost is deemed acceptable if it meets 2 of the following requirements:

- *C/N ratio $\leq$ 25;*
- *Oxygen uptake rate $\leq$ 150 mg O₂/kg volatile solids per hour; and*
- *Compost must not contain more than 1 percent foreign matter. Foreign matter is defined as:*

“Any matter over a 2 mm dimension that results from human intervention and having organic or inorganic constituents such as metal, glass and synthetic polymers (e.g. plastic and rubber) that may be present in the compost but excluding mineral soils, woody material and rocks.”

Foreign matter less than 1 percent by weight must not exceed 12.5 mm in any dimension.

The Bioretention Soil Mixture (BSM) shall be a uniform mix, free of plant residue, stones, stumps, roots or other similar objects larger than two inches excluding mulch. No other materials or substances shall be mixed or dumped within the bioretention area that may be harmful to plant growth, or prove a hindrance to the planting or maintenance operations.

The Bioretention Soil Mixture shall be tested and meet the following criteria:

Item	Criteria	Test Method
Corrected pH	5.5 – 7.5	ASTM D4972
Magnesium	Minimum 32 ppm	*
Phosphorus (Phosphate - P ₂ O ₅)	not to exceed 60 ppm plant available phosphorus	*
Potassium (K ₂ O)	Minimum 78 ppm	*
Soluble Salts	Not to exceed 500 ppm	*

*

Use authorized soil test procedures.

Should the pH fall outside of the acceptable range, it may be modified with lime (to raise) or ammonium sulfate (to lower). The lime or ammonium sulfate must be mixed uniformly into the BSM prior to use in bioretention facilities.

Should the BSM not meet the minimum requirement for magnesium, it may be modified with magnesium sulfate. Likewise, should the BSM not meet the minimum requirement for potassium, it may be modified with potash. Magnesium sulfate and potash must be mixed uniformly into the BSM prior to use in bioretention facilities.

Planting soil and/or BSM that fails to meet the minimum requirements shall be replaced at the Contractor's expense. Mixing of the corrective additives to the BSM is incidental and shall be at the Contractor's expense.

Mixing of the BSM to a homogeneous consistency shall be done to the satisfaction of the Engineer. Upon approval of all requirements and testing above, the BSM shall be stockpiled, and no material shall be added to the BSM in the stockpile or during transport to the bioretention facility.

Other materials:

MATERIAL	SPECIFICATION
No. 57 Aggregate	ASTM D448
No. 7 Aggregate	ASTM D448
4-inch HDPE Plastic Pipe Underdrain	AASHTO M252
Geotextile Fabric	AASHTO M288
Mulch, 2x Shredded Hardwood Bark	See below
Water	See below.
Lime	ASTM C25
Ammonium Sulfate	See below.
Magnesium Sulfate	See below.
Potash	See below.

Shredded Hardwood Mulch: Shredded hardwood mulch shall be aged a minimum of 6 months and consist of the bark and wood (50/50) from hardwood trees which has been milled and screened to a maximum 4 in. particle size and provide a uniform texture free from sawdust, clay, soil, foreign materials, and any artificially introduced chemical compounds that would be detrimental to plant or animal life.

No. 7 and No. 57 Aggregate shall be double-washed to reduce suspended solids and potential for clogging. The aggregate shall be placed as shown in the Contract Drawings.

Water. Water used in the planting, establishing, or caring for vegetation shall be free from any substance that is injurious to plant life.

Lime. Lime shall contain not less than 85 percent calcium and magnesium carbonates. Dolomitic (magnesium) lime shall contain at least 10 percent magnesium as magnesium oxide and 85 percent calcium and magnesium carbonates.

Lime shall conform to the following gradation:

SIEVE SIZE	MINIMUM PERCENT PASSING BY WEIGHT
No. 10	100
No. 20	98
No. 100	50

Ammonium sulfate. Ammonium sulfate shall be a constituent of an approved horticultural product produced as a fertilizer for supplying nitrogen and as a soil acidifier.

Magnesium Sulfate. Magnesium sulfate shall be a constituent of an approved horticultural product produced as a fertilizer.

Potash. Potash (potassium oxide) shall be a constituent of an approved horticultural product produced as a fertilizer.

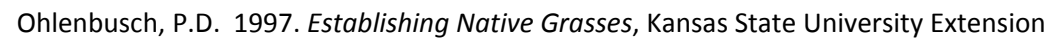
- 1.3 Construction: Bioretention facilities shall not be constructed until all contributing drainage areas are permanently stabilized against erosion and sedimentation as shown on the Contract Plans and to the satisfaction of the Engineer. Any discharge of sediment that affects the performance of the cell will require reconstruction of the cell to restore its defined performance. No heavy equipment shall operate within the perimeter of a bioretention facility during underdrain placement, backfilling, planting, or mulching of the facility.

Excavation. If the bioretention facility is to be used as a sediment basin the bioretention facility shall be excavated to the dimensions, side slopes, and **1 foot above** the bottom of the Bioretention Soil Mixture elevations shown on the Contract Plans. Any sediment from construction operations deposited in the bioretention facility shall be completely removed from the facility after all vegetation, including landscaping within the drainage area of the bioretention facility, has been established. The excavation limits shall then be final graded to the dimensions, side slopes, and **final** elevations shown on the Contract Plans. Excavators and backhoes, operating on the ground adjacent to the bioretention facility, shall be used to excavate the facility if possible. low ground-contact pressure equipment or, if approved by the engineer, by excavators and/or backhoes operating on the ground adjacent to the bioretention facility. Low ground-contact pressure equipment is preferred on bioretention facilities to minimize disturbance to established areas around perimeter of cell. No heavy equipment shall be used within the perimeter of the bioretention facility before, during, or after the placement of the BSM.

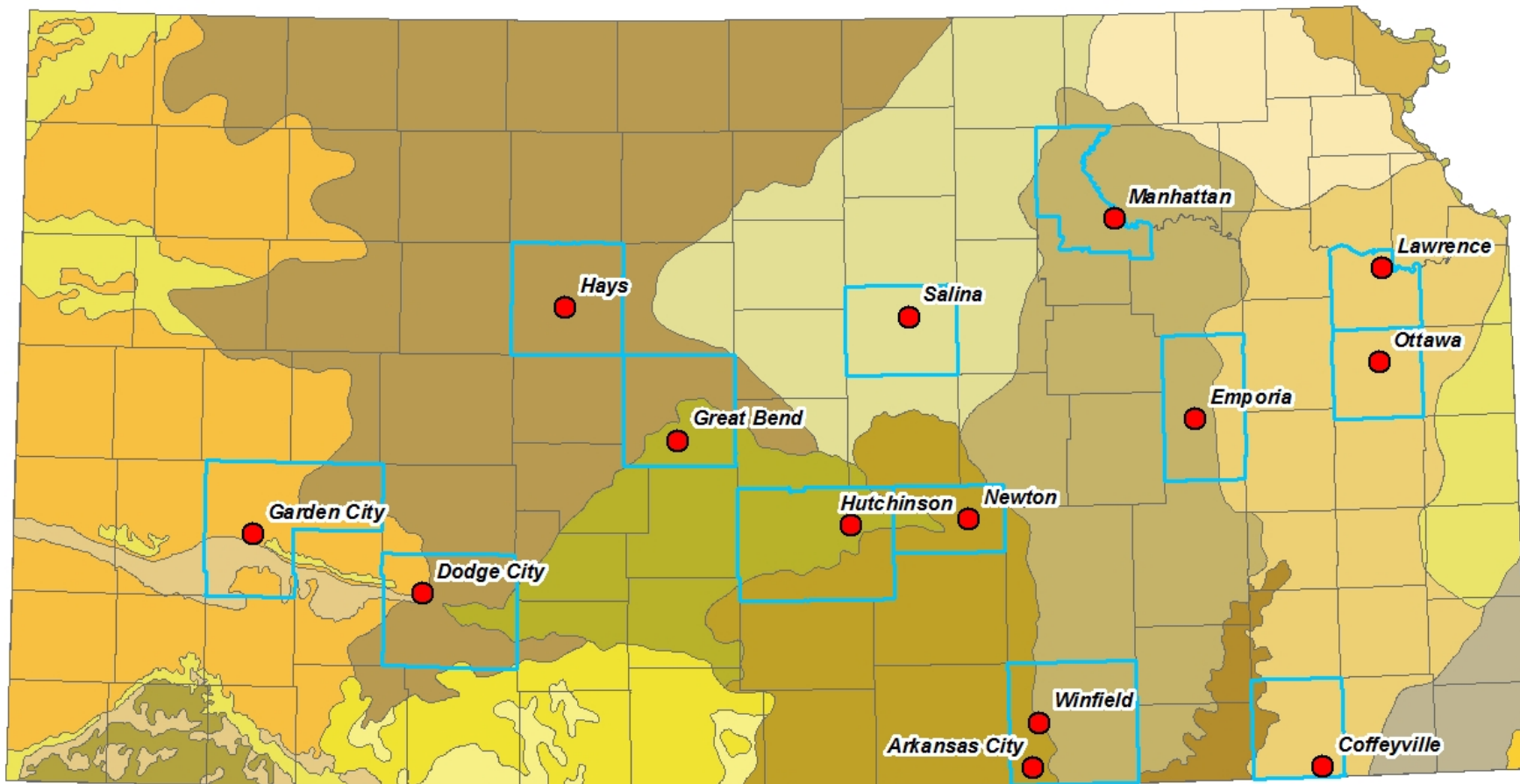
Excavated materials shall be removed from the bioretention facility site. Excavated materials shall be used or disposed of in conformance with the project specifications.

After placing the underdrain and aggregate and before the BSM, the bottom of the excavation shall be roto-tilled to a minimum depth of 6 inches to alleviate any compaction of the facility bottom. Any substitute method for roto-tilling must be approved by the Engineer prior to use. Any ponded water shall be removed from the bottom of the facility and the soil shall be friable





Zone	Optimum	Acceptable
1	March 25–April 10	Feb. 15–May 1
2	April 1–April 20	March 1–May 15
3	April 10–April 30	March 1–May 15



CDM

Eco-Regions



0 40 80 Miles

1" = 40 Miles

- | | | | |
|--|--|--|---|
| ● City | Study County | Flint Hills | Rolling Cropland and Range |
| County | Cherokee Plains | Great Bend Sand Prairie | Rolling Plains and Breaks |
| Cimarron Breaks | Missouri Alluvial Plain | Loess and Glacial Drift Hills | Rolling Sand Plains |
| Cross Timbers | Moderate Relief Rangeland | Nebraska/Kansas Loess Hills | Smoky Hills |
| Flat Tablelands and Valleys | Osage Cuestas | Wellington-McPherson Lowland | Springfield Plateau |
| Flat to Rolling Cropland | Rainwater Basin Plains | Wooded Osage Plains | |

Eco-Region	Typical Vegetation
Cherokee Plains	Tallgrass prairie and oak hickory woodland in areas of greater relief. Upland areas dominated by hardpan and claypan prairie with little bluestem, side oats grama, varying amounts of big bluestem and Indiangrass, and a variety of forbs.
Cimarron Breaks	Mixedgrass prairie, dominated by big bluestem (on more mesic sites), little bluestem, side oats grama, blue grama, and some hairy grama, with eastern red cedar a dominant tree, especially in sites sheltered from fire.
Cross Timbers	Cross timbers savanna: post oak, blackjack oak, hickory, and eastern red cedar with an understory of tallgrass and mixedgrass species.
Flat Tablelands and Valleys	Sandsage prairie common in sites with sandy or well-drained soils. Floodplain woodlands dominated by plains cottonwood, black willow, and peach leaf willow. Common hackberry, green ash, and American elm locally common, especially in the eastern part of the region.
Flat to Rolling Cropland	Mixedgrass prairie in the north: needle and thread, blue grama, threadleaf sedge, prairie sandreed, and western wheatgrass. Shortgrass prairie to the south: blue grama, buffalograss, and scattered, isolated sites with alkali sacaton, western wheatgrass, and inland saltgrass.
Flint Hills	Tallgrass prairie: big bluestem, little bluestem, switchgrass, and Indiangrass. Largest area of intact, native, tallgrass prairie in the Great Plains.
Great Bend Sand Prairie	Sand prairie bunch grasses: sand bluestem, sand dropseed, and sand reedgrass.
Loess and Glacial Drift Hills	Tallgrass prairie with cottonwood dominated forests along floodplains and oak hickory forests on bluffs.
Missouri Alluvial Plain	Northern floodplain forest: cottonwood, green ash, boxelder, and elm, with lowland tallgrass prairie: big bluestem, prairie cordgrass, switchgrass, and sedges.
Moderate Relief Rangeland	Combination of shortgrass and mixedgrass prairies, with mostly mixedgrass prairie in the north. Shortgrass prairie (blue grama and buffalograss) dominates on upland sites, giving way to mixedgrass prairie (little bluestem, side oats grama) on slopes, more mesic sites along rivers and streams, and also on sites overlain by thicker loess deposits. In the south, largely on Cretaceous chalks, a unique association called the chalk flat prairie, which is a mixedgrass prairie.

Eco-Region	Typical Vegetation
Nebraska/Kansas Loess Hills	Tallgrass prairie: big bluestem, Indiangrass, switchgrass, and little bluestem. Scattered oak hickory forests and some floodplain woodlands along rivers and streams: bur oak, basswood, black walnut, green ash, plains cottonwoods, and willows.
Osage Cuestas	Transitional: mostly tallgrass prairie in the west to a combination of tallgrass prairie and oak hickory woodland in the east. Upland forests dominated by shagbark hickory, bitternut hickory, red oak, white oak, and black oak, with Ohio buckeye, American bladderpod, and pawpaw common understory trees.
Rainwater Basin Plains	Tallgrass prairie: big bluestem, little bluestem, and Indiangrass, with switchgrass in more mesic sites. Floodplain forests are well developed along rivers and streams and are dominated by plains cottonwood, black willow, peach leaf willow, common hackberry, American elm, green ash, and black walnut, with bur oak becoming less abundant westward.
Rolling Cropland and Range	Shortgrass prairie in loess mantled areas with sandsage prairie in areas with coarse textured soils.
Rolling Plains and Breaks	Mixedgrass prairie: big bluestem, little bluestem, blue grama, needle and thread, side oats grama, and western wheatgrass. Some areas of floodplain forests along major riparian corridors.
Rolling Sand Plains	Sandsage prairie: sand sagebrush, sand bluestem, prairie sandreed, and little bluestem. This community type sometimes is called sandsage steppe due to the presence of a dominant shrub, however, sandsage prairie is the name most frequently used in the plains.
Smoky Hills	Transitional from tallgrass prairie in the east to mixedgrass prairie in the west. Some floodplain forests along riparian areas.
Springfield Plateau	Tallgrass prairie species, Oak hickory mixed forest along rivers and streams, with flowering Dogwood on uplands.
Wellington-McPherson Lowland	Tallgrass prairie: big bluestem, little bluestem, and Indiangrass, with switchgrass in more mesic sites. Floodplain forests are well developed along rivers and streams and are dominated by plains cottonwood, black willow, peach leaf willow, common hackberry, American elm, green ash, and black walnut, with bur oak becoming less abundant westward.
Wooded Osage Plains	Mixture of oak hickory woodland and tallgrass prairie with a greater concentration of hardwood forest. Much like 40b, but Shumard oak, pecan, pin oak, and persimmon a bit more common, especially along the Marais des Cygnes River.

Native Vegetation Resources	
Documents	
K-State Extension Fact Sheet MF-2291	www.oznet.ksu.edu/library/crpsl2/MF2291.pdf
Managing Kansas Grazing lands for Water Quality MF-2086	www.oznet.ksu.edu/library/crpsl2/mf2086.pdf
Websites	
Kansas Native Plant Society	www.kansasnativeplantsociety.org
Tallgrass Prairie Center	www.tallgrassprairiecenter.org/
Kansas Wildflowers and Grasses	www.kswildflower.org
Natural Resources Conservation Service (NRCS)	www.nrcs.org
Grown Native	www.grownative.org
Nurseries	
Sharp Brothers Seed Company (Healy, KS)	www.sharpseed.com
Hamilton Seed (Elk Creek, MO)	www.hamiltonseed.com
Junilee Native (Gardner, KS)	www.jubileenative.com
Feyh Farm Company (Alma, KS)	www.feyhfarmseed.com
Star Seed (Beloit, KS)	www.gostarseed.com/
Outside Pride	www.outsidepride.com/resources/states/kansas.html



Short Term Vegetated BMP Maintenance	
Prior to and During Installation and Establishment of BMP	
Task	Explanation
Encourage phased construction of development surrounding BMP	Utilize staged construction to limit erosion potential of land exposed
Provide temporary stormwater control	Stormwater runoff shall be routed around facility until vegetation is established (generally 2-3 months)
Provide site stabilization	Utilize erosion control during construction and until facility is established
Protection from foot traffic and BMP education through signage	Use fencing and signage to prevent damage from animal and human foot traffic and to initiate public interest and education
Planting of native vegetation	Optimum planting window depends on location in KS; for seeding rates and other assistance contact local NRCS
Mulching	Use mulch made from native hay or native plants to reduce potential competition for resources
Fertilization	Typically with native vegetation fertilization is not required, however consult local NRCS for fertilizing suggestions after soils test
Irrigation/Watering	Watering schedule must be established for upkeep of vegetation
During 3 Months Post-Installation	
Post wet-weather event (Precipitation > 0.5")	Ensure that vegetation and other erosion stabilizing mechanisms are intact and check inlet/outlet structures and surrounding area for signs of erosion or instability
Protection from foot traffic and BMP education through signage	Use fencing and signage to prevent damage from animal and human foot traffic and to encourage BMP education and interest
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Irrigation/Watering	Watering schedule must be established for upkeep of vegetation
Weeding	Particularly important during initial growth to reduce competition for moisture, nutrients, and sunlight
Replacement of dead plants	All dead plants should be removed, the cause of their death investigated, and if the cause is the BMP environment, attempt growth of new plant type
Establish "Green Teams" or other community groups	Encourage community involvement and establish maintenance crews to perform routine clean out of trash and debris and to maintain appearance of BMP

Long Term Vegetated BMP Maintenance

End of Growing Season (August - September)

Task	Explanation
General Inspection	Check for standing water, slope stability, sediment accumulation, trash and debris, presence of burrows and erosion, and integrity of inlet/outlet, dam, and other engineered structures
Clean out sediments and debris	Clean out sediments and debris from inlet, outlet, the BMP and for detention basins, remove sediment when accumulation reduces the permanent pool by 10% or the forebay by 50% and dispose of appropriately
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Mowing/Harvest	Native grasses should be trimmed to 4-6" to provide adequate biomass for regrowth the following year
Maintain BMP Signage	Repairs should be made to signage, walkways, picnic tables, or any other public recreation equipment as necessary
Winter stabilization	May be necessary to establish erosion prevention practices to maintain BMP over the winter when plants are dormant
Continue to support and educate "Green Teams" or other community groups	It is important to maintain community involvement and provide education and opportunities for service

Beginning of Growing Season (March-April)

General Inspection	Check for standing water, slope stability, sediment accumulation, trash and debris, presence of burrows and erosion, and integrity of inlet/outlet, dam, and other engineered structures
Clean out sediments and debris	Clean out sediments and debris from inlet, outlet, the BMP and for detention basins, remove sediment when accumulation reduces the permanent pool by 10% or the forebay by 50% and dispose of appropriately
Provide site stabilization	Ensure that vegetation and other erosion stabilizing mechanisms are intact
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Weeding/Pruning	Remove invasive and excess biomass and dispose of appropriately.
Replace/augment vegetation	Augment existing plants by same planting procedure as during construction if necessary and dead plants should be removed and replaced
Continue to support and educate "Green Teams" or other community groups	It is important to maintain community involvement and provide education and opportunities for service

Short Term Non-Vegetated BMP Maintenance

Prior to and During Installation of BMP

Task	Explanation
Encourage phased construction of development surrounding BMP	Utilize staged construction to limit erosion potential of land exposed
Provide site stabilization	Utilize erosion control during construction and until facility is established
Encourage infiltration through BMP bottom into surrounding soil	Roto-till the bottom soil to increase potential for deep percolation
Protection from foot traffic and BMP education through signage	Use fencing and signage to prevent damage from animal and human foot traffic and to initiate public interest and education

During 3 Months Post-Installation

Post wet-weather event (Precipitation > 0.5")	Ensure erosion stabilizing mechanisms are intact and check inlet/outlet structures and surrounding area for signs of erosion or instability
Prevent surface clogging	Remove surface debris (grass clippings, sediment, etc.) and monitor ponding
Monitor internal clogging	Check levels of well to ensure proper infiltration from BMP to surrounding soil
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Protection from foot traffic and BMP education through signage	Use fencing and signage to prevent damage from animal and human foot traffic and to encourage BMP education and interest
Establish "Green Teams" or other community groups	Encourage community involvement and establish maintenance crews to perform routine clean out of trash and debris and to maintain appearance of BMP

Long Term Non-Vegetated BMP Maintenance

End of Growing Season (August - September)

Task	Explanation
General Inspection	Check for standing water, slope stability, sediment accumulation, trash and debris, presence of burrows and erosion, and integrity of inlet/outlet, dam, and other engineered structures
Clean out sediments and debris	Clean out sediments and debris from surface and check for signs of ponding or clogging
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint
Maintain BMP Signage	Repairs should be made to signage, walkways, picnic tables, or any other public recreation equipment as necessary
Winter stabilization	May be necessary to establish erosion prevention practices to maintain BMP when soils become frozen and surface materials may freeze
Continue to support and educate "Green Teams" or other community groups	It is important to maintain community involvement and provide education and opportunities for service

Beginning of Growing Season (March-April)

General Inspection	Check for standing water, slope stability, sediment accumulation, trash and debris, presence of burrows and erosion, and integrity of inlet/outlet, dam, and other engineered structures
Prevent surface clogging	Remove surface debris (grass clippings, sediment, etc.) and monitor ponding
Monitor internal clogging	Check levels of well to ensure proper infiltration from BMP to surrounding soil
Clean out sediments and debris	Clean out sediments and debris from surface and check for signs of ponding or clogging
Provide site stabilization	Ensure that BMP media and other erosion stabilizing mechanisms are intact
Maintain aesthetics	General clean up of the BMP and surrounding areas to maintain aesthetics
Check areas surrounding BMPs	Check for signs of erosion or instability and make sure that aesthetics are maintained throughout the BMP footprint,
Continue to support and educate "Green Teams" or other community groups	It is important to maintain community involvement and provide education and opportunities for service

	Example Construction Schedule												Long Term Maintenance Schedule											
	Month of Year												Month of Year											
	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8
Project site/Building Construction																								
Project site Stabilization																								
Temporary Stormwater Control at BMP Site																								
BMP Installation & Veg. Establishment																								
Post Wet-Weather Checks																								
Annual Key Milestones-BMP																								
Fall Bi-annual Inspection/Maintenance																								
Spring Bi-annual Inspection/Maintenance																								

★ Indicates inspection and/or Maintenance Activity (See corresponding checklist)

BMP Construction Record

BMP Number _____

BMP Type _____

Designed By _____

Installation Date _____

Scheduled 3 Month Inspection Date: _____

Actual 3 Month Inspection Date: _____

Installed By _____

Phone _____

Email _____

Maintenance Bond or Escrow Account? _____

Number: _____

Date of Expiration: _____

Final Inspection _____

Added to Agency Maintenance Schedule? _____

Inspection for First Two Growing Seasons:

1st Fall Inspection Scheduled _____

Actual 1st Fall Inspection Date: _____

1st Fall Maintenance Completed _____

1st Spring Inspection Scheduled _____

Actual 1st Spring Inspection Date: _____

1st Spring Maintenance Completed _____

2nd Fall Inspection Scheduled _____

Actual 2nd Fall Inspection Date: _____

2nd Fall Maintenance Completed _____

2nd Spring Inspection Scheduled _____

Actual 2nd Spring Inspection Date: _____

2nd Spring Maintenance Completed _____





BMP Exhibit Stations

Some frequently used forestry BMPs are demonstrated along sections of this trail.

Each station has an accompanying sign that explains what the BMP is, where it is commonly used, and why it is important.

Also provided are the necessary 'Keys to Success' that should be implemented for adequate BMP function.

Look for these BMPs as you travel from station to station through the forest:

Bridgemats

Over the river, and through the woods...

Broad Based Dip

This isn't just some dippy idea, it really works!

Cross-Drain

Water flows downhill, naturally...

Culvert Crossing

Pipe down...

Daylighting

Shed some light on the problem...

Deck or Landing

Don't get decked by erosion...

Erosion Control Mat

Bare soil? Cover it with a blanket...

Ford Crossing

Road vehicles only, no logging tractors please...

Geotextile

It's the fabric that binds the traveled way...

Gravel

A rolling stone also gathers no mud...

Preharvest Planning

Plan to succeed, and succeed with a plan...

Road Layout

If you build it, they will drive on it...

Rock Check Dam

More rock, less roll...

Sediment Pit, Silt Trap

Put sediment and silt in its place...

Silt Fence

Good fences, good neighbors, good water quality...

Site Rehabilitation

Fix it up when you're done...

Skid Trails

Don't leave a trail of mud behind...

Streamside Management Zone (SMZ)

.....smmmmmz...that's good water!

Turnout, Wing Ditch

Not preventing erosion is a real turn-off...

Waterbars

Caution! Speedbump Ahead...



Thank you for your interest in forestry BMPs and water quality! We hope you learned something valuable about how a working forest is the preferred land use for protecting your water resources.

Additional BMP, water quality, and non-point source pollution information is on the Web at:

www.dfr.state.nc.us

Answers: Waterbar; sediment pit; seed/mulch; road contour layout.

Educational State Forests (ESF) and State Forest locations

- Bladen Lakes State Forest, Bladen county
910/588-4964
- Clemmons ESF, Johnston & Wake counties
919/553-5651
- Dupont State Forest, Henderson & Transylvania co.
828/877-6527
- Holmes ESF, Henderson county
828/692-0100
- Jordan Lake ESF, Chatham county
919/542-1154
- Mountain Island ESF, Gaston & Lincoln counties
704/827-7576
- Rendezvous Mountain ESF, Wilkes county
336/667-5072
- Turnbull Creek ESF, Bladen county (Cover photo)
910/588-4161
- Tuttle ESF, Caldwell county
828-757-5608

If you can't visit us in person, visit us on the Web at: www.ncesf.org



Michael F. Easley
Governor

William G. Ross Jr.
Secretary



www.epa.gov/owow/nps



North Carolina
Non-point Source
Program

h2o.enr.state.nc.us



NORTH CAROLINA DEPARTMENT OF
ENVIRONMENT AND NATURAL RESOURCES

This brochure and project were developed by the N.C. Division of Forest Resources with a Non-Point Source (NPS) Management Program Grant through Section 319(h) of the 1987 revision to the Clean Water Act as administered by the U.S. Environmental Protection Agency and the N.C. Division of Water Quality.

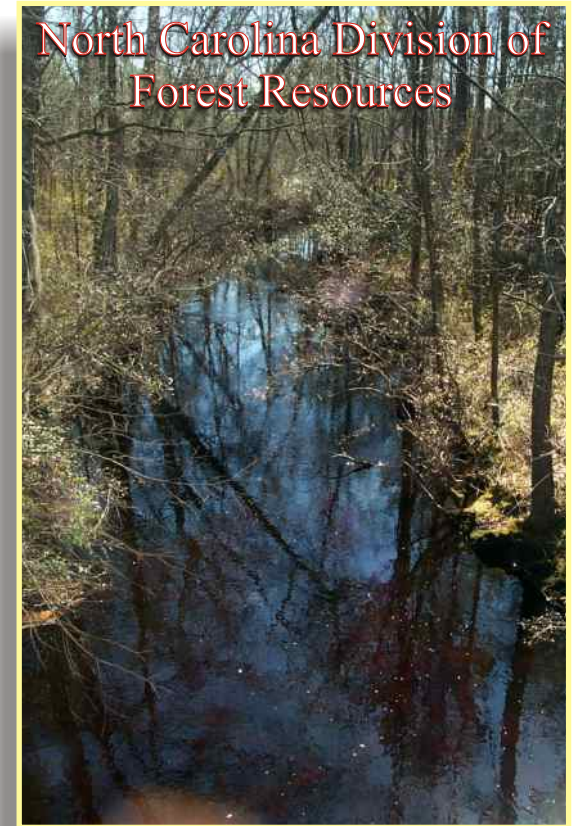
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Forestry

**Best
Management
Practices (BMP)**



Demonstration Trail



**Erosion Control &
Water Quality Protection**

Welcome to the Forestry BMP Demonstration Trail

The BMP's demonstrated along this trail will show how forestry activities can protect our water resources, while insuring a sustainable supply of renewable forest products that we all need and use.

Come along and enjoy the scenery, sounds, and smells of a working forest!



What Are Forestry BMPs?

Forestry Best Management Practices (BMPs) are proven, effective, and economical methods that prevent or control non-point source pollution runoff.

For a BMP to be considered practical for use in forestry, it must be:

- Technologically feasible
- Financially viable (not too expensive!)
- Legally allowable by all laws or rules

The Water Quality Rules for Forestry in North Carolina

In our state, there are performance - based standards that forestry operations must meet. These standards are essentially a series of goal-oriented 'best practices', that describe the desired end result, but not necessarily how to achieve that end result.

These performance standards are known as the "Forest Practices Guidelines Related to Water Quality" (FPGs).

The FPGs cover all phases of a forestry operation, including road construction, stream crossings, and timber harvesting, just to name a few.



The Difference Between FPGs and BMPs

In North Carolina, the FPGs are the rules! The FPGs require you to take whatever actions are needed to remain in compliance.

By selecting and implementing appropriate BMPs a logger, landowner, or forest manager can improve the likelihood that their forest management activities will remain in compliance with the FPGs.

Think of BMPs as the tools in your toolbox. You can pick one, or several, to meet your needs.

What Types of BMPs Are There?

- **BMPs can prevent runoff...**
- **Many BMPs control runoff...**
- **Other BMPs capture runoff...**

Plus, there are some BMPs that you do not actually see, but instead are part of the decision-making process when planning and conducting a forestry operation.



See if you can find the BMP example at each exhibit station.

(Hint: The signs should help you figure it out!)



How to Use BMPs

Effective use of BMPs is a multi-step process:

1. Select the correct BMP

Take into account the site conditions, type of activity, duration of work, and other factors specific to that operation.

2. Correctly implement the BMP

Doing things right the first time will usually save time and money, while protecting the water resources from the beginning, and not waiting until trouble occurs.

3. Monitor and maintain the BMP

Watch and examine how well the BMP is functioning. Recognizing a problem early, then fixing it, provides the best results!

4. Stabilize the site and close it out

Once the operation is complete, use BMPs to cover bare soil areas and rehabilitate sensitive areas near creeks. Also take this time to clean up the work area and make sure nothing is left behind that could wash away into the water.



These calculations should be used when designing the outlet structures for extended wet and dry detention basins (Sections 4.7 and 4.8). The water quality outlet size and the trash rack design will vary depending on structure type. Be sure to follow the design procedure outlined in Sections 4.7 and 4.8 to determine appropriate water quality outlet type.

WQ Outlet Design

Single Orifice

Orifice diameter

$$\text{Equation G.1 } D_o = 24 \sqrt{\frac{Q_{wQ}}{C_o \times \Pi \times \sqrt{2 \times g \times H_{wQ}}}}$$

Where:

D_o	=	Orifice diameter (inches)
Q_{wQ}	=	Average WQ outflow rate (cubic feet per second)
C_o	=	Orifice coefficient (1.0 for circular entrance, 0.62 for square-edged entrance)
H_{wQ}	=	Average head of WQ_v over invert of WQ outlet (feet)

Perforated riser/Orifice Plate

Outlet area per perforation row

$$\text{Equation G.2 } A_o = \frac{WQ_v}{n \times Z_{wQ}^2 + 0.22Z_{wQ} - .10}$$

Where:

A_o	=	Recommended maximum outlet area per row (square inches)
WQ_v	=	Water quality volume (acre feet)
Z_{wQ}	=	Depth of WQ_v over above permanent pool (feet) (determined by designer)
n	=	Manning's 'n' for perforated pipe

Circular perforation diameter per row

$$\text{Equation G.3 } D_1 = \sqrt{\frac{4A_o}{\Pi}}$$

Where:

D_1	=	Circular perforation diameter per row (inch)
A_o	=	Maximum outlet area per row of perforations (square inch)

Circular perforation diameter

$$\text{Equation G.4 } D_{perf} = \sqrt{\frac{4A_o}{\Pi n_c}}$$

Where:

D_{perf}	=	Circular perforation diameter (inch)
A_o	=	Maximum outlet area per row of perforations (square inch)
n_c	=	Number of columns of perforations

Number of perforation rows

$$\text{Equation G.5 } n_f = \frac{12Z_{wQ}}{S_c}$$

Where:

n_f	=	Number of rows of perforations
Z_{wQ}	=	Depth of WQ_v over above permanent pool (feet)
S_c	=	Center to center column spacing; if $n > 1$, $S_c = 4$ inch

V-notch Weir

Weir angle (with calculator set in radians)

$$\text{Equation G.6 } \theta = 2 \left(\frac{180}{\Pi} \right) \arctan \left(\frac{Q_{WQ}}{C_V \times H_{WQ}^{5/2}} \right)$$

Where:

θ	=	V-notch weir angle (degrees)
Q_{WQ}	=	Average WQ outflow rate (cubic feet per second)
C_V	=	V-notch coefficient (2.5 is typical value)
H_{WQ}	=	Average head of WQ _V over invert of WQ outlet (feet)

OR

Weir angle (with calculator set in degrees)

$$\text{Equation G.7 } \theta = 2 \arctan \left(\frac{Q_{WQ}}{C_V \times H_{WQ}^{5/2}} \right)$$

Where:

θ	=	V-notch weir angle (degrees)
Q_{WQ}	=	Average WQ outflow rate (cubic feet per second)
C_V	=	V-notch coefficient (2.5 is typical value)
H_{WQ}	=	Average head of WQ _V over invert of WQ outlet (feet)

Top width of V-notch weir

$$\text{Equation G.8 } W_V = 2 \times Z_{WQ} \times \tan \left(\frac{\theta}{2} \right)$$

Where:

W_V	=	V-notch top width (feet)
θ	=	V-notch weir angle (degrees)
Z_{WQ}	=	Depth of WQ _V over above permanent pool (feet)

Trash Rack Design

Single Orifice

Water quality outlet area

$$\text{Equation G.9 } A_{OT} = \frac{\Pi}{4} D_o^2$$

Where:

A_{OT}	=	Outlet area (square inches)
D_o	=	Orifice diameter (inches) calculated in Equation G.1

Trash rack open area

$$\text{Equation G.10 } A_T = A_{OT} \times 77e^{(-0.124D_o)}$$

Where:

A_T	=	Required trash rack open area (square inches)
A_{OT}	=	Outlet area (square inches) calculated in Equation G.9
D_o	=	Orifice diameter (inches) calculated in Equation G.1

Perforated riser/Orifice Plate

Water quality outlet area

$$\text{Equation G.11 } A_{OT} = A_O \times n_C \times n_F$$

Where:

A_{OT} = Outlet area (square inches)

A_O = Maximum outlet area per row (square inches) calculated in Equation G.2.

n_C = Number of perforation columns calculated in Equation G.4

n_f = Number of perforations rows calculated in Equation G.5

Trash rack open area

$$\text{Equation G.12 } A_T = \frac{A_{OT}}{2} \times 77e^{(-0.124D_1)}$$

Where:

A_T = Required trash rack open area (square inches)

A_{OT} = Outlet area (square inches) calculated in Equation G.11

D_1 = Circular perforation diameter per row (inch) calculated in Equation G.3.

V-notch Weir

Water quality outlet area

$$\text{Equation G.13 } A_{OT} = \frac{1}{2} W_V \times \sin\left(\frac{\theta}{2}\right)$$

Where:

A_{OT} = Outlet area (square inches)

W_V = V-notch top width (feet) calculated in Equation G.8.

θ = V-notch weir angle (degrees) calculated in Equation G.7.

Trash rack open area

$$\text{Equation G.13 } A_T = 4A_{OT}$$

Where:

A_T = Required trash rack open area (square inches)

A_{OT} = Outlet area (square inches) calculated in Equation G.13

Design Procedure Form: Extended Dry Detention Basin (EDDB)
Main Worksheet

Designer: _____
 Checked By: _____
 Company: _____
 Date: _____
 Project: _____
 Location: _____

<u>I. Basin Water Quality Storage Volume</u>		
Step 1) Tributary area to EDDB, A_T (ac)	A_T (ac) =	50.0
Step 2) Calculate WQv	WQv (ac-ft) =	2.4
Step 3) Add 20 percent to account for silt and sediment deposition in the basin.	V_{design} (ac-ft) =	2.9
<u>IIa. Water Quality Outlet Type</u>		
Step 1) Set water quality outlet type: Type 1 = single orifice Type 2 = perforated riser or plate Type 3 = v-notch weir	Outlet Type =	1.0
Step 2) Proceed to step 2b, 2c, or 2d based on water quality outlet type selected		
<u>IIb. Water Quality Outlet, Single Orifice</u>		
Step 1) Depth of water quality volume at outlet, Z_{WQ} (ft)	Z_{WQ} (ft) =	3.0
Step 2) Average head of water quality volume over invert of orifice, H_{WQ} (ft) $H_{WQ} = 0.5 * Z_{WQ}$	H_{WQ} (ft) =	1.5
Step 3) Average water quality outflow rate, Q_{WQ} (cfs) $Q_{WQ} = (WQv * 43,560) / (40 * 3,600)$	Q_{WQ} (cfs) =	0.7
Step 4) Set value of orifice discharge coefficient, C_o	C_o =	0.6
Step 5) Water quality outlet orifice diameter (minimum of 4 inches), D_o (in) $D_o = 12 * 2 * (Q_{WQ} / (C_o * \pi * (2 * g * H)^{0.5}))^{0.5}$ (If orifice diameter < 4 inches, use outlet type 2 or 3)	D_o (in) =	4.7
Step 6) To size outlet orifice for EDDB with an irregular stage-volume relationship, use the Single Orifice Worksheet		
<u>IIc. Water Quality Outlet, Perforated Riser</u>		
Step 1) Depth at outlet above lowest perforation, Z_{WQ} (ft)	Z_{WQ} (ft) =	_____
Step 2) Recommended maximum outlet area per row, A_o (in ²) $A_o = (WQv) / (0.013 * Z_{WQ}^2 + 0.22 * Z_{WQ} - 0.10)$	A_o (in ²) =	_____
Step 3) Circular perforation diameter per row assuming a single column, D_1 (in)	D_1 (in) =	_____
Step 4) Number of columns, n_c	n_c =	_____
Step 5) Design circular perforation diameter (should be between 1 and 2 inches), D_{perf} (in)	D_{perf} (in) =	_____
Step 6) Horizontal perforation column spacing when $n_c > 1$, center to center, S_c If $D_{perf} \geq 1.0$ in, $S_c = 4$	S_c (in) =	_____
Step 7) Number of rows (4" vertical spacing between perforations, center to center), n_r	n_r =	_____

Design Procedure Form: Extended Dry Detention Basin (EDDB)
Main Worksheet

Designer: _____
 Checked By: _____
 Company: _____
 Date: _____
 Project: _____
 Location: _____

<u>II. Water Quality Outlet, V-notch Weir</u>	
Step 1) Depth of water quality volume above permanent pool, Z_{WQ} (ft)	Z_{WQ} (ft) = _____
Step 2) Average head of water quality pool volume over invert of v-notch, H_{WQ} (ft) $H_{WQ} = 0.5 * Z_{WQ}$	H_{WQ} (ft) = _____
Step 3) Average water quality pool outflow rate, Q_{WQ} (cfs) $Q_{WQ} = (WQ_v * 43,560) / (40 * 3,600)$	Q_{WQ} (cfs) = _____
Step 4) V-notch weir coefficient, C_v	C_v = _____
Step 5) V-notch weir angle, θ (deg) $\theta = 2 * (180/\pi) * \arctan(Q_{WQ} / (C_v * H_{WQ}^{5/2}))$ V-notch angle should be at least 20 degrees. Set to 20 degrees if calculated angle is smaller.	θ (deg) = _____
Step 6) Top width of V-notch weir $W_v = 2 * Z_{WQ} * \tan(\theta/2)$	W_v (ft) = _____
Step 7) To calculate v-notch angle for EDDB with an irregular stage-volume relationship, use the V-notch Weir Worksheet	
<u>III. Flood Control</u>	
Refer to local agency specification.	
<u>IV. Trash Racks</u>	
Step 1) Total outlet area, A_{ot} (in ²)	A_{ot} (in ²) = 17.0
Step 2) Required trash rack open area, A_t (in ²) $A_t = A_{ot} * 77 * e^{(-0.124 * D)}$ for single orifice outlet $A_t = (A_{ot}/2) * 77 * e^{(-0.124 * D)}$ for orifice plate outlet $A_t = 4 * A_{ot}$ for v-notch weir outlet	A_t (in ²) = 732.1
<u>V. Basin Shape</u>	
Step 1) Length to width ratio should be at least 3:1 (L:W) wherever practicable	(L:W) = _____
Step 2) Low flow channel side lining	Concrete: _____ Soil / riprap: _____ No low flow channel: _____
Step 3) Top stage floor drainage slope (toward low flow channel), S_{is} (%) Top stage depth, D_{is} (ft)	S_{is} (%) = _____ D_{is} (ft) = _____
Step 4) Bottom stage volume, V_{bs} (ac-ft)	V_{bs} (% of WQ_v) _____ V_{bs} (ac-ft) _____
<u>VI. Forebay (Optional)</u>	
Step 1) Volume should be greater than 10% of WQ_v	Min Vol_{FB} (ac-ft) = 0.2
Step 2) Forebay depth, Z_{FB} (ft)	Z_{FB} (ft) = 4.0
Step 3) Forebay surface area, A_{FB} (ac)	Min A_{FB} (ac) = 0.1
Step 4) Paved/hard bottom and sides?	_____

Design Procedure Form: Extended Dry Detention Basin (EDDB)
Main Worksheet

Designer: _____
Checked By: _____
Company: _____
Date: _____
Project: _____
Location: _____

<u>VII. Basin side slopes</u> Basin side slopes should be at least 4:1 (H:V) Side Slope (H:V) = _____
<u>VIII. Dam Embankment side slopes</u> Dam Embankment side slopes should not exceed 3:1 (H:V) Dam Embankment (H:V) = _____
<u>IX. Vegetation</u> Check the method of vegetation planted in the EDDB or describe "other" ☐ Native Grass ☐ Irrigated Turf Grass ☐ Other: _____ _____
<u>X. Inlet Protection</u> Indicate method of inlet protection/energy dissipation at EDDB inlet _____
<u>XI. Access</u> Indicate that access has been provided for maintenance vehicles. _____

Design Procedure Form: Extended Wet Detention Basin (EWDB) Main Worksheet

Designer: _____
Checked By: _____
Company: _____
Date: _____
Project: _____
Location: _____

I. Basin Water Quality Volume

Step 1) Tributary area to EWDB, A_T (ac) A_T (ac) = 50.0

Step 2) Calculate WQv WQv (ac-ft) = 4.0

IIa. Permanent Pool Volume

Step 1) Average 14 day wet season rainfall, R_{14} (in) R_{14} (in) = 2.0

Step 2) Rational runoff coefficient, C C = 0.8
 $C = 0.3 + 0.6 * I$
 I = percent impervious area divided by 100

Step 3) Permanent pool volume 1, V_{P1} (ac-ft) V_{P1} (ac-ft) = 6.7
 $V_{P1} = (C * A_T * R_{14})/12$

IIb. Sedimentation Volume.

Step 1) Ratio of basin volume to runoff volume, $V_{B/R}$ $V_{B/R}$ = 4.0
 (from Figure 12; $V_{B/R}$ should be ≥ 4.0)

Step 2) Mean storm depth, S_d (in) S_d (in) = 0.5

Step 3) Impervious tributary area, A_i (ac) A_i (ac) = 42.5

Step 4) Permanent pool volume by Method 2, V_{P2} (ac-ft) V_{P2} (ac-ft) = 6.5
 $V_{P2} = (V_{B/R} * S_d * A_i)/12$

IIc. Permanent Pool Design Volume

Step 1) Design permanent pool volume, V_p , as larger of volumes calculated in IIa and Iib plus 20% V_p (ac-ft) = 8.0

Step 2) Average permanent pool depth, Z_p (ft) Z_p (ft) = 4.0

Step 3) Permanent pool surface area, A_p (ac) A_p (ac) = 2.0

Designer: _____
Checked By: _____
Company: _____
Date: _____
Project: _____
Location: _____

Step 1) Set water quality outlet type:	Outlet Type =	2.0
Type 1 = single orifice		
Type 2 = perforated riser or plate		
Type 3 = v-notch weir		

Step 7) Number of rows (4" vertical spacing between perforations, center to center), n_r $n_r = 9.0$

Design Procedure Form: Extended Wet Detention Basin (EWDB) Main Worksheet

Designer: _____
Checked By: _____
Company: _____
Date: _____
Project: _____
Location: _____

IIIId. Water Quality Outlet, V-Notch Weir⁶

- Step 1) Depth of water quality volume above permanent pool, Z_{WQ} (ft) Z_{WQ} (ft) = _____
- Step 2) Average head of water quality pool volume over invert of v-notch, H_{WQ} (ft)
 $H_{WQ} = 0.5 * Z_{WQ}$ H_{WQ} (ft) = _____
- Step 3) Average water quality pool outflow rate, Q_{WQ} (cfs)
 $Q_{WQ} = (WQv * 43,560) / (40 * 3,600)$ Q_{WQ} (cfs) = _____
- Step 4) V-notch weir coefficient, C_v C_v = _____
- Step 5) V-notch weir angle, θ (deg)
 $\theta = 2 * (180/\pi) * \arctan(Q_{WQ} / (C_v * H_{WQ}^{5/2}))$
 V-notch angle should be at least 20 degrees. Set to 20 degrees if calculated angle is smaller. θ (deg) = _____
- Step 6) V-notch weir top width, W_v (ft)
 $W_v = 2 * Z_{WQ} * \tan(\theta/2)$ W_v (ft) = _____
- Step 7) To calculate v-notch angle for EWDB with an irregular stage-volume relationship, use the V-notch Weir Worksheet

IV. Trash Racks

- Step 1) Total outlet area, A_{ot} (in²) A_{ot} (in²) = 106.4
- Step 2) Required trash rack open area, A_t (in²)
 $A_t = A_{ot} * 77 * e^{(-0.124 * D)}$ for single orifice outlet
 $A_t = (A_{ot}/2) * 77 * e^{(-0.124 * D)}$ for orifice plate or perforated riser outlet
 $A_t = 4 * A_{ot}$ for v-notch weir outlet A_t (in²) = 2910.6

V. Forebay

- Step 1) Volume should equal at least 10% of WQv Min Vol_{FB} (ac-ft) = 0.4
- Step 2) Forebay depth, Z_{FB} (ft) Z_{FB} (ft) = 4.0
- Step 3) Minimum forebay surface area, A_{FB} (ac) Min A_{FB} (ac) = 0.1
- Step 4) Paved/hard bottom and sides? _____

**Design Procedure Form: Extended Wet Detention Basin (EWDB)
Main Worksheet**

Designer: _____
Checked By: _____
Company: _____
Date: _____
Project: _____
Location: _____

VI. Littoral Bench

Step 1) Littoral bench should be 25% - 50% of the permanent pool surface area	Min A_{LB} (ac) =	0.5
	Max A_{LB} (ac) =	1.0
Step 2) Approximate minimum and maximum bench widths, assuming circular permanent pool	Min W_{LB} (ft) =	83.4
	Max W_{LB} (ft) =	117.9
Step 3) Design bench width around perimeter of EWDB, W_{LB} (ft)	W_{LB} (ft) =	100.0
Step 4) Bench depth below permanent pool surface, Z_{LB} (ft)	Z_{LB} (ft) =	12.0

VII. Basin side slopes

Basin side slopes should be at least 4:1 (H:V) Side Slope (H:V) = _____

VIII. Dam Embankment side slopes

Dam Embankment side slopes should be at least 3:1 (H:V) Dam Embankment (H:V) = _____

IX. Vegetation

Check the method of vegetation planted in the EWDB or describe "other"

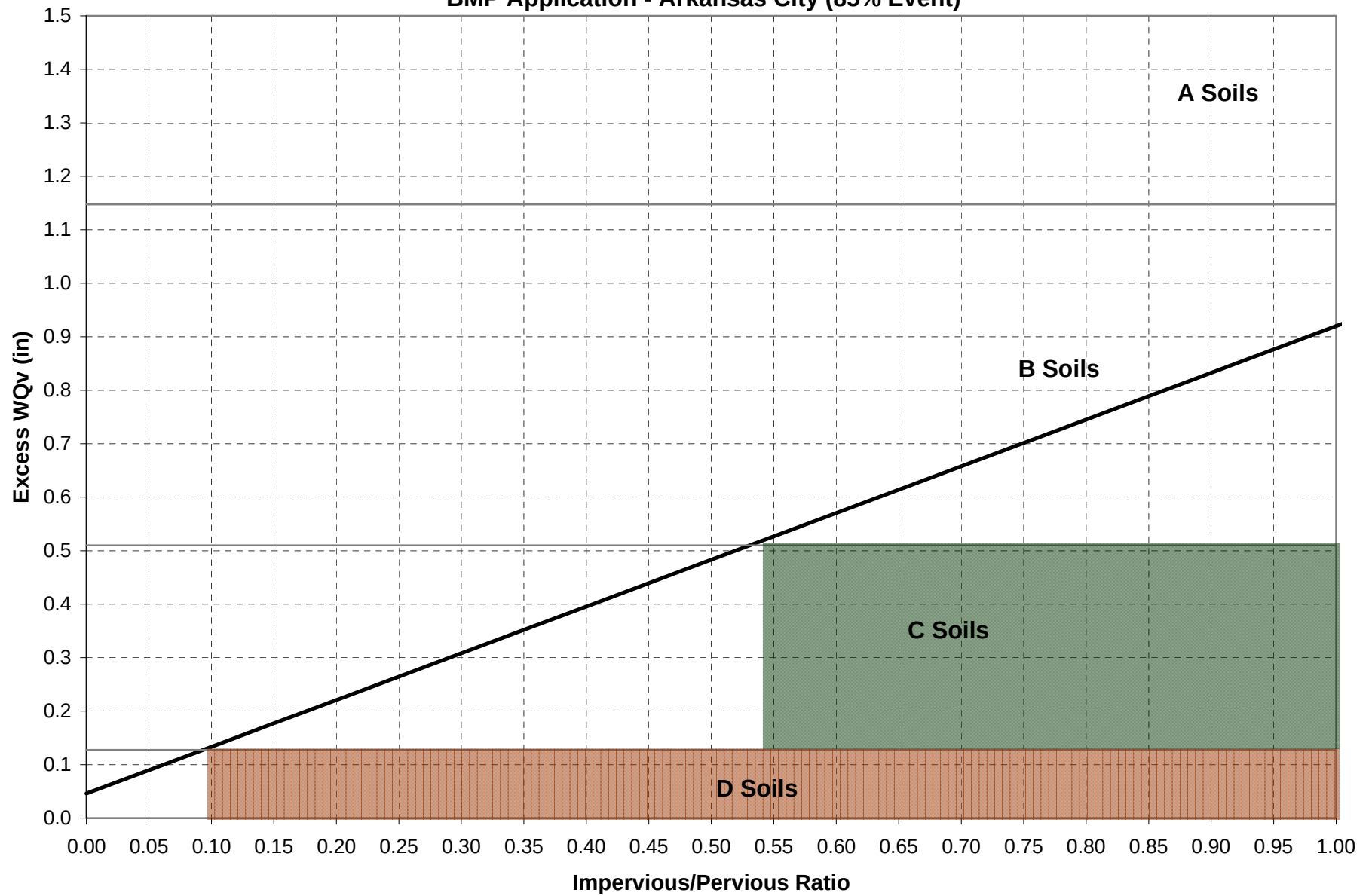
	☐ Native Grass
	☐ Irrigated Turf Grass
	☐ Native Aquatic Species
	☐ Other: _____

X. Inlet Protection

Indicate method of inlet protection/energy dissipation at EWDB inlet _____



BMP Application - Arkansas City (85% Event)



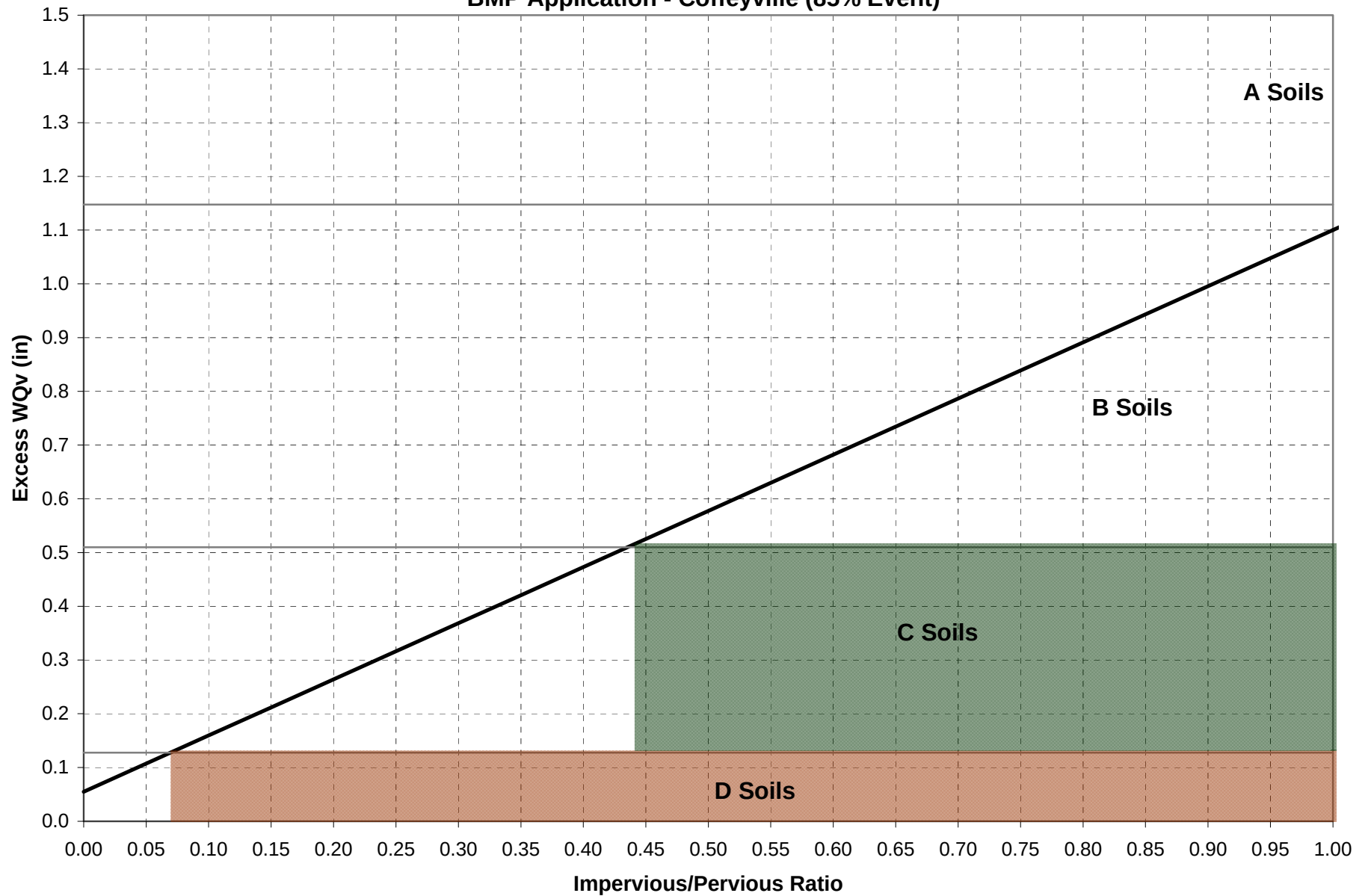
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Coffeyville (85% Event)



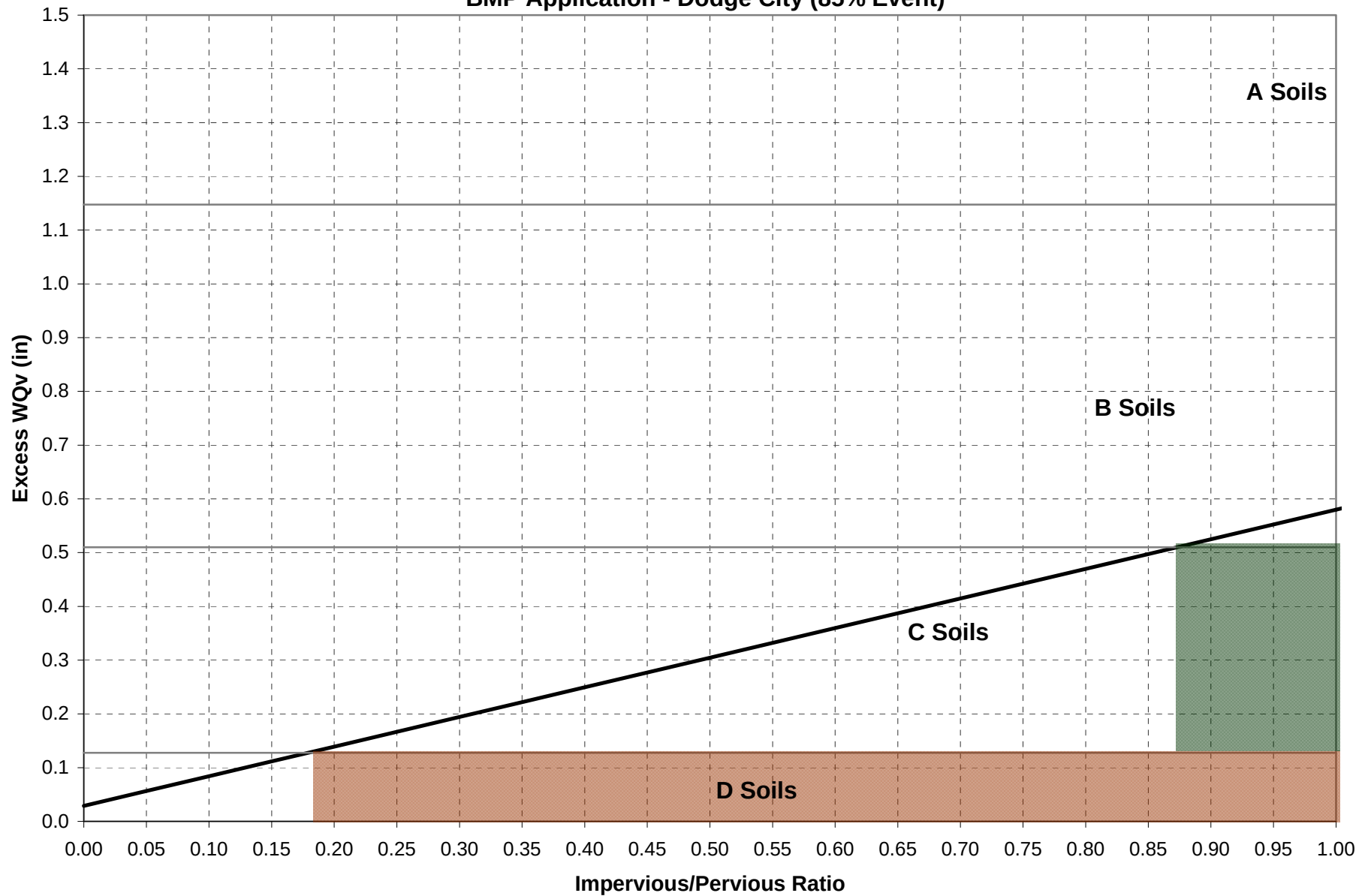
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Dodge City (85% Event)



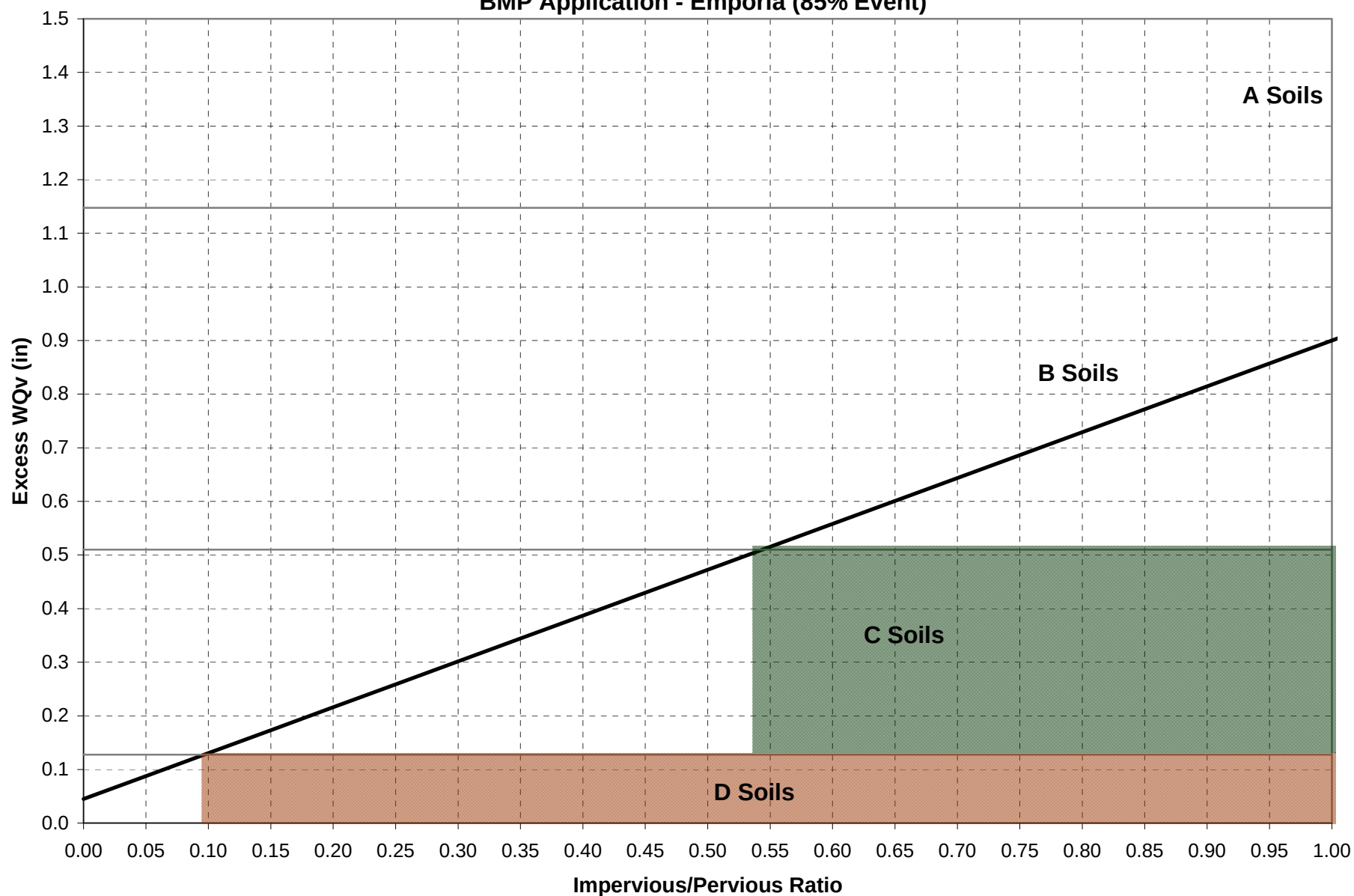
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Emporia (85% Event)



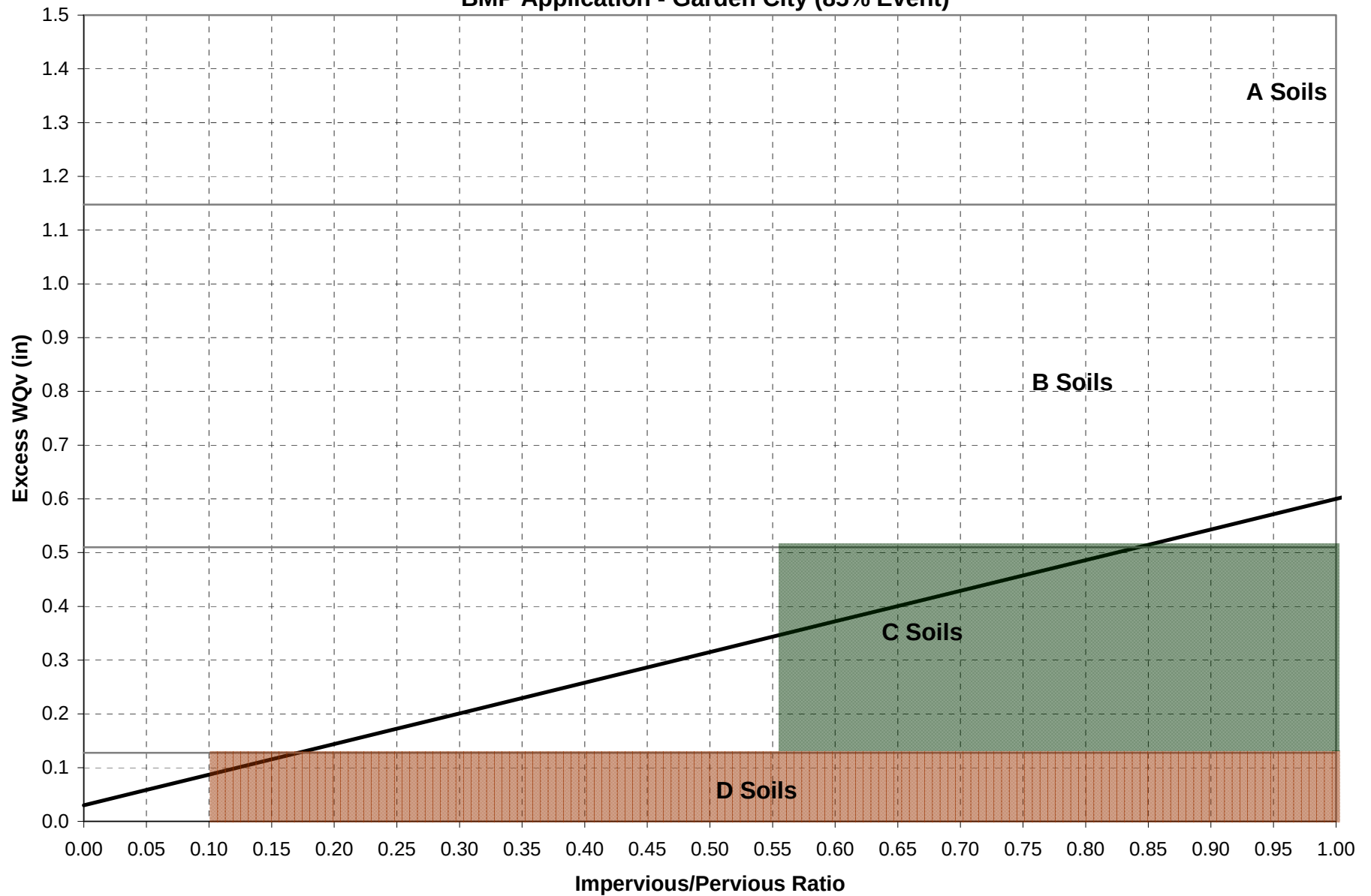
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Garden City (85% Event)



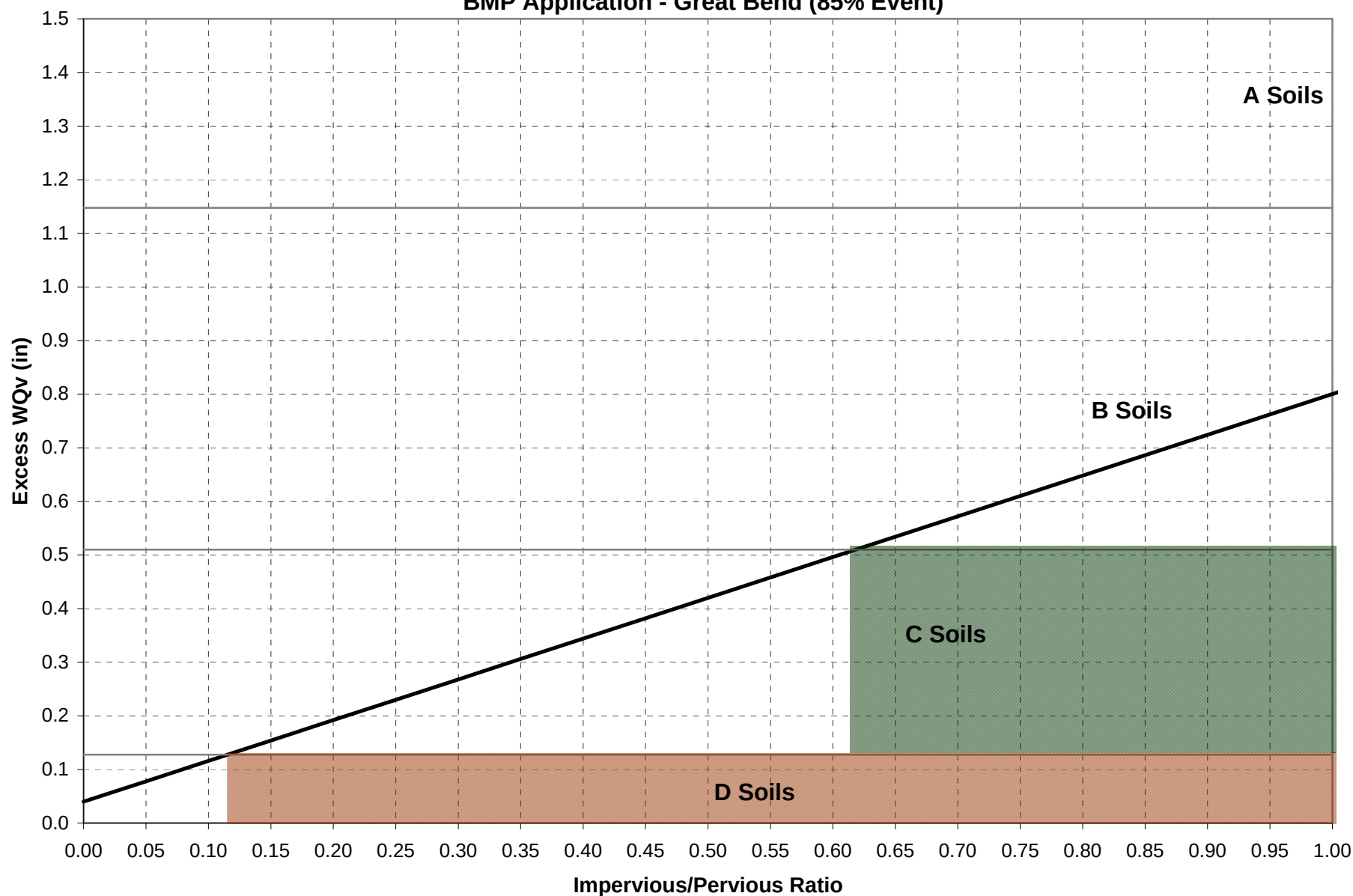
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Great Bend (85% Event)



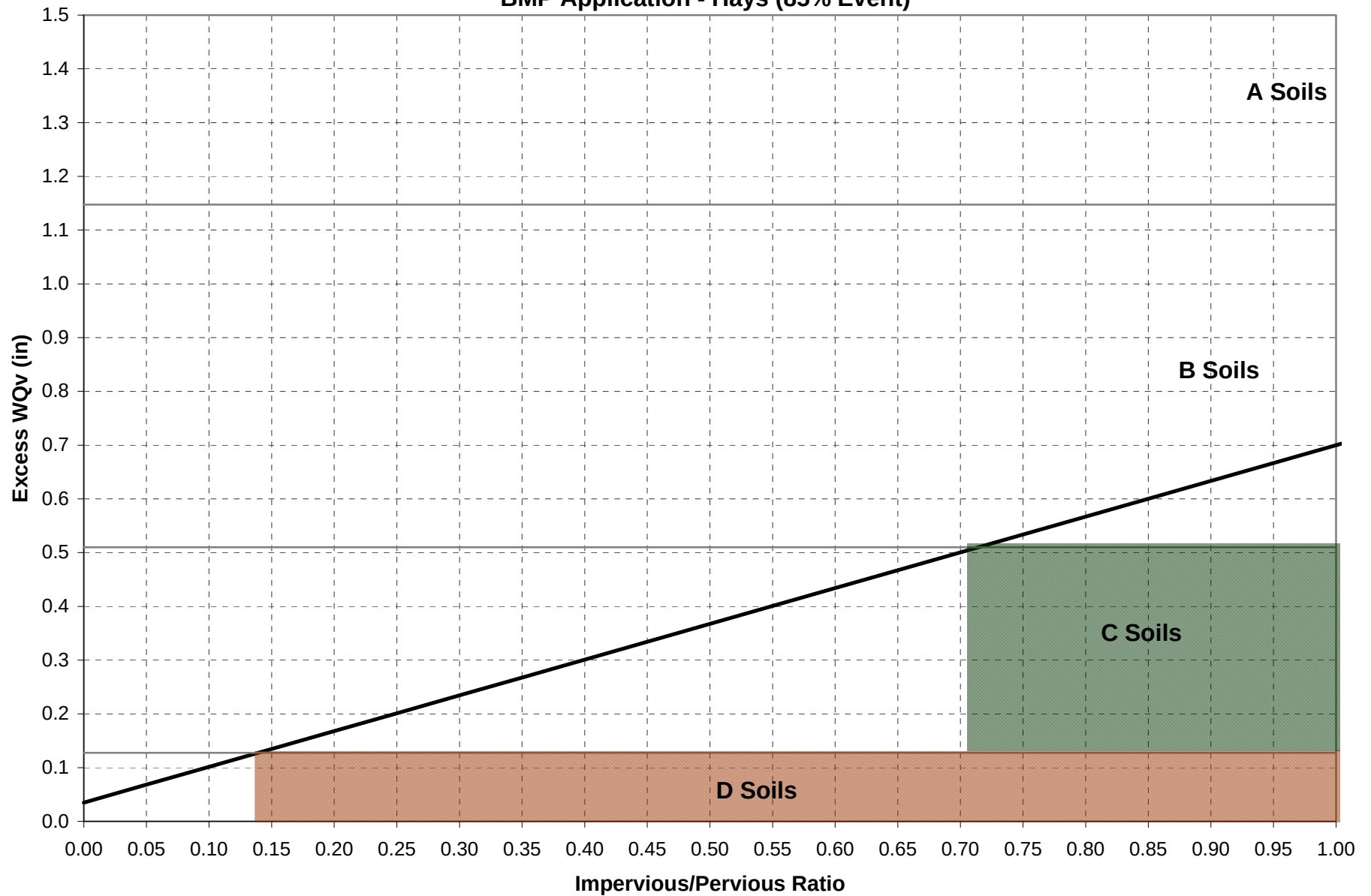
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Hays (85% Event)



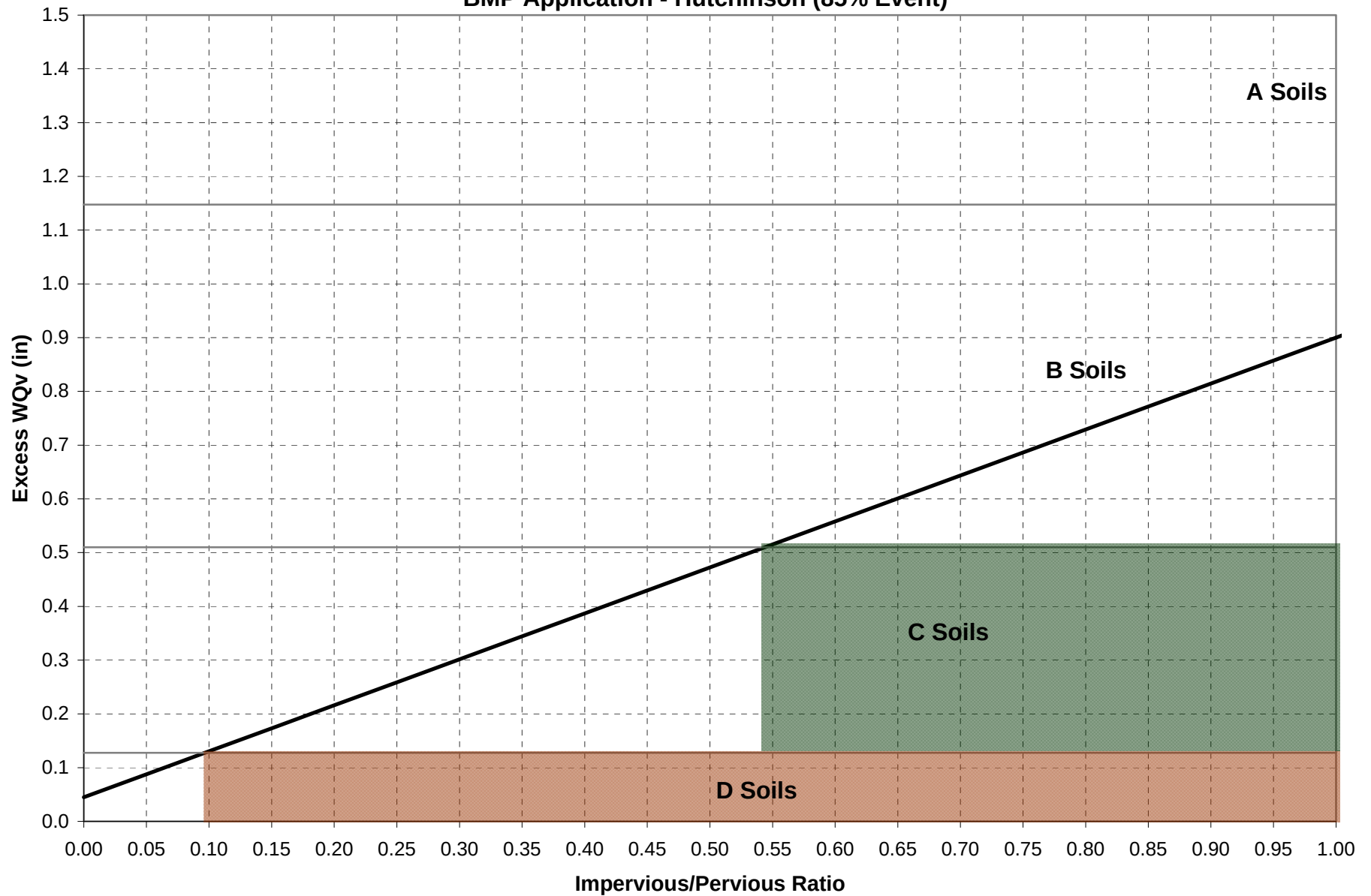
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Hutchinson (85% Event)



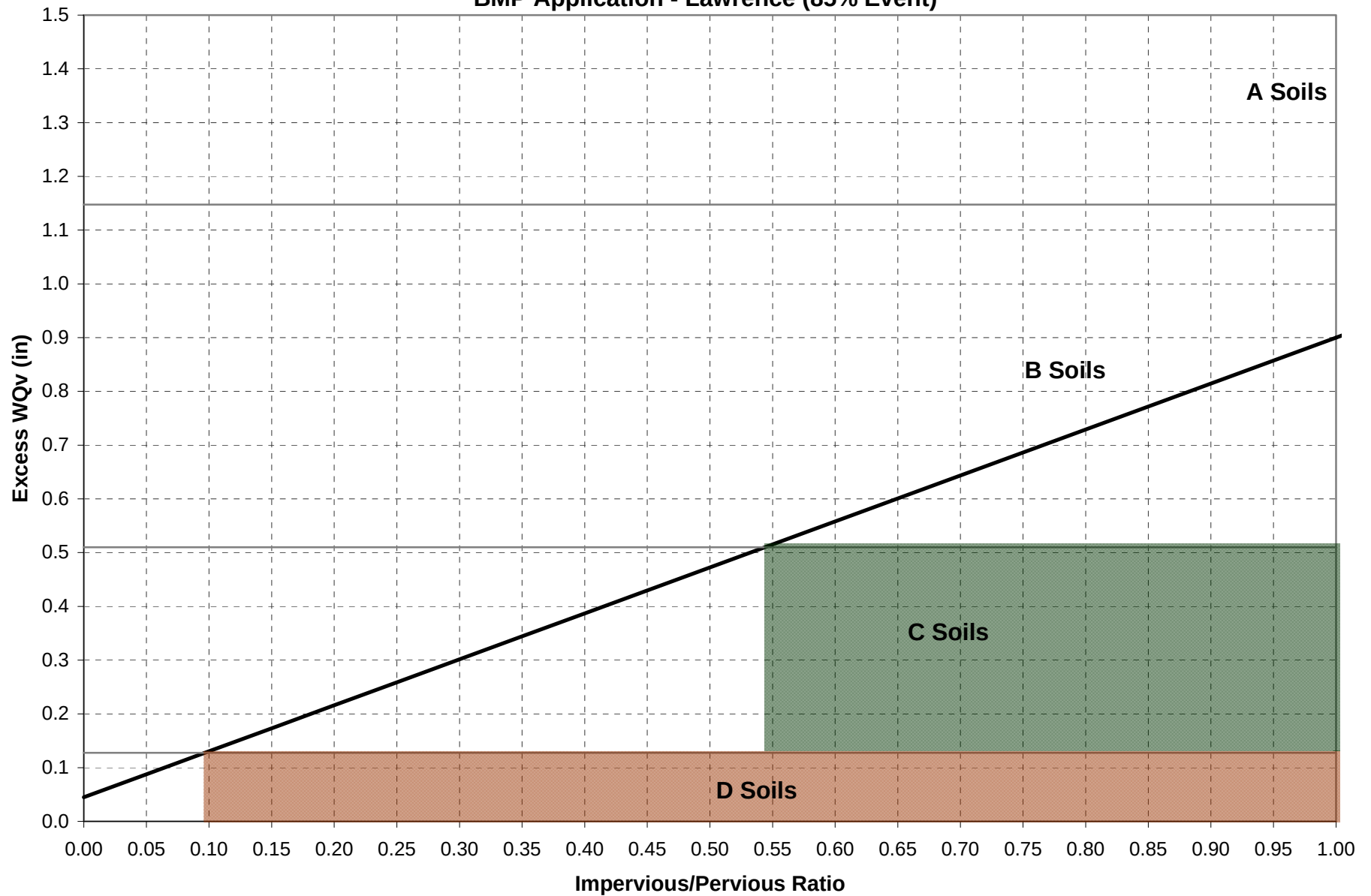
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Lawrence (85% Event)



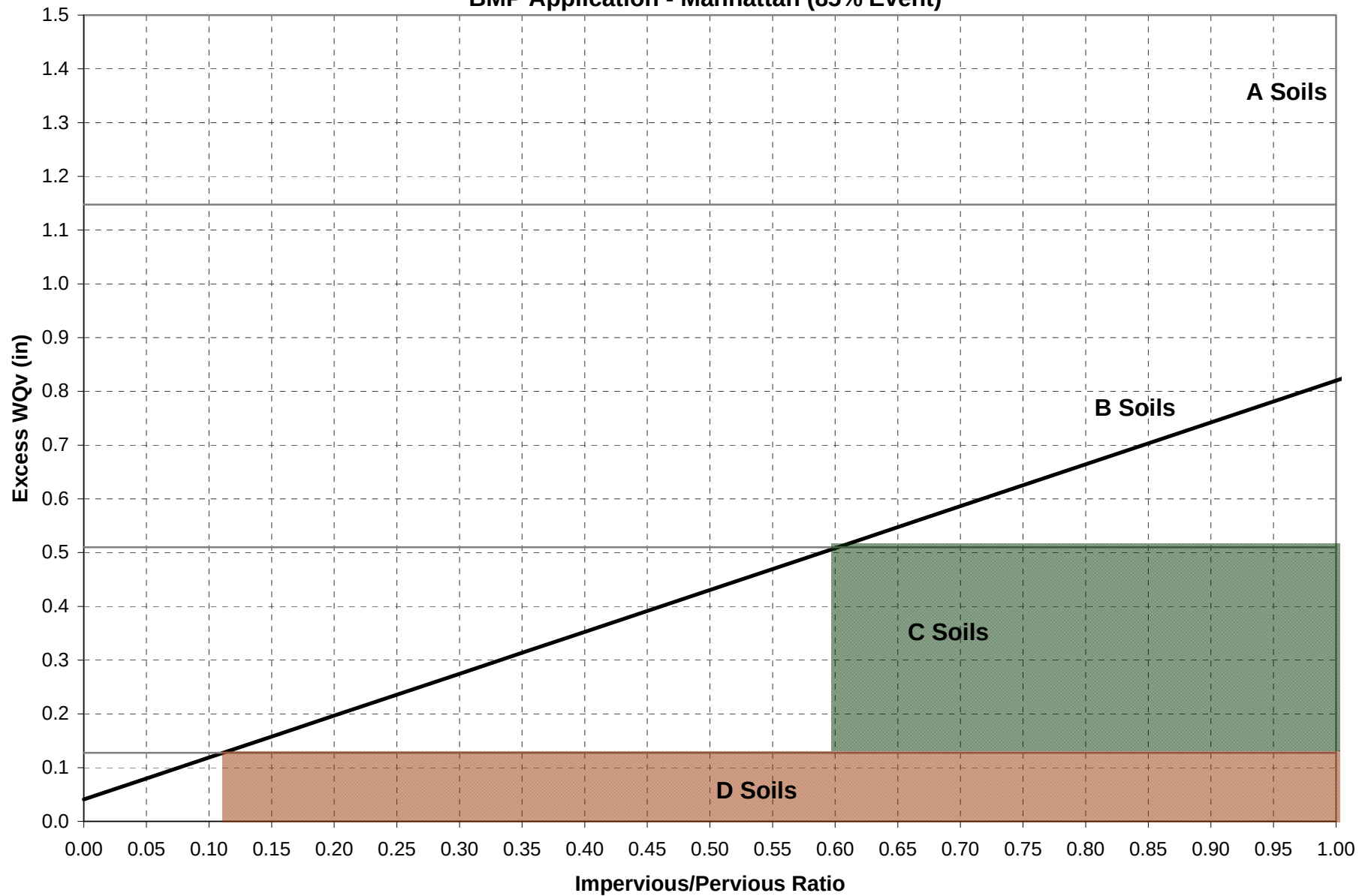
BMPs required within shaded area.

BMPs required for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Manhattan (85% Event)



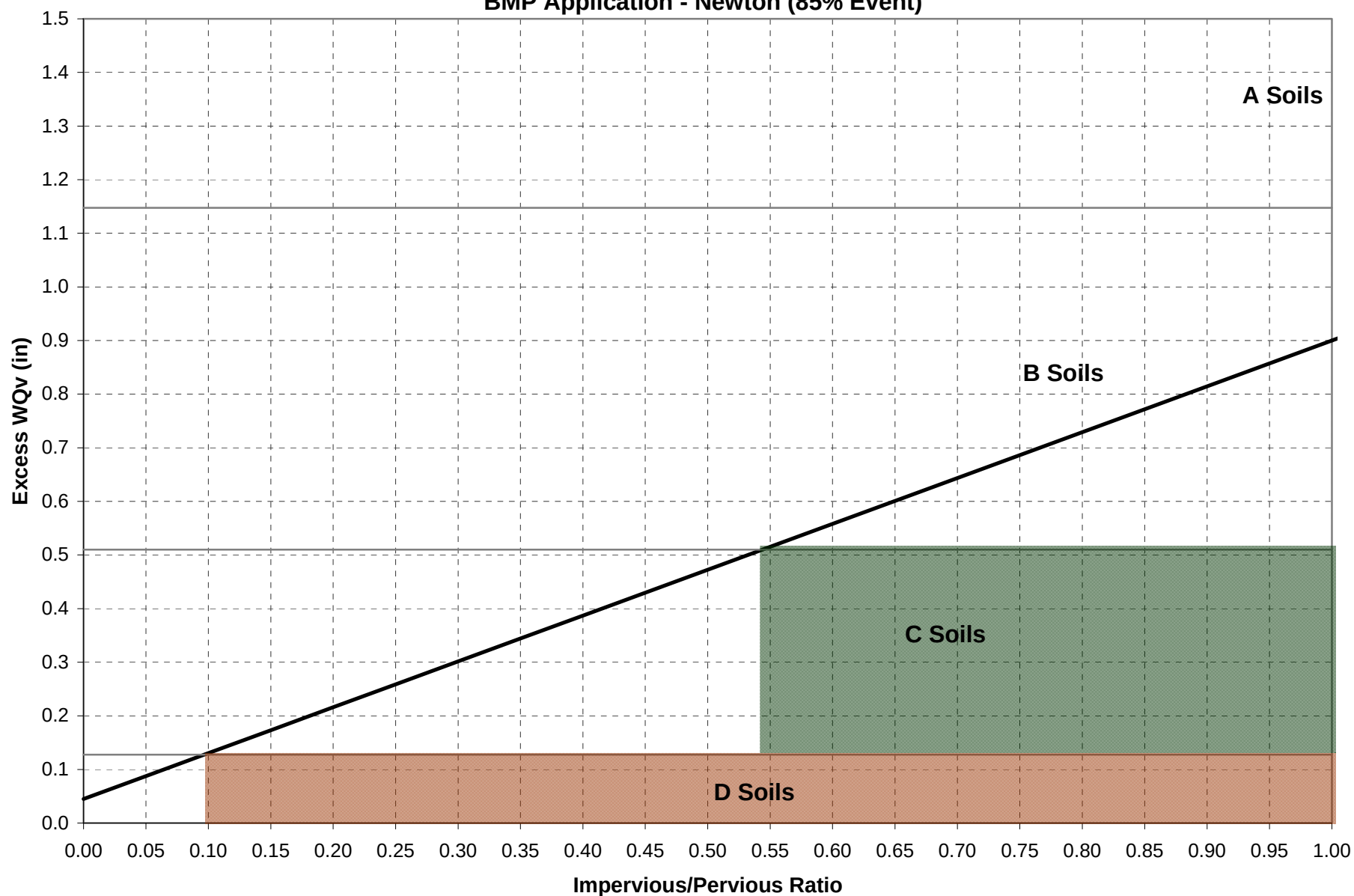
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Newton (85% Event)



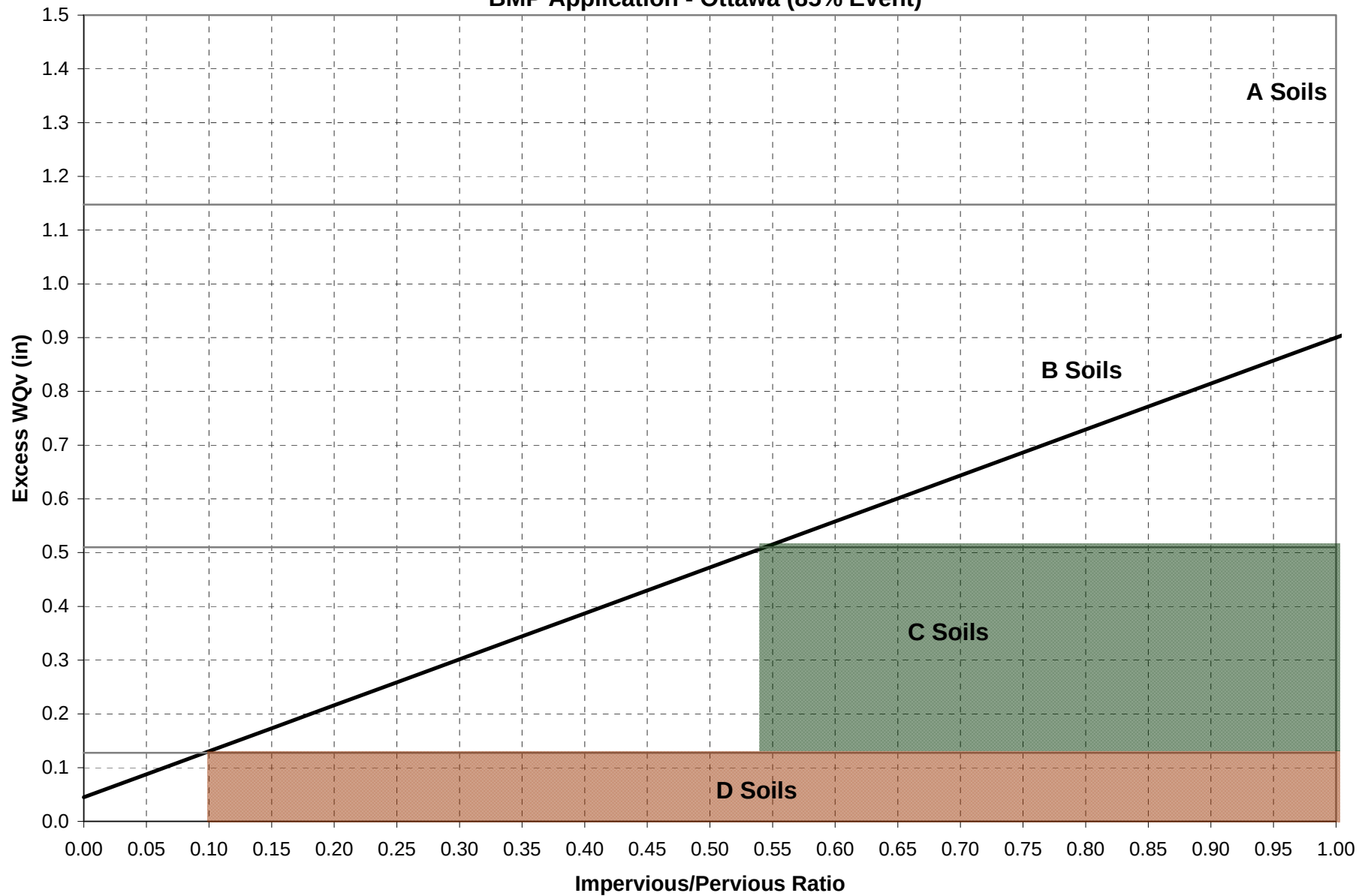
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Ottawa (85% Event)



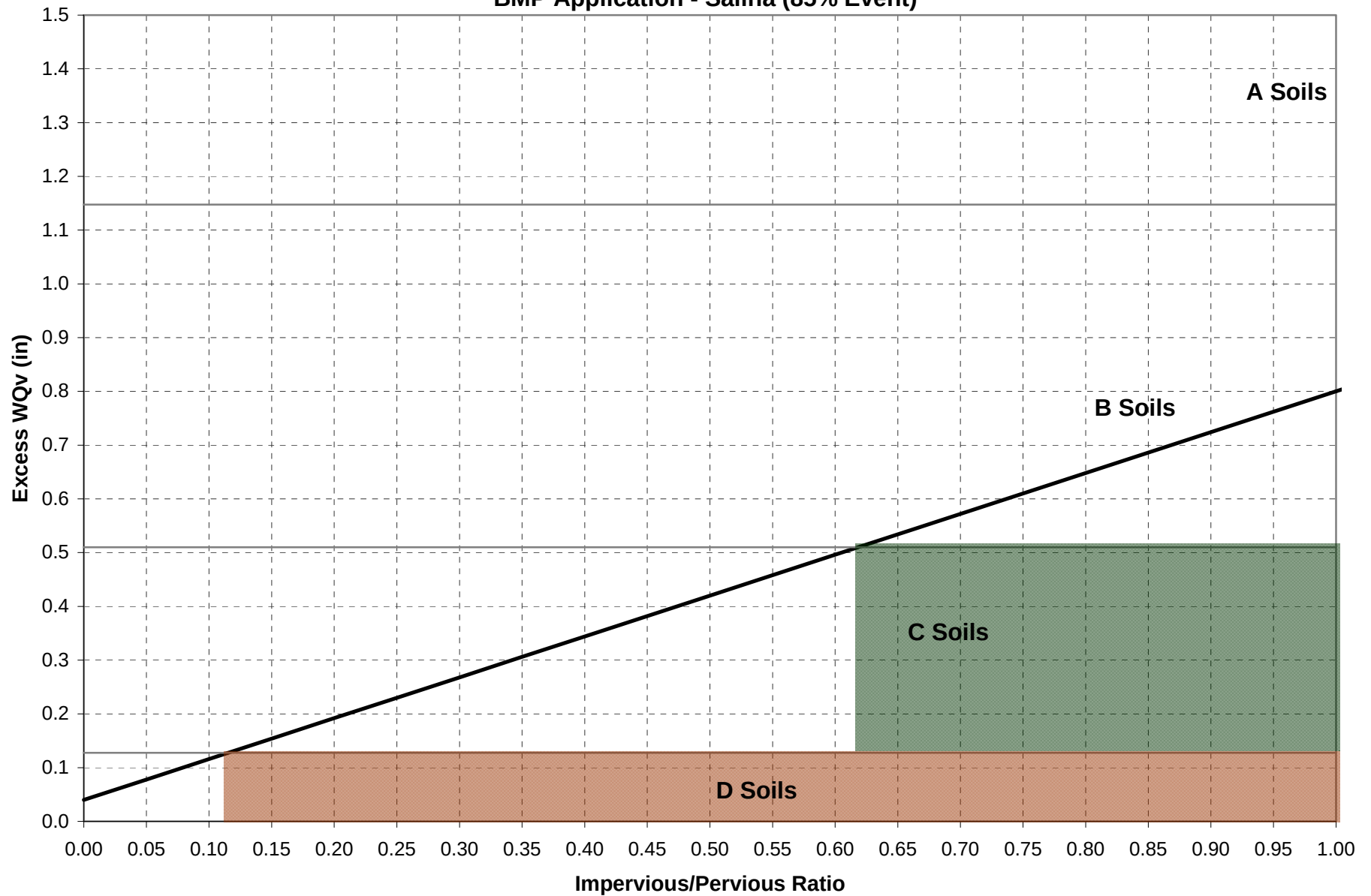
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Salina (85% Event)



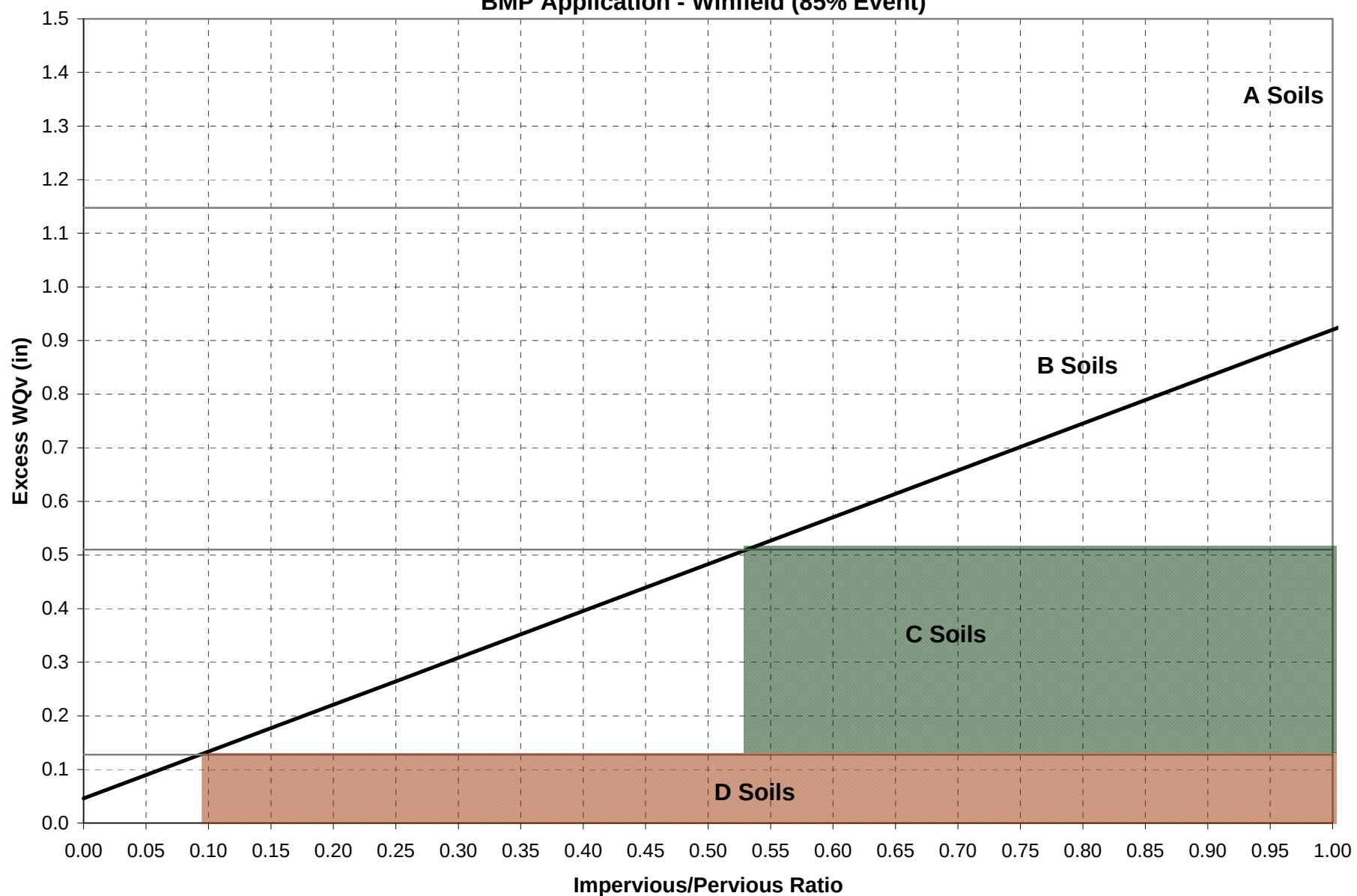
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Winfield (85% Event)



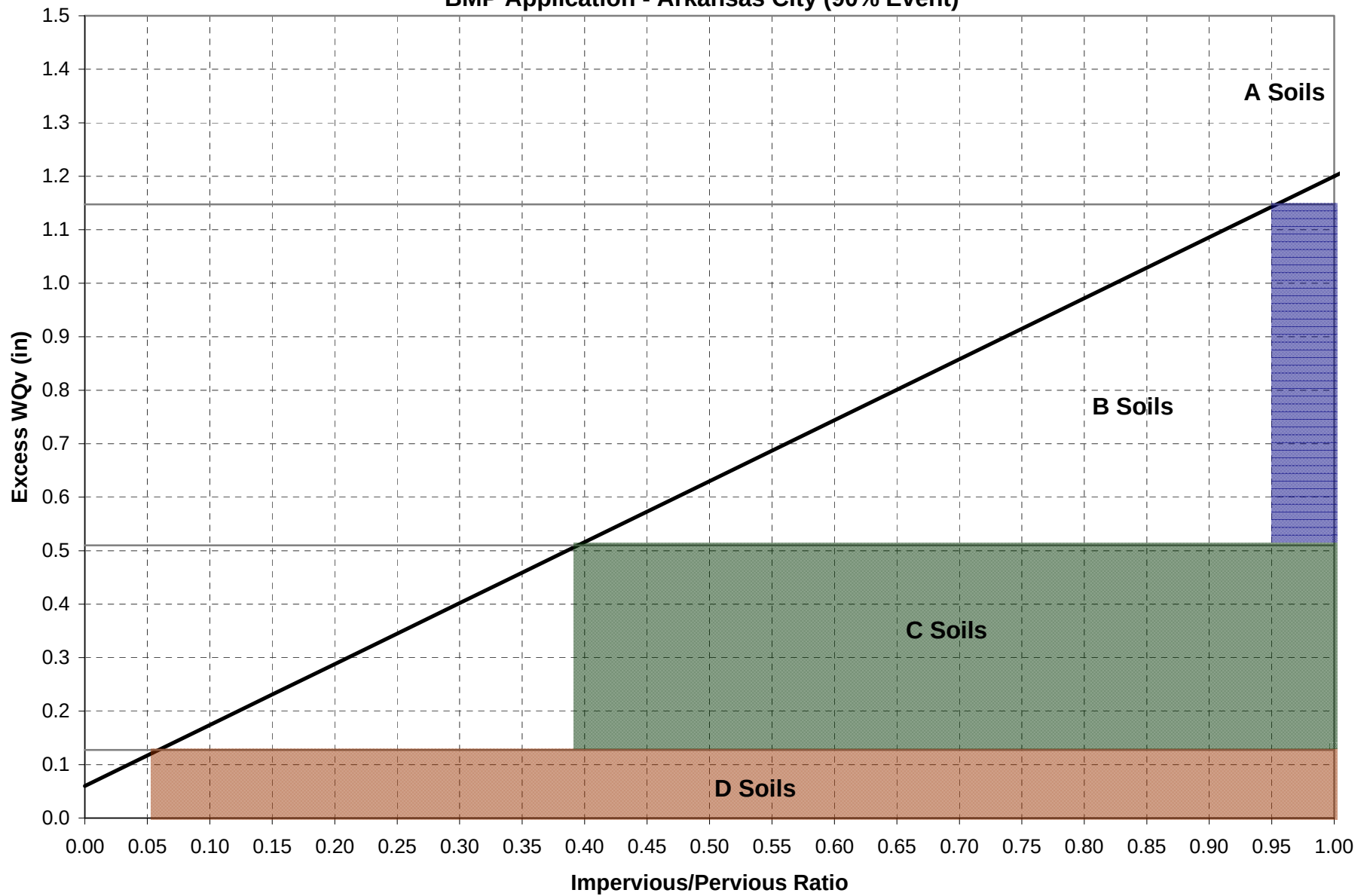
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Arkansas City (90% Event)



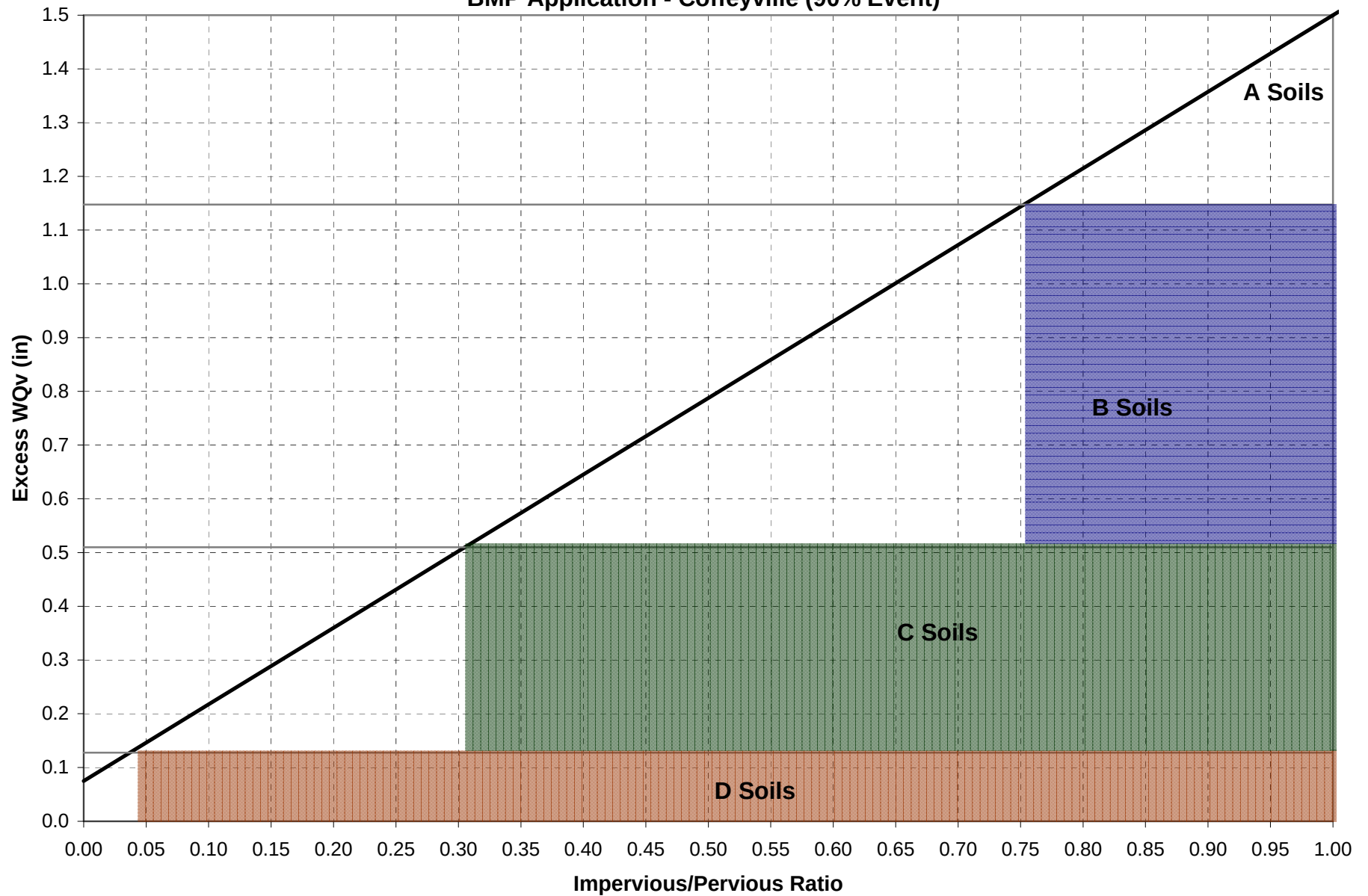
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Coffeyville (90% Event)



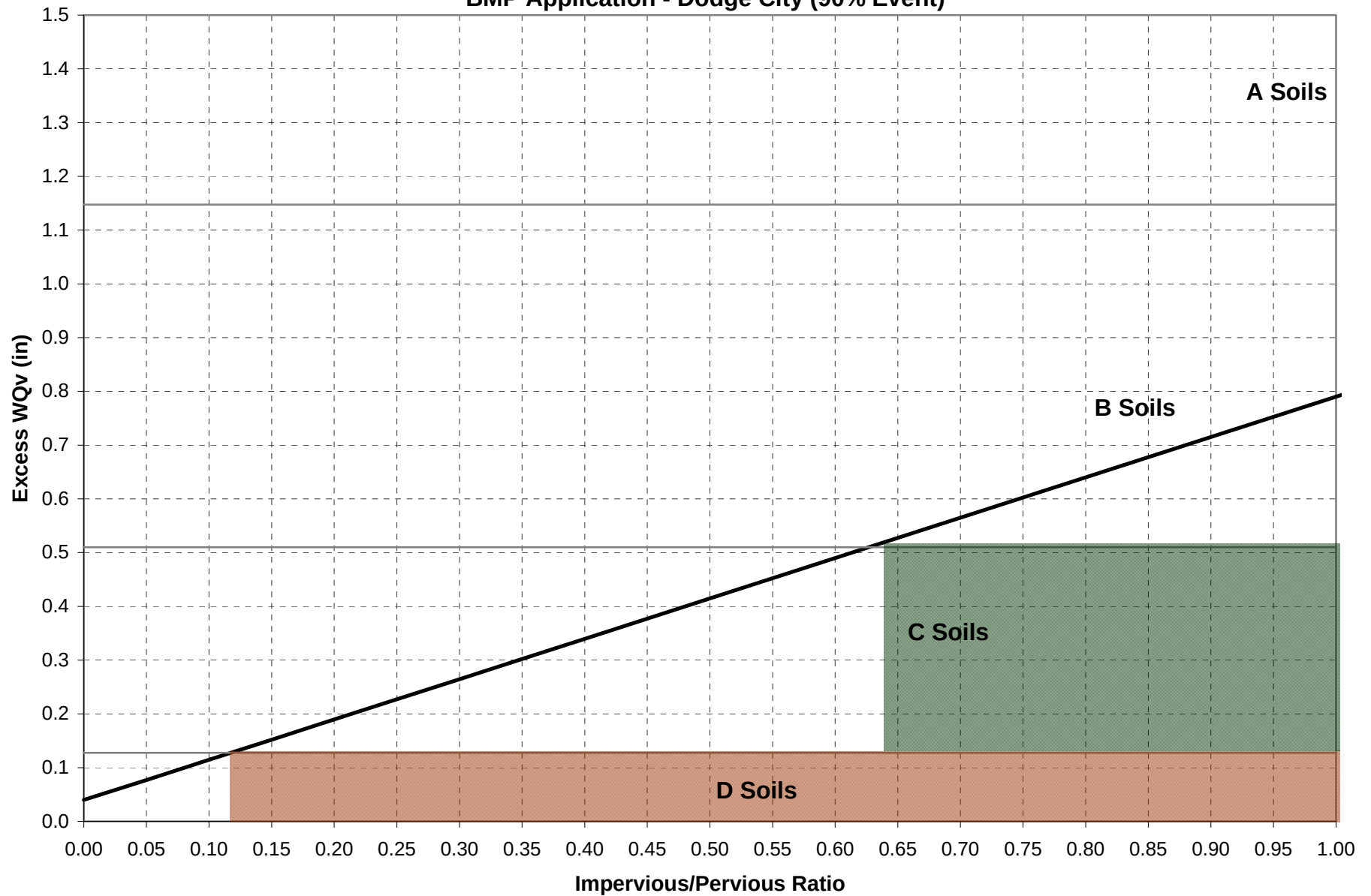
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Dodge City (90% Event)

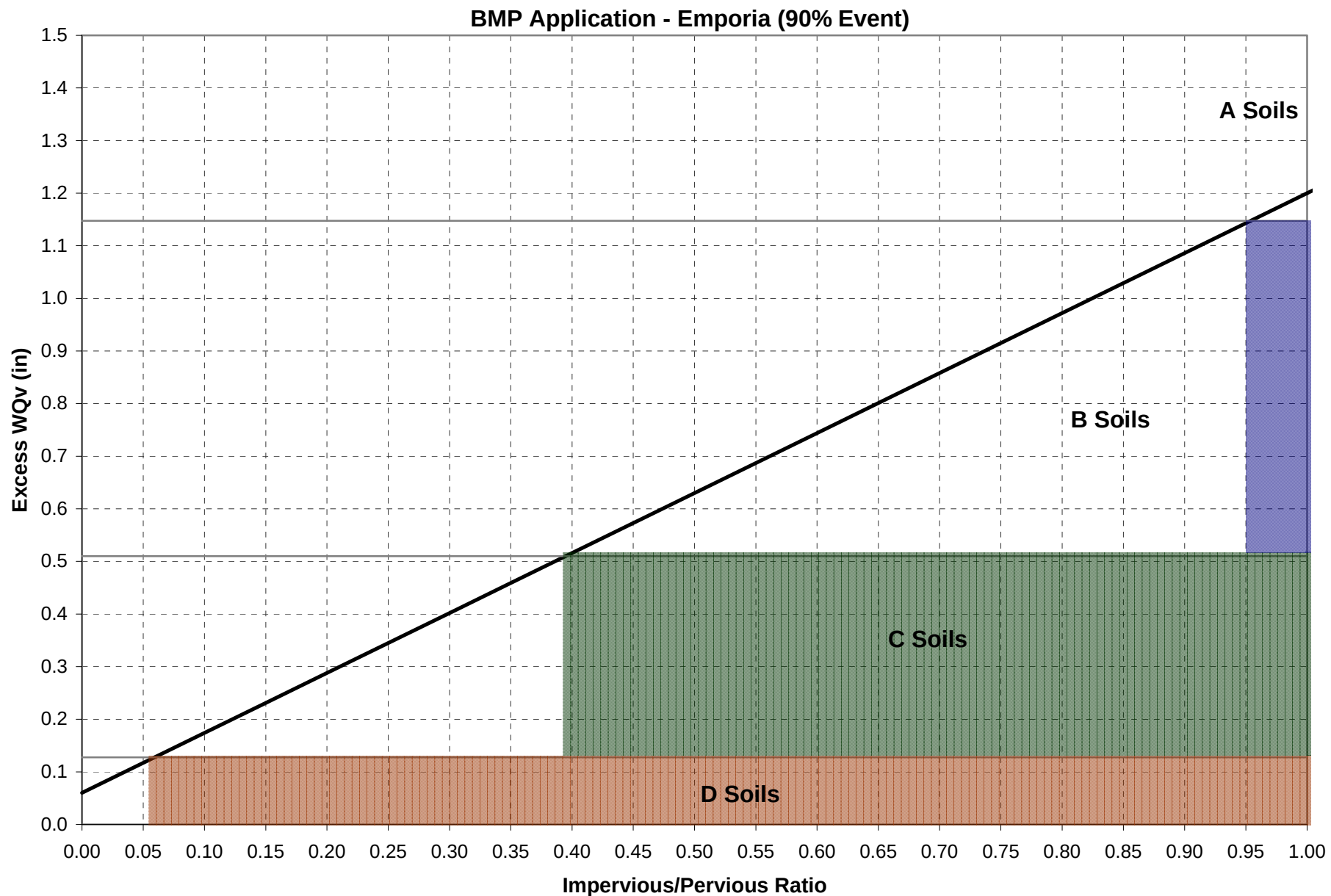


BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody



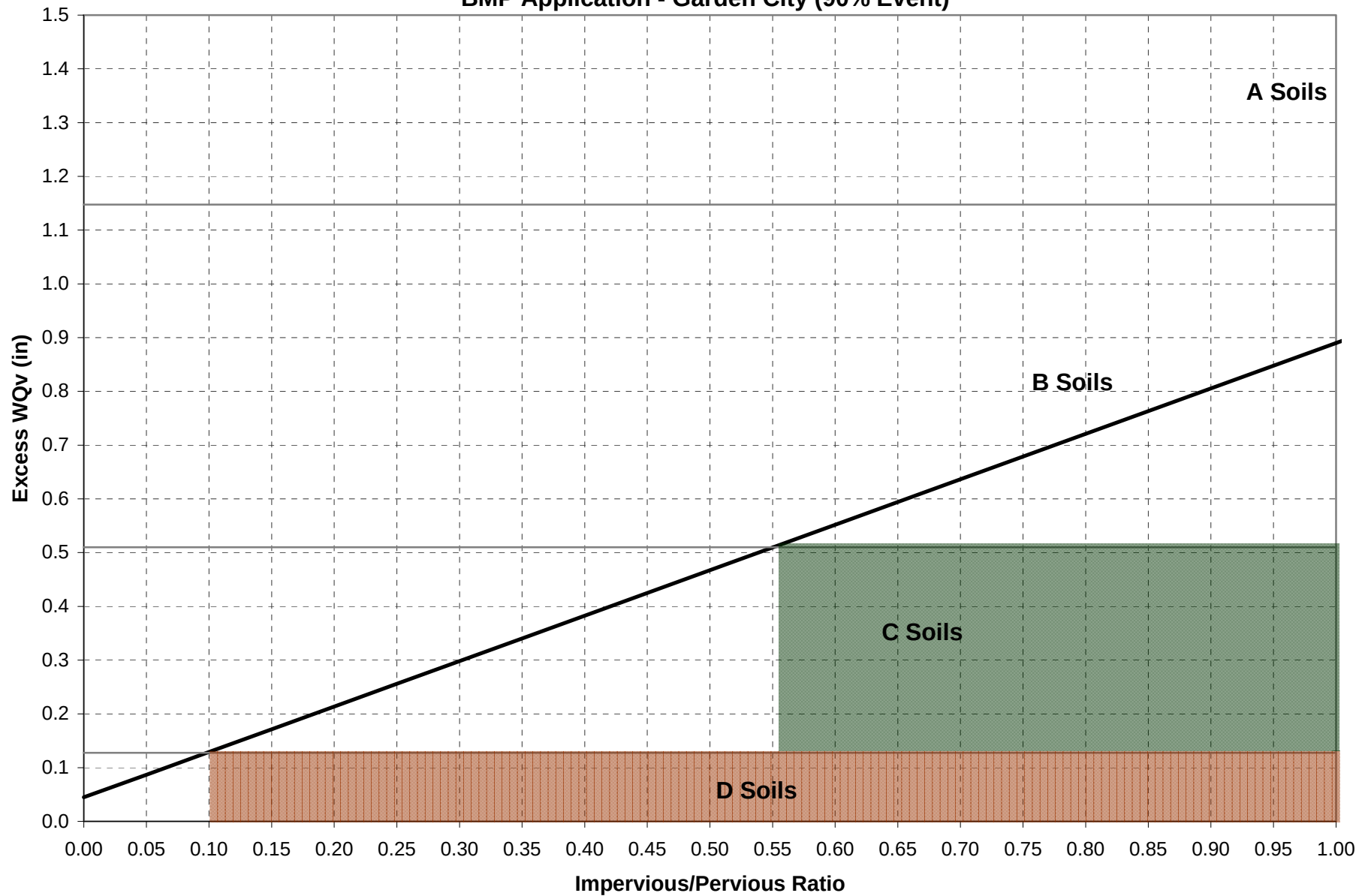
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Garden City (90% Event)



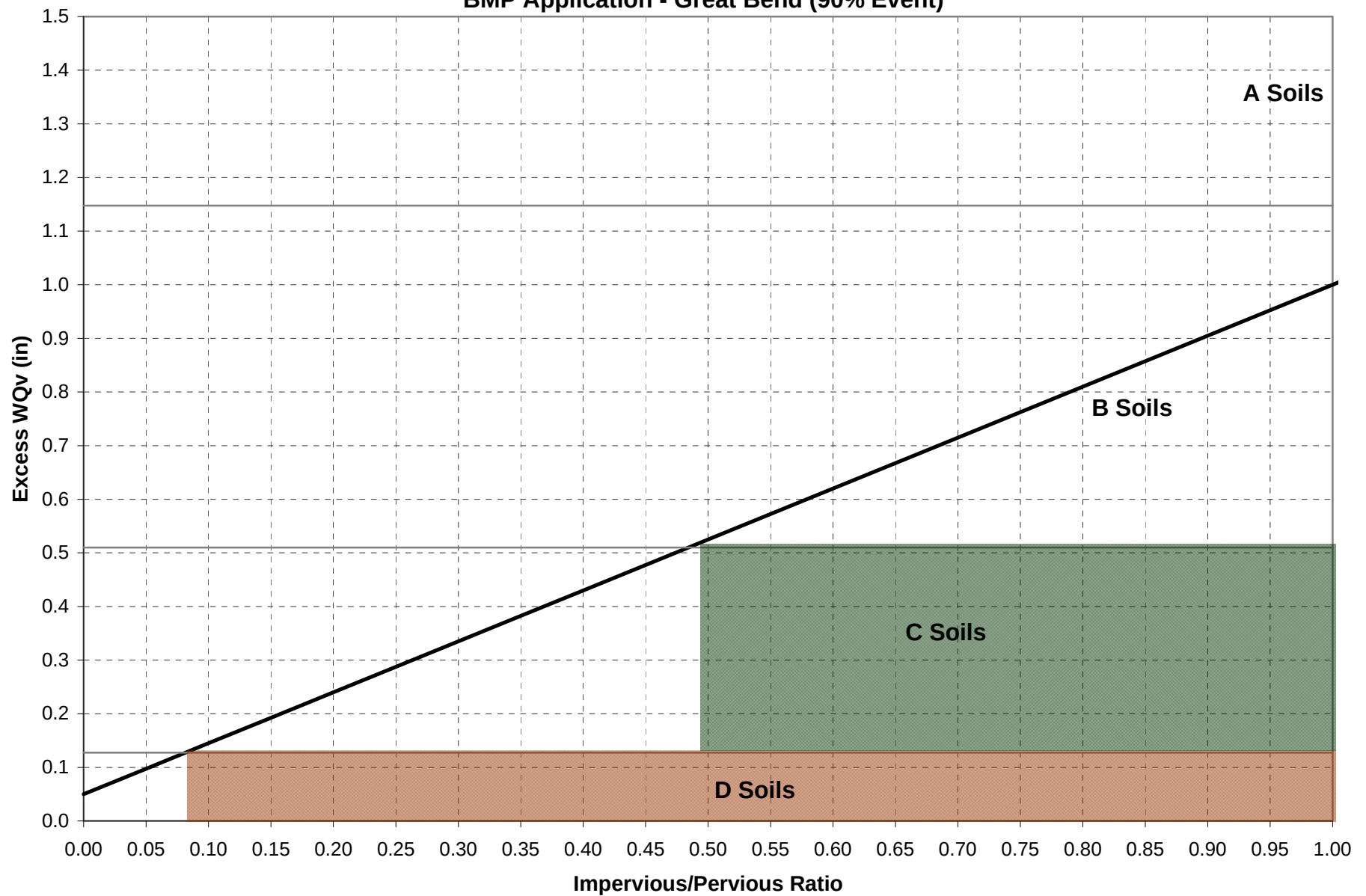
BMPs required within shaded area.

BMPs required for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Great Bend (90% Event)

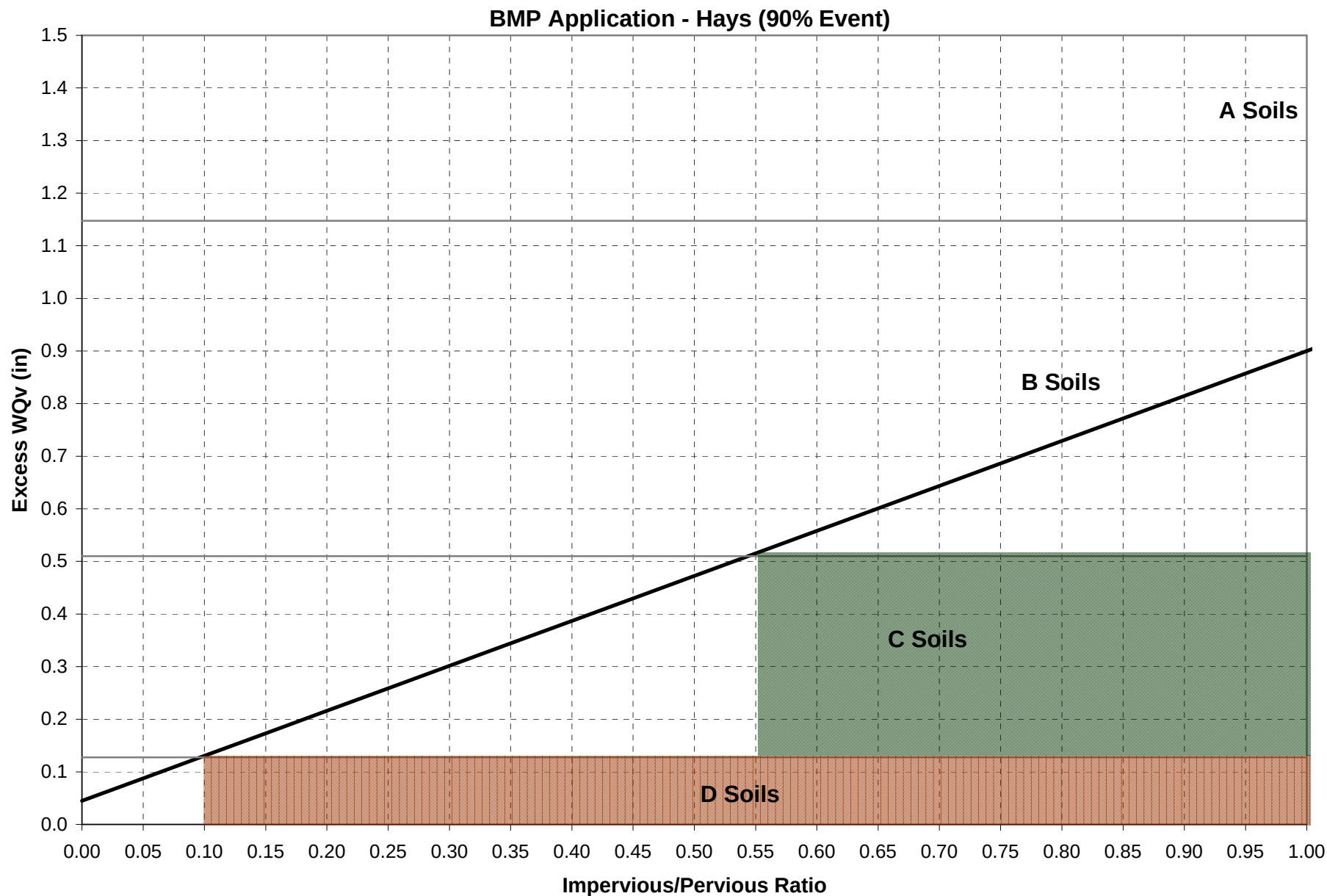


BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody



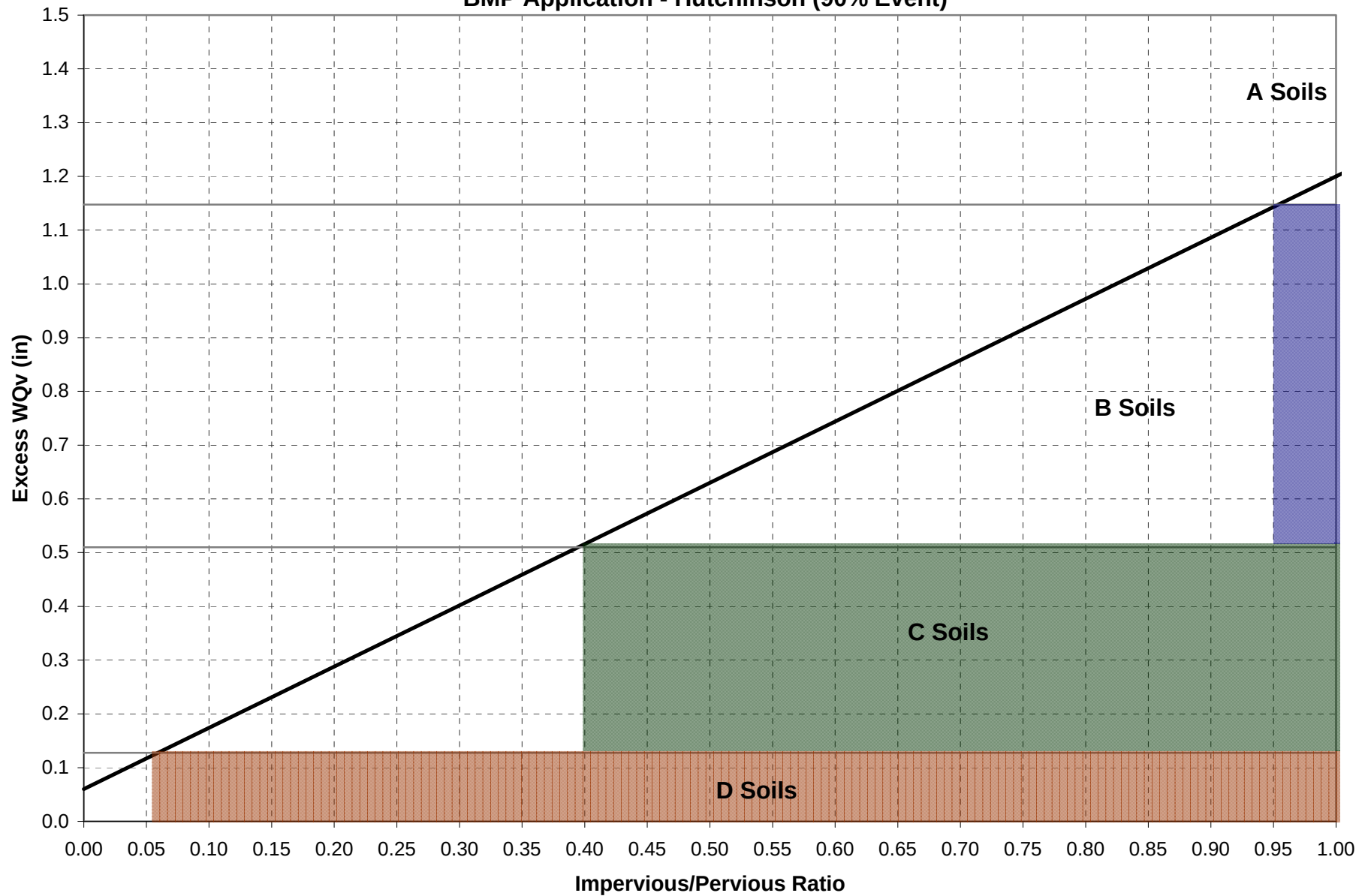
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Hutchinson (90% Event)



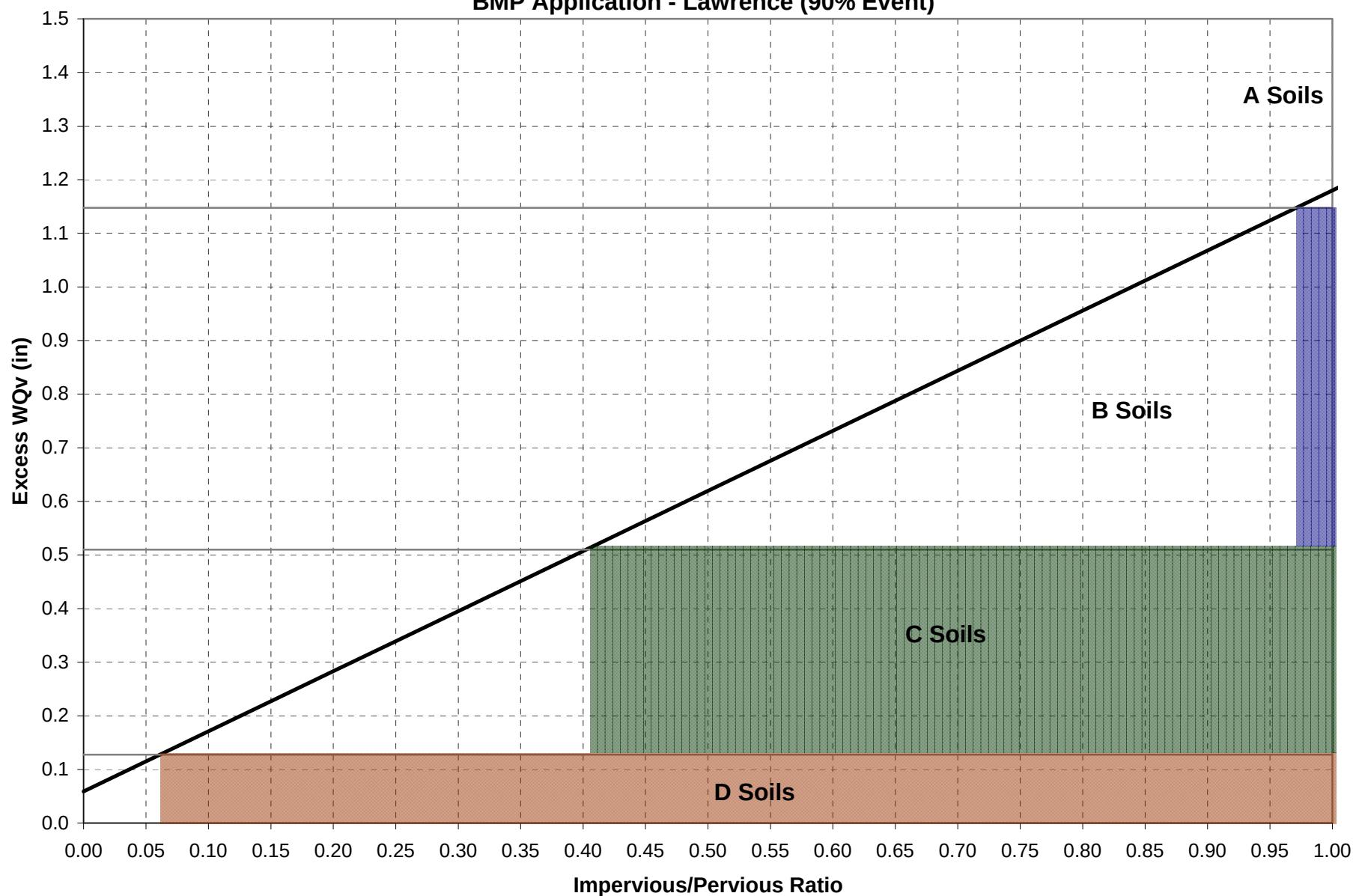
BMPs required within shaded area.

BMPs required for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Lawrence (90% Event)



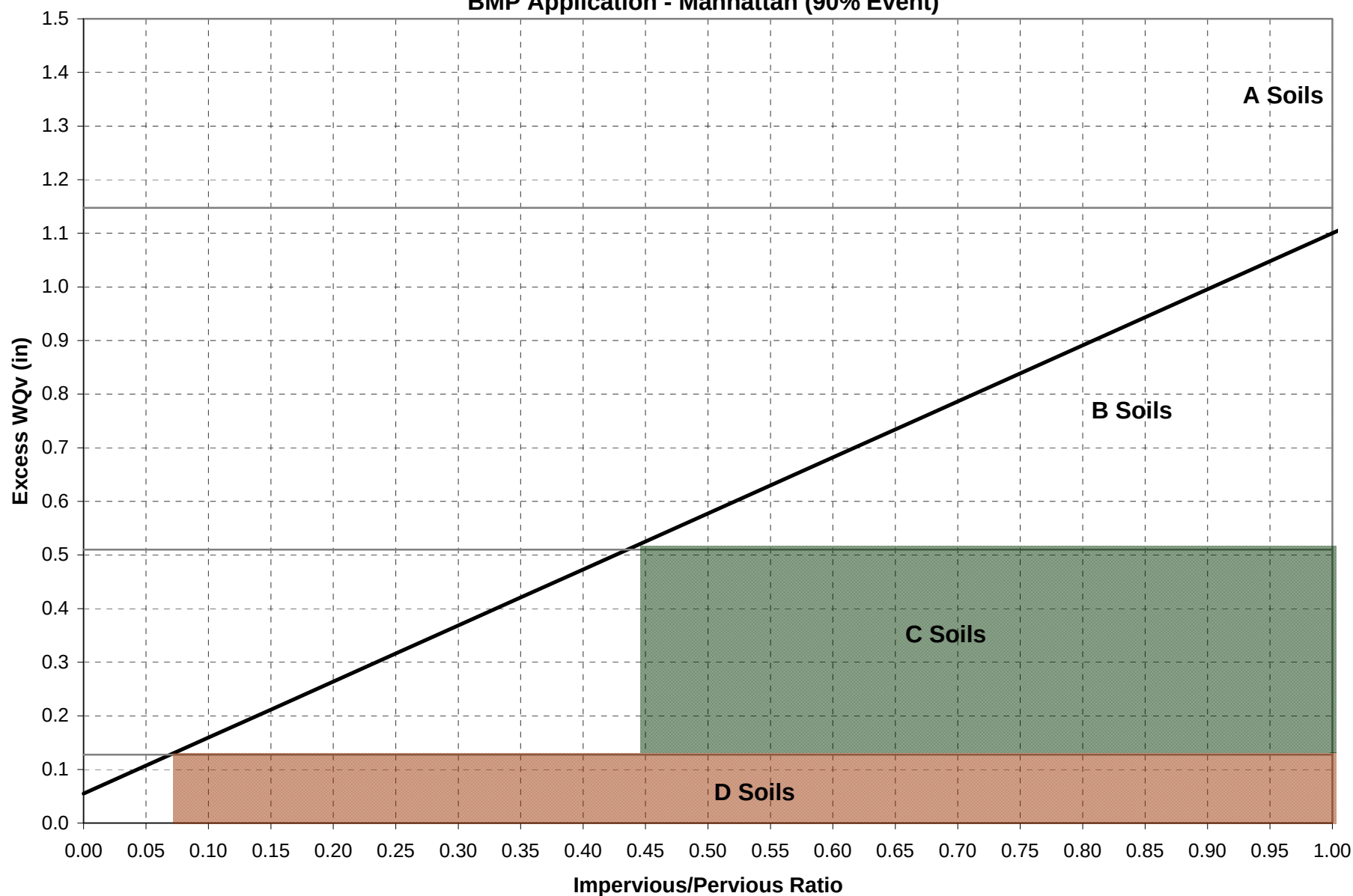
BMPs required within shaded area.

BMPs required for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Manhattan (90% Event)



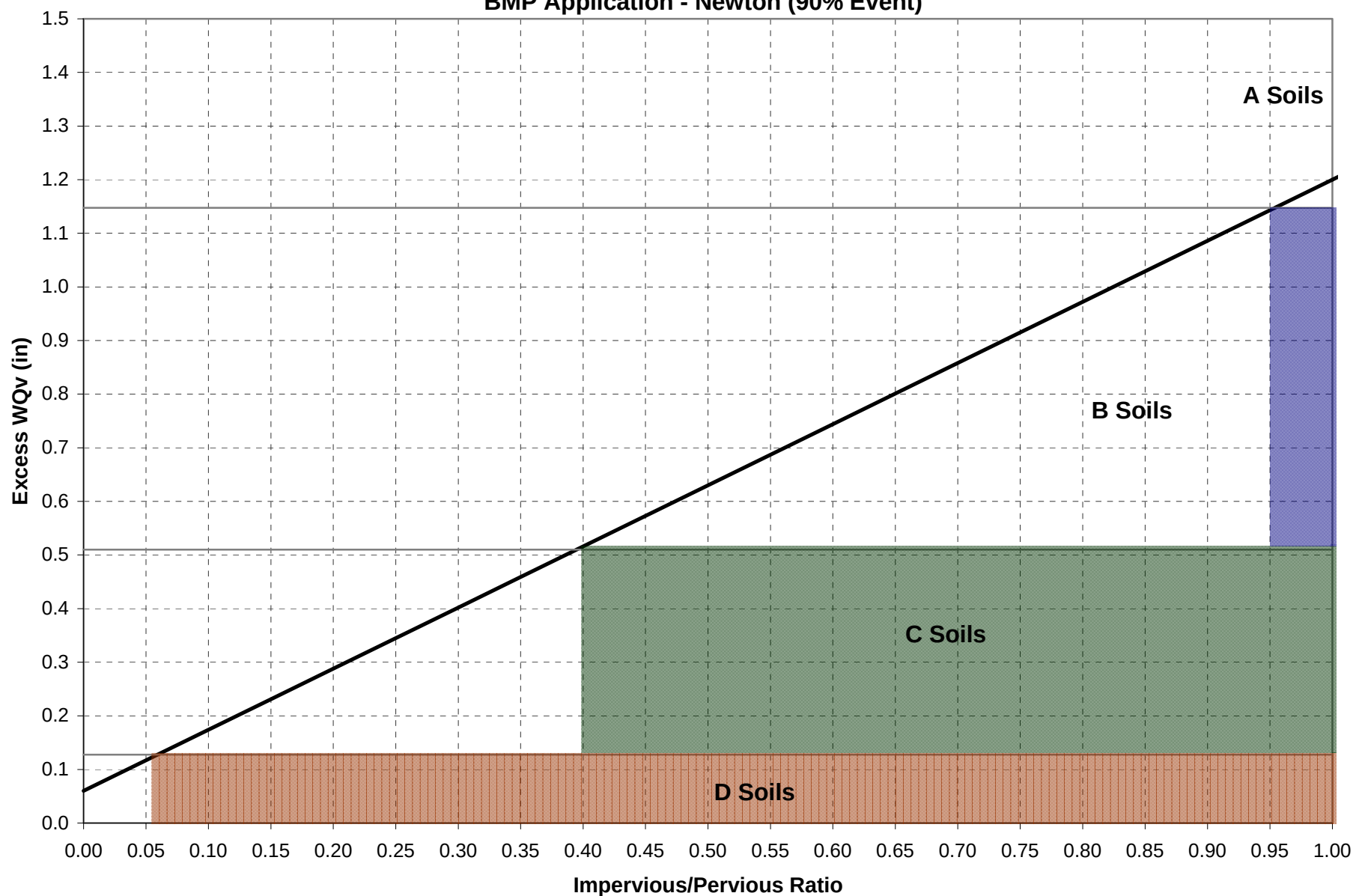
BMPs required within shaded area.

BMPs required for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Newton (90% Event)

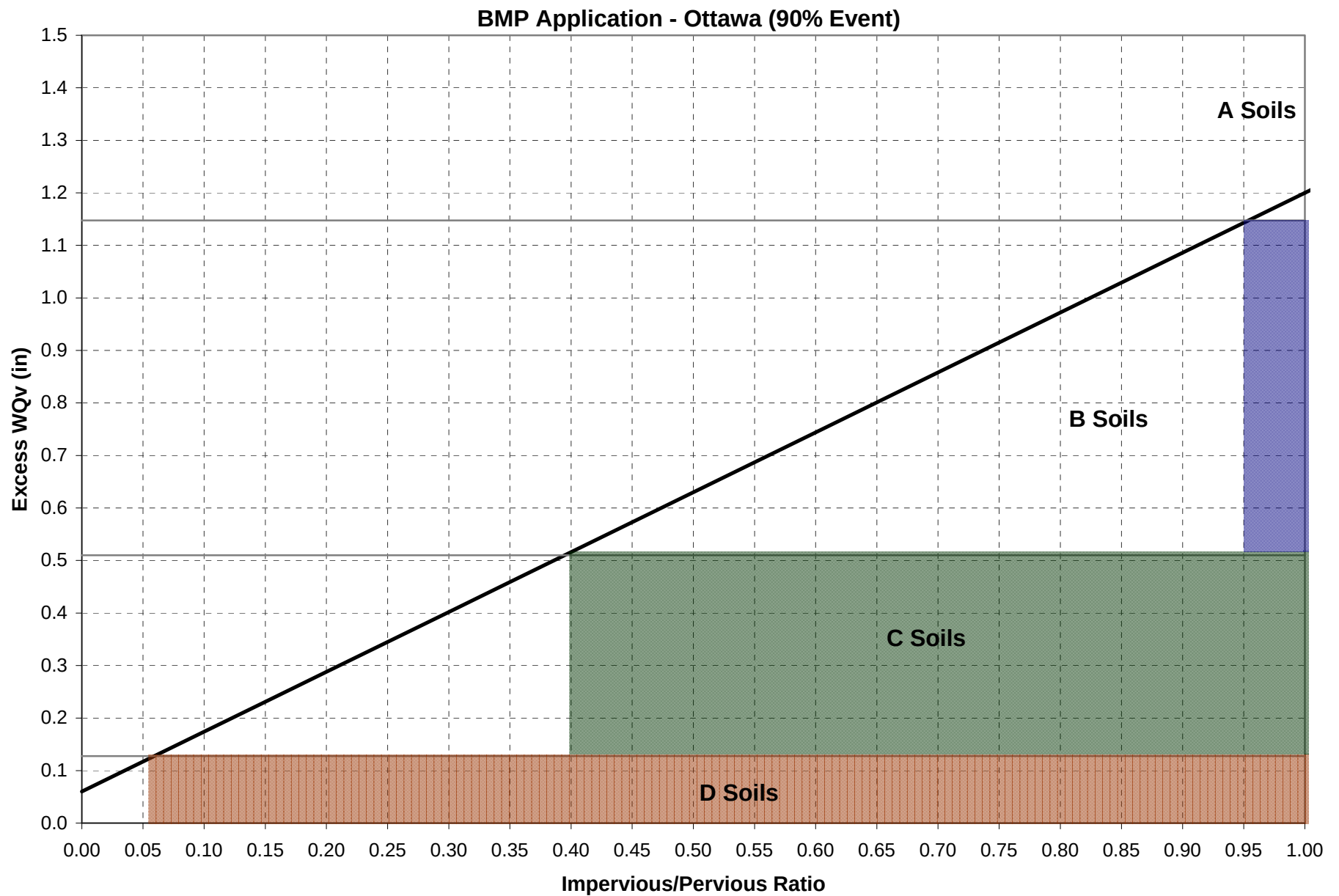


BMPs required within shaded area.

BMPs required for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody



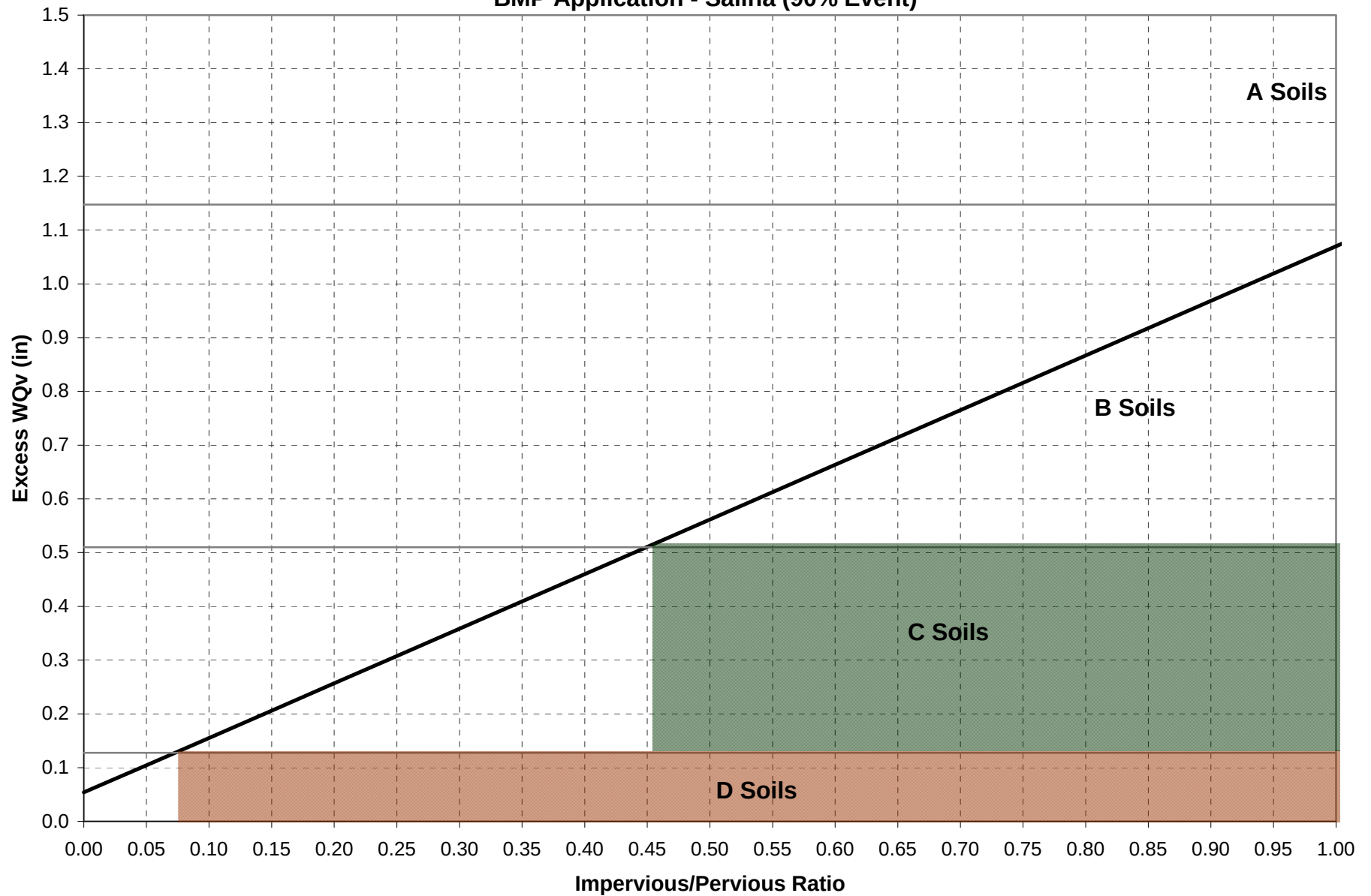
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Salina (90% Event)



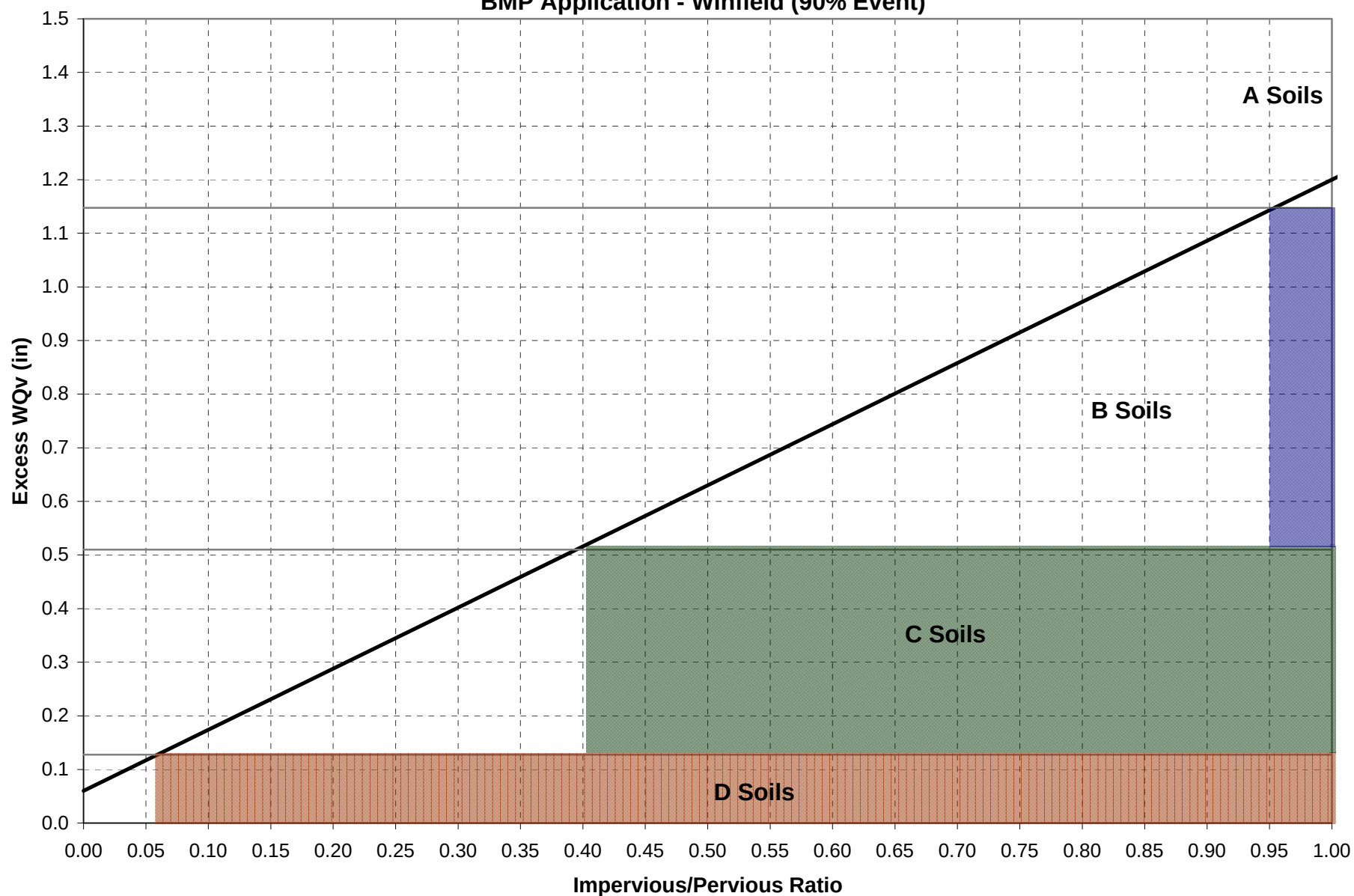
BMPs **required** within shaded area.

BMPs **required** for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody

BMP Application - Winfield (90% Event)



BMPs required within shaded area.

BMPs required for an impervious/pervious ratio > 1.0

Site hydrologic soil group (HSG) must be decreased one soil group level (e.g. B to C) if existing soils not preserved (See Section 2.1)

BMPs may be required outside of shaded area if receiving waters have established TMDL or a sensitive waterbody



